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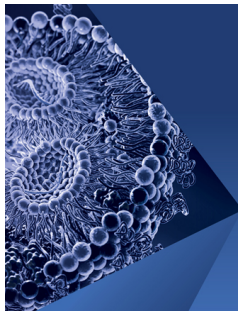
Publisher's Note: "Some rotational corrections to the acoustic energy equation in injection-driven enclosures" **[Phys. Fluids 17, 074102 (2005)]** **FREE**

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Physics of Fluids 19, 049901 (2007)

<https://doi.org/10.1063/1.2719179>



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(Received 22 November 2006; published online 25 April 2007)

[DOI: 10.1063/1.2719179]

This article was originally published online and in print with typographical errors in Table I; certain diacritical accents, such as the tilde and circumflex, needed to denote either rotational or irrotational components, were missing. AIP apologizes for this error. All online versions of the article have been corrected. The correct table appears below:

TABLE I. Linear growth rate corrections and the critical parameters delineating stability boundaries.

	Improved rotational set in general form	Evaluated growth rates (dimensionless)
α_1 : Pressure coupling	$E_m^2 = \frac{1}{2} \iiint [(\hat{p}_m)^2 + \hat{\mathbf{u}}_m \cdot \hat{\mathbf{u}}_m + 2\hat{\mathbf{u}}_m \cdot \hat{\mathbf{u}}_m^i + \hat{\mathbf{u}}_m^i \cdot \hat{\mathbf{u}}_m^i + \hat{\mathbf{u}}_m^i \cdot \hat{\mathbf{u}}_m^i + \hat{\mathbf{u}}_m^i \cdot \hat{\mathbf{u}}_m^i] dV$ $-E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle \hat{p}_m \hat{\mathbf{u}} + \frac{1}{2} M_b \mathbf{U}(\hat{p})^2 \rangle + M_b [\hat{\mathbf{u}} \cdot \nabla(\mathbf{U} \cdot \hat{\mathbf{u}})]} dV$	$\frac{4}{5} M_b [A_b^{(r)} - \gamma]$
α_2 : Dilatational	$E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle \frac{4}{3} \delta^2 \hat{\mathbf{u}} \cdot \nabla(\nabla \cdot \hat{\mathbf{u}}) \rangle} dV$	$-\frac{8}{15} \xi M_b^3 \ll O(1)$
α_3 : Acoustic mean	$E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle M_b \hat{\mathbf{u}} \cdot (\hat{\mathbf{u}} \times \boldsymbol{\Omega}) \rangle} dV$	0
α_4 : Flow turning	$E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle M_b \hat{\mathbf{u}} \cdot (\mathbf{U} \times \boldsymbol{\omega}) \rangle} dV$	$-\frac{4}{5} M_b (1 + \pi^{-2} M_b^2 \xi^2 l^2 m^{-2})^{-1}$
α_5 : Rotational flow	$-E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle \hat{\mathbf{u}} \cdot \nabla \hat{p} \rangle} dV$	$\frac{4}{5} M_b (1 + \pi^{-2} M_b^2 \xi^2 l^2 m^{-2})^{-1}$
α_6 : Mean vorticity	$E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle M_b \hat{\mathbf{u}} \cdot (\mathbf{U} \times \boldsymbol{\omega}) \rangle} dV$	$\frac{2}{5} M_b$
α_7 : Viscosity	$-E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle \delta^2 (\hat{\mathbf{u}} + \hat{\mathbf{u}}) \cdot (\nabla \times \boldsymbol{\omega}) \rangle} dV$	$-\frac{4}{15} M_b \xi [1 - \frac{1}{2} \xi + \frac{1}{3} \xi^2 - \frac{1}{15} \xi^3 + O(\xi^4)]$
α_8 : Pseudo acoustic	$E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle -\hat{\mathbf{u}} \cdot \nabla \hat{p} \rangle} dV$	$\frac{2}{5} (M_b^3 l^2 / m^2) \ll O(1)$
α_9 : Pseudo vorticity	$-E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle \hat{\mathbf{u}} \cdot \nabla \hat{p} \rangle} dV$	$\frac{9}{125} \pi M_b [(\xi^2 - \frac{3}{2}) \exp(-2\xi) + \frac{3}{2} - 3\xi + 2\xi^2] \xi^{-4}$
α_{10} : Unsteady nozzle	$-E_m^{-2} \exp(-2\alpha_m t) \iiint \sqrt{\langle M_b (\hat{\mathbf{u}} + \hat{\mathbf{u}}) \cdot \nabla(\mathbf{U} \cdot \hat{\mathbf{u}}) \rangle} dV$	$-\frac{4}{3} \pi M_b \{[\pi^2 + 4(\xi + \sqrt{2})^2]^{-1} - \frac{1}{500}\}$
Critical damping parameter	$\xi_r = -3\gamma_b + \sqrt{9\gamma_b^2 + 12M_b^2 / (4M_b^2)}$	
Critical aspect ratio	$l_r = m\pi\delta M_b^{-3/2} / \sqrt{\frac{5}{6} + \frac{\sqrt{35}}{3} \sinh(\frac{1}{3} \sinh^{-1}\{4[\frac{325}{4} + 27(-\frac{15}{2} - 15\gamma_b)]] / (35\sqrt{35})\}}$	
Critical Mach number	$M_{br} = \sqrt{6\{\frac{1}{2} - \gamma_b - [\frac{1}{4}\xi^{-2}(1 - 2\xi + 2\xi^2 - e^{-2\xi})]\}} \sqrt{(4\xi - 3l^2/m^2)}$	

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