

## E R R A T A

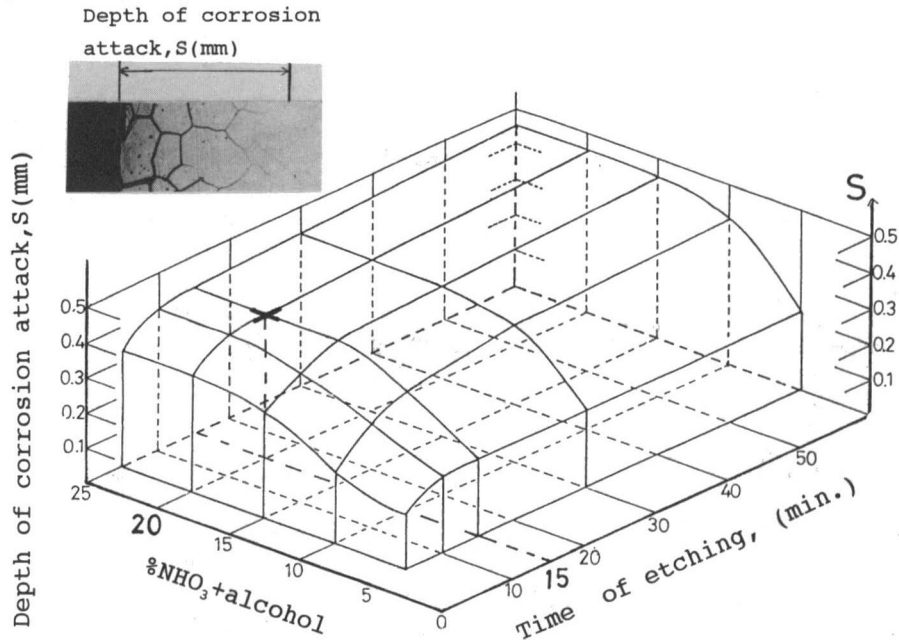
The following equations should read:<sup>1</sup>

$$u = \frac{R}{E \cos^2 \alpha} \left[ -(1 + \mu) A_{1j} R^{M_1} + (1 - \mu) A_{2j} R^{M_2} + (\cos^2 \alpha - \mu) A_0 \right] \quad (41)$$

$$P_{j+1} = \frac{R_j^2}{2} \left\{ A_{3j} \cos^2 \alpha \frac{E u_j}{R_j} - \left( \frac{2}{R_j^2} + \cos^2 \alpha A_{3j} - A_{4j} \right) A_0 - (\mu A_{3j} - A_{4j}) P_j \right\} \quad (42)$$

Due to a printer's error, the following figures were not reproduced:

Figure 11 on p. 18<sup>2</sup>



**Fig. 11 Graph for determining best condition of HNO<sub>3</sub> + alcohol solution as a substitute for the special picric acid solution**

Figure 2 on p. 22<sup>3</sup>



**Fig. 2 Window sample from furnace A is approximately 2 in. x 6 in. The longer length is the longitudinal direction (parallel to tube axis). The creep rupture test specimens were prepared so that the circumferential direction was tested.**

<sup>1</sup>For "A New Approach to Stress Analysis of Various Wound Vessels," by P. S. Huang and C. R. Friedrich, published in the November 1994 issue of the JOURNAL OF PRESSURE VESSEL TECHNOLOGY, Vol. 116, pp. 359-364.

<sup>2</sup>For "A Creep Damage Estimation Method for In-Service Fossil Fuel Boiler Superheater Tubes," by F. Nogata and H. Takahashi, published in the February 1995 issue of the JOURNAL OF PRESSURE VESSEL TECHNOLOGY, Vol. 117, pp. 14-18.

<sup>3</sup>For "Life Assessment of 1/4 Cr-1/2 Mo Steel Catalytic Reformer Furnace Tubes Using the MPC Omega Method," by S. Ibarra and R. R. Konet, published in the February 1995 issue of the JOURNAL OF PRESSURE VESSEL TECHNOLOGY, Vol. 117, pp. 19-23.