

Determination of the optimal rate for the microaerobic treatment of several H₂S concentrations in biogas from sludge digesters

I. Díaz, A. C. Lopes, S. I. Pérez and M. Fdz-Polanco

ABSTRACT

The treatment of H₂S in the biogas produced during anaerobic digestion has to be carried out to ensure the efficient long-lasting use of its energetic potential. The microaerobic removal of H₂S was studied to determine the treatment capacity at low and high H₂S concentrations in the biogas (0.33 and 3.38% v/v) and to determine the optimal O₂ rate that achieved a concentration of H₂S of 150 mg/Nm³ or lower. Research was performed in pilot-plant scale digesters of sewage sludge, with 200 L of working volume, in mesophilic conditions with a hydraulic retention time of 20 d. O₂ was supplied at different rates to the headspace of the digester to create the microaerobic conditions. The treatment successfully removed H₂S from the biogas with efficacies of 97% for the low concentration and 99% for the highest, in both cases achieving a concentration below 150 mg/Nm³. An optimal O₂ rate of 6.4 NLO₂/Nm³ of biogas when treating the biogas was found with 0.33% (v/v) of H₂S and 118 NLO₂/Nm³ of biogas for the 3.38% (v/v) concentration. This relation may be employed to control the H₂S content in the biogas while optimising the O₂ supply.

Key words | biogas, dose control, H₂S removal, microaerobic, optimal O₂ rate

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INTRODUCTION

The treatment of wastewater in municipal wastewater treatment plants (WWTP) generates sludge as a by-product of the overall processes employed during treatment. When disposing of this sludge, anaerobic digestion (AD) is an important step in most treatment processes. AD is able to transform a large part of the organic matter content into biogas, 60–70% (v/v) of methane.

In the AD of S-containing organic matter, H₂S is generated to a different extent (10–70 g/m³ in the biogas) based on the outcome of the competition between sulfur-reducing bacteria and methanogens (Lens & Pol 2000). H₂S in the biogas reduces the lifetime of the pipework and other installations needed for the utilisation of biogas. For example, the trouble free operation of CHP (combined heat and power) requires limit values between 100 and 500 mg/Nm³, depending on the specifications of the CHP manufacturer, and these values may not be exceeded. H₂S is toxic and corrosive to many types of steel (Deublein & Steinhauser 2008). Therefore, the treatment of the biogas has to be carried out to ensure the efficient long-lasting use of its energetic potential.

Biological treatment technologies have shown lower treatment costs and low or no requirements for additional chemical products compared to the traditional physico-chemical technologies (Syed *et al.* 2006). Besides, biological removal has proven successful in the large-scale employment of biotrickling filters and bioscrubbers (Janssen *et al.* 2001).

The technologies are based on the biological oxidation of H₂S, which employs O₂ as electron acceptor, carried out by sulfide-oxidising microorganisms. The final products of the biological oxidation depend on the amount of O₂ available for sulfide-oxidising bacteria. Some well-known and novel sulfur-oxidising bacteria are able to employ sulfide as an electron donor under anaerobic conditions similar to those in the AD of sludge, such as *Thiomicrospira* sp. and *Thiobacillus* sp. (Tang *et al.* 2009). The predominance of S⁰ or SO₄²⁻ as the final product of the oxidation depends on the O₂ availability, thus in limited conditions (microaerobic) S⁰ is the main final product (Janssen *et al.* 1995).

Microoxygenation of the ‘anaerobic digester’ is an alternative to perform biological removal of H₂S due to some of the bacteria responsible for the sulfur oxidation

being present in the sludge (Abatzoglou & Boivin 2009). Several agro-industrial applications of AD perform this process in Europe by continuously supplying 4–6% of air in relation to the biogas production into the headspace of the biodigester, where sulfur-oxidising microorganisms develop, thereby reaching H₂S concentrations below 200 ppmv (Weiland 2010).

In this sense, Jenicek *et al.* (2008) reported H₂S removal from the biogas and enhanced VSS and soluble COD degradation when air was supplied during sludge recirculation and a slight decrease in some recalcitrant compounds (AOX) in full-scale sludge digesters (Jenicek *et al.* 2010).

In previous studies we have found that the removal of H₂S in the biogas produced in an anaerobic sludge digester by microoxygenation reduced the concentration of H₂S from 0.9 to 1.2% (v/v) to less than 0.3% (v/v) with no effect on digestion performance (Fdz-Polanco *et al.* 2009). The utilisation of air with a similar O₂ rate to pure O₂ was also found successful while NO₃⁻ could not be used to desulfurise the biogas in the case of sludge digestion (Díaz *et al.* 2010a) and the headspace was the optimal dosing point for H₂S removal from the biogas (Díaz *et al.* 2010b).

Finally, in full-scale treatment of sewage sludge, biogas production varies as a result of the variable COD and VS concentrations of the feed. Then, the O₂ rate to the bioreactor for the microaerobic removal of H₂S must vary according to the amount of H₂S produced to optimise the O₂ flow supplied and to avoid an excessive concentration of O₂ not utilised in the biogas or, otherwise, not enough for the expected H₂S removal. Khanal & Huang (2003) suggested employment of the oxidation–reduction potential (ORP) to control the O₂ dosing; however, in the particular case of sludge digestion, ORP remains invariable during microaerobic treatment (Jenicek *et al.* 2010; Díaz *et al.* 2010b), therefore a different controlling method must be found.

In this study, we focus on evaluating the performance of the H₂S removal in a wider concentration interval (0.33 and 3.3% (v/v)), and on the determination of the optimal O₂ flow for the H₂S content in the biogas, subsequently observing the feasibility of the control of the dosing by the biogas production rate.

MATERIALS AND METHODS

Pilot plant description

The treatment of sludge and the removal of H₂S were performed in pilot-plant scale reactors with a working

volume of 200 L (250 L total volume), as shown in Figure 1. The reactors were insulated, and the walls were heated with electric resistance. The reactors were also mixed with biogas recirculation provided at a rate of ~4 L/min of biogas; this flow was periodically checked with a rotameter. The feed was provided from a continuously stirred tank with a peristaltic pump. Microaerobic conditions were maintained using the regulated flow of pure O₂ with a mass flow controller from an O₂ cylinder injected into the headspace. The headspace in the bioreactor (50 L) allowed the storage of ~1/4 of the daily biogas production.

Operational conditions

The pilot-plant study was developed in the anaerobic sludge digesters from previous anaerobic/microaerobic experiments. A pseudo-stationary anaerobic state was obtained prior to the beginning of the experiments by maintaining at least 20 days without any O₂ supply. Digestion of the sludge was performed in the mesophilic range (35 ± 1 °C) with an HRT of ~20 days. The feed consisted of mixed sludge (approximately 60% of primary sludge and 40% of activated sludge) from the Villalonquejar WWTP (Burgos, Spain) with a variable organic load (COD_T max–min [68–35] g/L). In experiment 1, raw sewage sludge was treated while in experiment 2, Na₂SO₄ was added to the feed with a concentration of ~2,200 mg/L of SO₄²⁻ to increase the amount of H₂S produced. O₂ supply was increased in stages until H₂S concentration in the biogas was

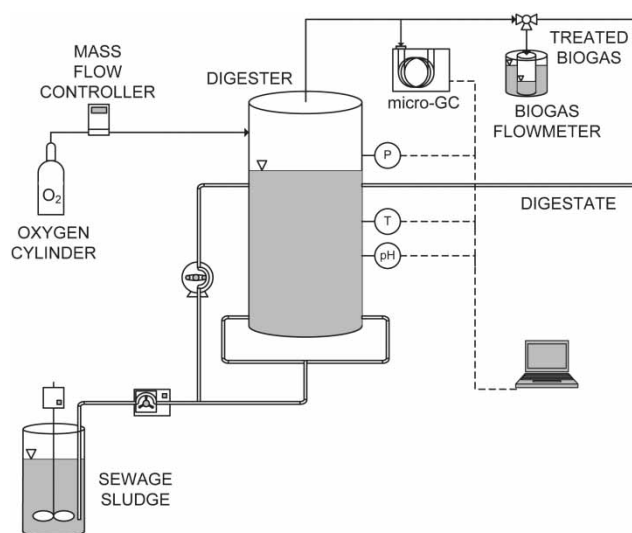


Figure 1 | Pilot-plant diagram.

Table 1 | Operational conditions during the study

	Experiment 1	Experiment 2
Duration (d)	80	45
Mixing	BR	BR
Microoxygenation		
Rates applied (NL/d)	0, 0.47, 0.51, 0.74, 0.97	0, 9.3, 10.9, 14.1
Sulfate concentration in feed (mg/L)	0	~2,200

BR: biogas recirculation.

consistently below 150 mg/Nm³. These conditions are summarised in Table 1.

Monitoring and experimental analysis

The pilot-plant conditions were monitored online using pressure, temperature (PT100) and pH probes.

The biogas production gas measured by a fixed volume of liquid displacement (472 ± 8 Nm L) in an inverted cylinder equipped with an electrovalve. The biogas composition was measured by gas chromatography in intervals of 6 to 24 h depending on the variability of the H₂S concentration in the biogas as reported by Díaz *et al.* (2010b). The combination of biogas production and H₂S concentration in the biogas allowed us to evaluate the performance of the H₂S removal.

SO₄²⁻ and S₂O₃²⁻ concentrations were measured by HPLC according to the method described by van der Zee *et al.* (2007).

Total and soluble COD concentrations as well as total dissolved S²⁻, in feed sludge and digested sludge, were evaluated weekly according to standard methods (Clesceri *et al.* 1998). The present research is not suited to evaluating the effect of oxygen introduction on organic matter removal and biogas production; in this sense, Fdz-Polanco *et al.* (2009) and Díaz *et al.* (2010a) developed this

aspect for similar O₂ rates to those employed in this research.

RESULTS AND DISCUSSION

H₂S removal capacity

The average H₂S concentration in the biogas produced during experiment 1 in the anaerobic period (without O₂ supply) was 0.33 ± 0.02% (v/v). O₂ supply to the digester started on day 10 at a rate of 0.47 NL/d and was increased in stages as shown in Figure 2(a). The final H₂S concentration in the biogas dropped gradually as O₂ rate was increased. For the highest rate (0.97 NL/d), H₂S concentration was always below 0.01% (v/v). H₂S was removed from the biogas with an efficacy higher than 97% for a rate of 0.97 NL/d of O₂.

O₂ concentration in the biogas remained below 0.1% (v/v) during the study, while H₂S was removed, and slightly increased when H₂S was totally removed indicating an excess of O₂ supplied.

CH₄ and CO₂ concentrations in the biogas remained stable during the experiment as shown in Figure 3(a), and were not affected by O₂ supply in the headspace. CH₄ accounted for an average 64.9 ± 1.4% (v/v) in the anaerobic period without O₂ supply and an average 64.5 ± 1.3% (v/v) during the microaerobic period at the highest O₂ rate (0.97 NL/d). Neither was the biogas production was affected by the limited oxygen supply to the digester.

To evaluate the result of H₂S oxidation, the sulfur species were analysed and are shown in Figure 4(a). The concentration of SO₄²⁻ in the effluent was negligible during all the experiment while S₂O₃²⁻ appeared in the microaerobic period to reach a final concentration of ~10 mg/L. Total dissolved S²⁻ was ~46 mg/L in the anaerobic period and it dropped below 15 mg/L in the final microaerobic period. This shows that both gaseous and dissolved sulfide were removed as a result of the biogas recirculation.

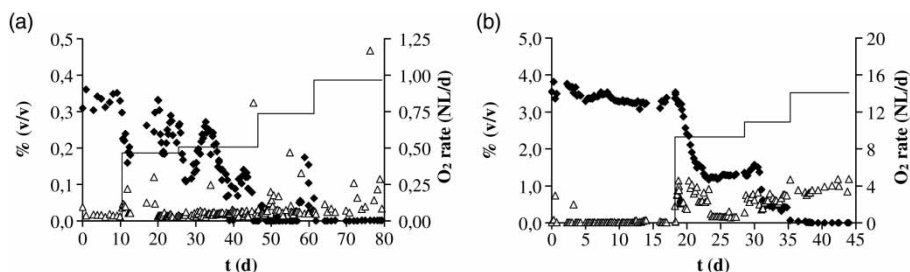


Figure 2 | H₂S (◆) and O₂ (△) concentrations in the biogas and O₂ rate (—) during the study. (a) Experiment 1 (raw sludge feed). (b) Experiment 2 (sludge and SO₄²⁻ feed).

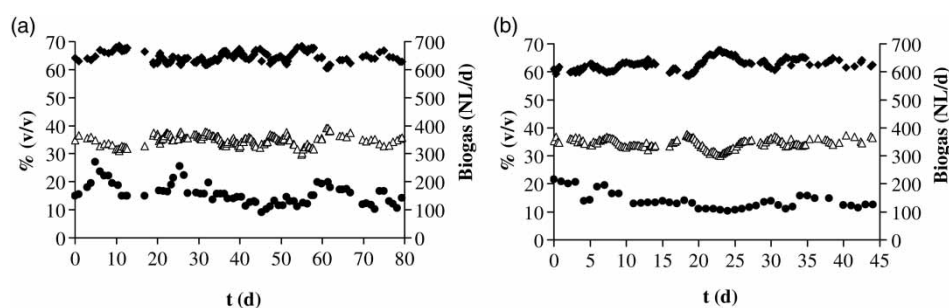


Figure 3 | CH₄ (◆) and CO₂ (△) concentrations in the biogas and daily biogas production (●) during the study. (a) Experiment 1. (b) Experiment 2.

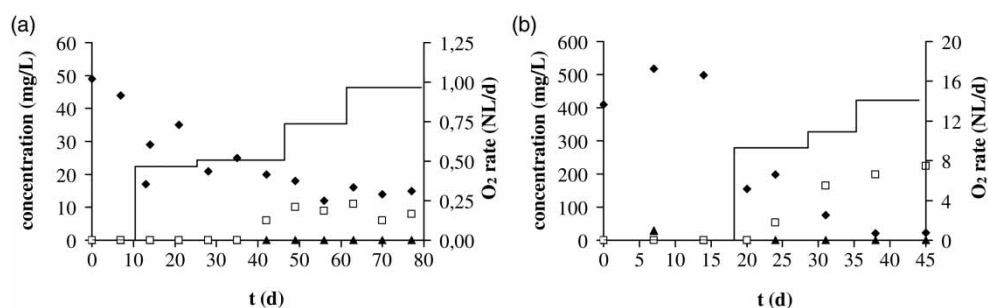


Figure 4 | Sulfur species concentration in the digester (mg/L), (◆) total dissolved S²⁻, (□) S₂O₃²⁻, (▲) SO₄²⁻, and O₂ rate (—). (a) Experiment 1. (b) Experiment 2.

Then, it can be assumed that the main product of H₂S was S⁰, limited oxygen introduction avoided SO₄²⁻ production.

During experiment 2, the average content of H₂S in the biogas in the anaerobic period was $3.38 \pm 0.16\%$ (v/v). This high concentration was the result of SO₄²⁻ addition to the feed sludge. To observe the capacity of microaerobic removal with the high concentration of H₂S produced in this study, O₂ was supplied beginning on day 18 with a rate of 9.3 NL/d of pure O₂. In the same way as in experiment 1, O₂ supply was increased in stages as shown in Figure 2(b) until the concentration was below 0.01% (v/v) in all the biogas composition analyses. Microaerobic conditions with a rate of 14.1 NL/d removed the H₂S content from the biogas with a removal efficacy higher than 99%.

In experiment 2, a final concentration of O₂ in the biogas of ~1% (v/v) was found when H₂S was totally removed. This concentration was higher compared to experiment 1 as a result of mass transfer limitations.

The concentrations of the main constituents of biogas, CH₄ and CO₂, were not reduced in this case (Figure 3(b)) despite the higher O₂ rate necessary to remove the larger amount of H₂S. CH₄ concentration in the anaerobic stage of experiment 2 was $61.5 \pm 1.7\%$ (v/v) and average concentration of CH₄ with an O₂ supply of 14.1 NL/d was $63.1 \pm 1.0\%$ (v/v). This slight increase of CH₄ in the biogas is the result of the H₂S disappearance from the biogas. This effect was also observed

in the CO₂ concentration, which rose from $34.6 \pm 1.2\%$ (v/v) in the anaerobic period to $35.6 \pm 1.0\%$ (v/v) in the microaerobic period with the highest O₂ rate.

The sulfur species in experiment 2 (Figure 4(b)) showed an increase in S₂O₃²⁻ concentration as O₂ rate was increased, while total dissolved S²⁻ dropped from ~475 mg/L in the anaerobic period to a final concentration of ~20 mg/L. In this case, dissolved sulfide was also removed as in experiment 1 with S⁰ as the main product; nevertheless, the appearance of S₂O₃²⁻ was observed until a final concentration of ~210 mg/L indicating oxidation slightly further than S⁰. The formation of S₂O₅²⁻ was probably because the result of a higher rate of O₂ applied to oxidise all the H₂S content and a further oxidation took place as a consequence of O₂ availability.

Therefore, limited oxygen supply to the bioreactor can be employed in a wide range of H₂S production (previous research showed 99% removal efficacy for a concentration of H₂S around 1% v/v, Fdz-Polanco et al. 2009) whereas the energetic content of the biogas (CH₄ concentration) was maintained in microaerobic conditions.

Optimal oxygen rate determination

The biogas production variability, a result of the variable COD in the feed sludge, caused deviations in the H₂S

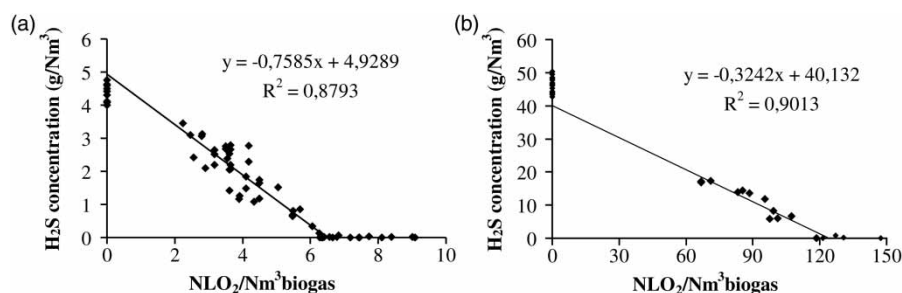


Figure 5 | Correlation between the ratio of O₂ supplied/biogas produced and the concentration of H₂S in the biogas. (a) Experiment 1. (b) Experiment 2.

concentration as O₂ is the limiting reactive for the lower O₂ rates. So, optimal O₂ rate must be adjusted to the biogas production to avoid a lack of the expected removal (when COD in the feed sludge is low) or an excess of O₂ in the biogas (for the higher COD loads in the feed sludge).

The ratio of O₂ rate/Biogas production rate was compared to the final H₂S concentration in the biogas during the study to achieve the mentioned optimal flow (Figure 5).

In experiment 1, it was found that a ratio of 6.4 NLO₂/Nm³ of biogas or higher led to a concentration of H₂S in the biogas lower than 150 mg/Nm³ (Figure 5(a)). This rate represents approximately 3.3 times the stoichiometric amount to oxidise both H₂S (gas) and dissolved sulphide to S⁰ in the digester. So, employing such a ratio O₂ supply can be optimised to achieve a removal higher than 97% with a minimal O₂ amount unemployed for the removal.

Furthermore, a statistical analysis was performed to correlate the H₂S concentration and the ratio NLO₂/Nm³ biogas for a ratio equal to or lower than 6.4. This data proved to follow a normal distribution ($R = 0.94$) and a linear regression ($R^2 = 0.88$) showed moderate linear behaviour during the experiment.

For experiment 2, a ratio of 118 NLO₂/Nm³ biogas or higher resulted in a concentration of H₂S lower than 150 mg/Nm³ (Figure 5(b)); this represents 6.5 times the stoichiometric amount to oxidise H₂S to S⁰. A removal higher than 99% was achieved when this ratio or higher was achieved. Comparing this optimal rate with the one from experiment 1, a concentration of H₂S around 10 times higher required a ratio of NLO₂/Nm³ around 20 times higher. This is the result of the higher dissolved sulfide concentration in equilibrium with the biogas in the biodigester, which was also removed by microoxygenation, and the higher production of S₂O₃²⁻ in experiment 2.

The statistical analysis of the data was performed in this case only for the points where pseudo-stationary conditions were achieved for rates equal to or lower than 118 NLO₂/Nm³ biogas, owing to the fact that transition states

when O₂ rate was raised from stage to stage were longer for this experiment (see Figure 2(b)). The data were shown to follow a normal distribution ($R = 0.96$) and a strong linear behaviour ($R^2 = 0.90$).

CONCLUSIONS

The microaerobic treatment showed to effectively remove H₂S from the biogas in a wide range of the H₂S concentrations found on AD. To achieve the target, O₂ rate can be optimised to achieve low O₂ concentrations in the biogas, around 0.1% (v/v) for low H₂S anaerobic concentrations, while eliminating H₂S and controlling the final product of the H₂S oxidation. In this sense, S⁰ was the main product during the treatment; however, when a higher amount of H₂S was present in anaerobic conditions, a small fraction of S₂O₃²⁻ was found for the optimal rate. Finally, the ratio O₂ rate/biogas production rate was found an adequate parameter to control the O₂ dose to the digester.

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REFERENCES

- Abatzoglou, N. & Boivin, S. 2009 *A review of biogas purification processes*. *Biofuels Bioproducts and Biorefining–Biofpr* 3 (1), 42–71.
- Clesceri, L. S., Greenberg, A. E. & Eaton, A. D. 1998 *Standard Methods for the Examination of Water and Wastewater*, 20th ed., American Public Health Association, Washington, DC.

- Deublein, D. & Steinhauser, A. 2008 *Biogas from Waste and Renewable Resources: An Introduction*. Wiley-VCH, Weinheim.
- Díaz, I., Lopes, A. C., Pérez, S. I. & Fdz-Polanco, M. 2010a Performance evaluation of oxygen, air and nitrate for the microaerobic removal of hydrogen sulphide in biogas from sludge digestion. *Bioresource Technology* **101** (10), 7724–7730.
- Díaz, I., Lopes, A. C., Pérez, S. I. & Fdz-Polanco, M. 2010b Effect of oxygen dosing point and mixing on the microaerobic removal of hydrogen sulphide in sludge digesters. *Bioresource Technology* **102** (4), 3768–3775.
- Fdz-Polanco, M., Díaz, I., Pérez, S. I., Lopes, A. C. & Fdz-Polanco, F. 2009 Hydrogen sulphide removal in the anaerobic digestion of sludge by microaerobic processes: pilot plant experience. *Water Science and Technology* **60** (12), 3045–3050.
- Janssen, A. J. H., Sleyster, R., Kaa, C. v. d., Jochemsen, A., Bontsema, J. & Lettinga, G. 1995 Biological sulphide oxidation in a fed-batch reactor. *Biotechnology and Bioengineering* **47** (3), 327–333.
- Janssen, A. J. H., Ruitenbergh, R. & Buisman, C. J. N. 2001 Industrial applications of new sulphur biotechnology. *Water Science and Technology* **44** (8), 85–90.
- Jenicek, P., Keclik, F., Maca, J. & Bindzar, J. 2008 Use of microaerobic conditions for the improvement of anaerobic digestion of solid wastes. *Water Science and Technology* **58** (7), 1491–1496.
- Jenicek, P., Koubova, J., Bindzar, J. & Zabranska, J. 2010 Advantages of anaerobic digestion of sludge in microaerobic conditions. *Water Science and Technology* **62** (2), 427–434.
- Khanal, S. K. & Huang, J.-C. 2003 ORP-based oxygenation for sulfide control in anaerobic treatment of high-sulfate wastewater. *Water Research* **37** (9), 2053–2062.
- Lens, P. N. L. & Pol, L. W. H. 2000 *Environmental Technologies to Treat Sulphur Pollution. Principles and Engineering*, 1st ed., IWA Publishing, London.
- Syed, M., Soreanu, G., Faletta, P. & Béland, M. 2006 Removal of hydrogen sulphide from gas streams using biological processes-A review. *Canadian Biosystems Engineering* **48**, 2.1–2.14.
- Tang, K., Baskaran, V. & Nemat, M. 2009 Bacteria of the sulphur cycle: An overview of microbiology, biokinetics and their role in petroleum and mining industries. *Biochemical Engineering Journal* **44** (1), 73–94.
- van der Zee, F. P., Villaverde, S., García, P. A. & Fdz-Polanco, F. 2007 Sulfide removal by moderate oxygenation of anaerobic sludge environments. *Bioresource Technology* **98** (3), 518–524.
- Weiland, P. 2010 Biogas production: current state and perspectives. *Applied Microbiology and Biotechnology* **85** (4), 849–860.

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