

DISCUSSION

In a similar way, if $\Delta > 0$, $[\Gamma] \Rightarrow [C]$. Analogous results can also be obtained for cases of perfect plasticity ($\Delta = 0$) and strain softening ($\Delta < 0$) [8] – provided the stress-space formulations are properly framed. This is what the authors mean by the word *equivalent*.

We apologize if the use of this word has proved misleading to some readers of the subject paper. The main point to be stressed is that in designing a computational algorithm for plasticity, one is at liberty to work from either the stress or strain-space version, whichever is more convenient, since the two approaches can, with certain restrictions, be made to yield the same physical behavior. The computational experience reported in [2] and [8] lends additional support to the interchangeability of these two formulations.

References

- 1 Yoder, P. J., and Iwan, W. D., "On Formulation of Strain-Space Plasticity With Multiple Loading Surfaces," *ASME JOURNAL OF APPLIED MECHANICS*, Vol. 48, 1981, pp. 773-778.
- 2 Yoder, P. J., and Iwan, W. D., "Computational Aspects of Strain Space Plasticity," accepted for publication in *ASCE J. Engineering Mechanics Div.*
- 3 McMeeking, R. M., and Rice, J. R., "Finite Element Formulation for Problems of Large Elastic-Plastic Deformation," *Int. J. Solids Structures*, Vol. 11, 1975, pp. 601-616.
- 4 Hughes, T. J. R., and Winget, J., "Finite Rotation Effects in Numerical Integration of Rate Constitutive Equations Arising in Large-Deformation Analysis," *Int. J. Numerical Methods in Engineering*, Vol. 15, 1980, pp. 1862-1867.
- 5 Naghdi, P. M., and Trapp, J. A., "The Significance of Formulating Plasticity Theory With Reference to Loading Surfaces in Strain Space," *Int. J. Eng. Sci.*, Vol. 13, 1975, pp. 785-797.
- 6 Naghdi, P. M., "Some Constitutive Restrictions in Plasticity," *Proc. Symp. on Constitutive Equations in Viscoplasticity: Computational and Engineering Aspects*, AMD Vol. 20, 1976, pp. 79-93.
- 7 Casey, J., and Naghdi, P. M., "On the Characterization of Strain-Hardening in Plasticity," *ASME JOURNAL OF APPLIED MECHANICS*, Vol. 48, 1981, pp. 285-296.
- 8 Yoder, P. J., "A Strain-Space Plasticity Theory and Numerical Implementation," Ph.D. Thesis, California Institute of Technology, 1981.

[The Annular Membrane Under Axial Load¹

Robert Schmidt.² Let us introduce auxiliary notations x , y , z , and p defined by

$$r^2 x = r^2, \quad 4Dy = r^2 N_r, \quad (1a,b)$$

$$2^{3/2} tz = [3(1 - \nu^2)]^{1/2} r\beta, \quad (1c)$$

$$2^{5/2} \pi E t^4 p = [3(1 - \nu^2)]^{3/2} r^2 P, \quad (1d)$$

where $D = Et^3/12(1 - \nu^2)$, and the remaining symbols have the meaning assigned to them in the Note under discussion. With these notations, the nonlinear differential equations [1] governing moderately large axisymmetric deflections of circular plates become [2, 3]

$$x^2 y'' = -z^2, \quad x^2 z'' = yz + px, \quad (2a,b)$$

where primes denote derivatives with respect to x .

For a membrane, the foregoing equations reduce to

$$x^2 y'' = -z^2, \quad yz = -px, \quad (3a,b)$$

and finally to Schwerin's form [4]

$$y^2 y'' = -p^2, \quad (4)$$

which possesses closed-form general implicit and special explicit solutions [4, 5], both of which were published by Schwerin in 1929 [4].³ Needless to say, Schwerin was rather proud of his discovery, which doubled the number of known closed-form solutions in the theory of slack membranes from one to two. The authors of the present Note have simply rediscovered Schwerin's special solution, which is valid for $\nu = 1/3$.

Much later, closed-form solutions, similar to Schwerin's, were obtained by Jahsman, Field, and Holmes [5] for a prestretched axisymmetrical membrane, and by E. Reissner for a spherical membrane.

References

- 1 Timoshenko, S., and Woinowsky-Krieger, S., *Theory of Plates and Shells*, 2nd ed., McGraw-Hill, New York, 1959.
- 2 Schmidt, R., "Large Deflections of a Clamped Circular Plate," *Journal of the Engineering Mechanics Division, Proc. ASCE*, Vol. 94, No. EM6, Dec. 1968, pp. 1603-1606.
- 3 Schmidt, R., "Finite Deflections of a Circular Plate Sealing an Incompressible Liquid," *ASME JOURNAL OF APPLIED MECHANICS*, Vol. 43, No. 4, Dec. 1976, pp. 694-695.
- 4 Schwerin, E., "Ueber Spannungen und Formaenderungen kreisringfoermiger Membranen," *Zeitschrift fuer technische Physik*, Vol. 10, No. 12, 1929, pp. 651-659.
- 5 Jahsman, W. E., Field, F. A., and Holmes, A. M. C., "Finite Deformations in a Prestressed, Centrally Loaded, Circular Elastic Membrane," *Proceedings of the Fourth U. S. National Congress of Applied Mechanics*, Vol. 1, 1962, pp. 585-594.

³ It should be noted that equation (4) is analogous to the differential equation $r^2 \ddot{r} = \text{const.}$, describing the free fall of two spherical bodies toward each other.

[The Annular Membrane Under Axial Load¹

C. W. Bert.² The authors are to be congratulated for obtaining a closed-form solution for a nonlinear problem which has not been solved previously in the context of the Föppl theory [1] used. The limitations of the Föppl theory have been discussed by Junkin and Davis [2] in comparison with an exact membrane theory obtained from Budiansky's shell equations [3]. In reference [2], it was shown that Föppl's theory is valid only when the ratio of the deflection to the outside radius is small compared to unity. Nevertheless, using order-of-magnitude considerations, reference [2] obtained, for $\nu = 1/3$, a closed-form solution equivalent to that obtained by the authors.

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Even in the context of the Föppl theory, the second of equations (2), is not quite correct, since it involves an extra derivative with respect to radius. The correct equation is

$$r \frac{d}{dr} \left[\frac{1}{r} \frac{d}{dr} \left(r \frac{d\Phi}{dr} \right) \right] + \frac{1}{2} Et \left(\frac{dw}{dr} \right)^2 = 0 \quad (1)$$

Then equation (6) becomes

$$c\beta^2(\beta-2)r^{\beta-2} + \frac{1}{2} Et k^2 \alpha^2 r^{2\alpha-2} = 0 \quad (2)$$

Fortunately, the solution obtained by the authors, as manifested in their equations (3), (4), and (7), satisfies the preceding corrected equations and thus is still correct.

The lower order in equation (1) follows directly from the appropriate compatibility equation for this problem:

$$\frac{d}{dr} (r\epsilon_\theta) - \epsilon_r = -\frac{1}{2} \left(\frac{dw}{dr} \right)^2 \quad (3)$$

since the strain-displacement relations are:

$$\epsilon_r = \frac{du}{dr} + \frac{1}{2} \left(\frac{dw}{dr} \right)^2; \quad \epsilon_\theta = u/r \quad (4)$$

To compare results with an existing numerical solution [4] (not based on Föppl's theory), the authors' equations can be cast in the following dimensionless form

$$w_{\max}/r_2 = (6f)^{1/3} (1 - \rho^{2/3}) \quad (5)$$

$$(\sigma_r)_{\max}/E = (9/16)^{1/3} f^{2/3} \rho^{-2/3} \quad (6)$$

where $\rho = r_1/r_2$, $f = P/2\pi Etr_2$. It is interesting to note that although Lidin's analysis [4] is not based on Föppl's theory, Lidin obtained the same form of the variation of w_{\max}/r_2 and $(\sigma_r)_{\max}/E$ with f as in equations (5) and (6). However, there is some difference between the respective dependencies on ρ , as can be seen in the following tabulation:

Radius ratio ρ	Values of $w_{\max}/r_2 f^{1/3}$		Values of $(\delta_r)_{\max}/E f^{2/3}$	
	Allman & Mansfield	[4]	Allman & Mansfield	[4]
0.1	1.426	1.239	3.832	3.906
0.3	1.003	0.9042	1.842	1.735
0.5	0.6724	0.6849	1.310	1.201
0.7	0.3846	0.4287	1.047	0.8697
0.9	0.1233	0.2394	0.8856	0.5420

It is noted that Lidin's result is purportedly valid for any Poisson's ratio, yet it is independent of Poisson's ratio, which seems unusual from a physical viewpoint.

References

- 1 Föppl, A., *Vorlesungen über Technische Mechanik*, Vol. 5, B. G. Teubner Leipzig, 1907, p. 132.
- 2 Junkin, G. II, and Davis, R. T., "General Non-Linear Plate Theory Applied to a Circular Plate with Large Deflections," *Int. J. Non-Lin. Mech.*, Vol. 7, 1972, pp. 503-526.
- 3 Budiansky, B., "Notes on Nonlinear Shell Theory," *ASME JOURNAL OF APPLIED MECHANICS*, Vol. 35, 1968, pp. 393-401.
- 4 Lidin, L., "Circular Elastic Membrane Loaded at Concentric Circle," *AIAA Journal*, Vol. 13, 1975, pp. 1242-1245.

Author's Closure

The authors are pleased to note the interest shown in their paper by Professor Bert and they are indebted to him for the valuable comparison of results with earlier work.

In response to his discussion, however, it must be restated here that the second of equations (2) is the correct Föppl equation (which is of fourth order) for the annular membrane under axial load. The third-order equation derived from first principles by Professor Bert is recognized as the first integral of the Föppl equation with the constant of integration zero, as is necessary for a solution of equation (6) to be obtained.

A subsequent paper [1] by the first author, which uses a variational formulation of Föppl's theory to obtain approximate solutions for the annular membrane under axial load, will also be published soon. Numerical results are presented there for a range of values of Poisson's ratio including the value of one-third considered in the present work.

References

- 1 Allman, D. J., "Variational Solutions for the Nonlinear Deflexion of an Annular Membrane Under Axial Load," to be published in *International Journal of Mechanical Sciences*.