

# Evaluation of the FAO Penman–Monteith, Priestley–Taylor and Hargreaves models for estimating reference evapotranspiration in southern Malawi

Cosmo Ngongondo, Chong-Yu Xu, Lena M. Tallaksen and Berhanu Alemaw

## ABSTRACT

This study evaluated the performance of the Food and Agriculture Organization (FAO) Penman–Monteith (PM) reference evapotranspiration ( $ET_0$ ) method for various limited data scenarios in southern Malawi. The study further evaluated the full data PM method against the radiation-based Priestley–Taylor (PT) and the temperature-based Hargreaves (HAG) methods, which are less data-intensive approaches commonly used to estimate  $ET_0$  in data-scarce situations. A comprehensive daily climate dataset observed at the Nchalo Sugar Estate in southern Malawi for the period 1971–2007 was the basis of the study. The results suggested that lack of data on wind speed and actual vapour pressure did not significantly affect the PM  $ET_0$  estimates. However, the estimation of radiation using various combinations of observed wind speed and relative humidity all resulted in significant deviations from the PM  $ET_0$ . Further, the HAG and PT methods significantly underestimated the PM. However, the PM method computed with estimated climate variables instead of observed climate variables still outperformed both the PT and HAG methods if their original parameters and estimated radiation were used. Thus, new monthly parameters for the PT and the HAG methods are proposed for more accurate daily  $ET_0$  estimates.

**Key words** | FAO Penman–Monteith, Hargreaves, Malawi, Priestley–Taylor, reference evapotranspiration

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## INTRODUCTION

Actual evapotranspiration (ET), the combined process of soil water evaporation, interception loss and transpiration (Trajkovic 2010), plays a significant role in the global water balance and in the energy balance at the Earth's surface (Tateishi & Ahn 1996; Chen *et al.* 2005). ET is also central in long-term water resources planning and management, as it is a consumptive water use that cannot be recovered (Committee on Opportunities in the Hydrologic Sciences 1991). Global estimates indicate that up to 64% of the land-based average annual total precipitation of 750 mm is returned to the atmosphere as evaporation (Fisher *et al.* 2005; Sumner & Jacobs 2005). However, ET is among the most difficult parts of the hydrological cycle to quantify due

to the complex interaction between the land surface, vegetation and atmosphere (Xu & Singh 2005; Fang *et al.* 2012).

ET can be directly estimated using hydrological approaches (e.g. soil water balance, weighing lysimeters), micro-meteorological methods (e.g. energy balance and Bowen's ratio, aerodynamic and eddy correlation method) and plant physiological approaches (e.g. sap flow and chambers system methods) (Rana & Katerji 2000). Due to complexities in the direct quantification of ET, the potential evaporation ( $ET_p$ ) provides the theoretical basis for the estimation of ET (Xu & Chen 2005; Xu & Singh 2005; Gong *et al.* 2006; Xu *et al.* 2006).  $ET_p$  can be defined as the maximum amount of water capable of

being lost as water vapour, either by evaporation or transpiration, in a given time by actively growing vegetation completely shading the ground, of uniform height and with adequate water in the soil profile (Chattopadhyay & Hulme 1997). The influence of surface types in  $ET_p$  is removed by using the concept of reference evapotranspiration ( $ET_0$ ), which is defined as the rate of ET from a hypothetical reference crop with an assumed crop height of 0.12 m, a fixed surface resistance of  $70 \text{ s m}^{-1}$  and an albedo of 0.23, closely resembling the ET from an extensive surface of green grass of uniform height, actively growing, well watered and completely shading the ground (Allen *et al.* 1998).  $ET_0$  expresses the evaporative demand of the atmosphere for a grass reference evapotranspiring surface with abundant water supply and can therefore be estimated from meteorological data alone (Xu *et al.* 2006; Sentelhas *et al.* 2010).

There exists a variety of models for estimating  $ET_0$  that are classified based on the climate input needed (Singh & Xu 1997a, b; Xu & Singh 2000, 2001, 2002). These include: mass-transfer-based methods (e.g. Dalton 1802; Thornthwaite & Holzman 1939; Kuzmin 1957); temperature-based approaches (e.g. Thornthwaite 1944; Blaney & Criddle 1950; Hargreaves 1975); radiation-based methods (e.g. Makkink 1957; Priestley & Taylor 1972); and combination methods based on the mass transfer principle and the energy balance (e.g. Penman 1948) and Food and Agriculture Organization (FAO) Penman–Monteith, or PM (Allen *et al.* 1998).

Among the various  $ET_0$  estimation methods, the PM method by Allen *et al.* (1998) was adopted in this study as the standard reference tool. The method has been evaluated for a wide range of climatic conditions and found to be more comparable to lysimeter measurements than other methods (Jensen *et al.* 1990; Allen *et al.* 1998; Ventura *et al.* 1999; Pereira & Pruitt 2004; Gavilán *et al.* 2006; Lopez-Urrea *et al.* 2006; Benli *et al.* 2010). The PM method is a physically based approach incorporating physiological and aerodynamic parameters that can be used globally without much need for additional adjustments of parameters (Allen *et al.* 1998; Sentelhas *et al.* 2010). Input data required include observed air temperature, relative humidity, solar radiation and wind speed. Apart from air temperature readings, the other climatic variables are

not commonly measured at many climate stations, even in developed countries (Gavilán *et al.* 2006). Consequently, the PM method has had limited application in many developing countries where infrastructure and equipment that directly measure  $ET_0$  or ET are almost non-existent. As a result, there is a limited understanding of the role of ET in data-scarce regions, despite it being a key water balance component. There is therefore a need in such regions for evaluating the performance of alternative approaches that only require readily available meteorological variables. Furthermore, the PM method as outlined in Allen *et al.* (1998) provides procedures for estimating  $ET_0$  with missing climate data. Such procedures, however, require the assessment of their accuracy in various climates, as addressed by numerous studies (e.g. Xu & Singh 2002; Popova *et al.* 2006; Gavilán *et al.* 2006; Jabloun & Sahli 2008; Sentelhas *et al.* 2010; Azhar & Perera 2011).

Malawi, located in south-eastern Africa, has a predominantly agro-based economy. Accurate quantification of ET is therefore critical for the better management of water resources and agricultural production in the country. The country experiences a wide range of climatic differences due to the combined influence of water bodies and different altitude. Such contrasting settings require a comprehensive understanding of the spatial and temporal variability in ET for water resources management.

Literature on  $ET_0$  studies in Malawi is very scarce. Wang *et al.* (2009) recently evaluated the applicability of the PM method at a monthly scale for various sets of missing data at five climate stations in Malawi. The study found that particular missing data on wind speed and relative humidity in high wind speed areas affected the calculated  $ET_0$ . Other previous ET-related studies as presented by Mandeville & Bachelor (1990) include: Pike (1961), who estimated monthly free water evaporation using the Penman formula at 23 stations during 1952–1961; World Meteorological Organization (WMO 1976), which estimated the average annual evaporation from Lake Malawi from a relationship between the Lake Chilwa water balance and adjacent evaporation pans; van der Velden (1979), who analysed pan measurements at 38 stations in Malawi and found the highest evaporation rates in

low-lying areas along Lake Malawi and in the lower Shire River valley; Dandaula (1979), who found approximately equal estimates of open water evaporation and  $ET_p$  using the Penman method at 19 stations for the period 1972–1979 (obtaining different open water evaporation estimates from Pike (1961)); and Mandeville & Bachelor (1990), who assessed the applicability of the catchment water balance, Thornthwaite's method, Penman method and three complimentary relationship-based approaches in estimating ET, and recommended the catchment water balance as a yardstick. However, these previous studies applied input-data-demanding models (e.g. Penman method by Dandaula (1979)), which are not observed in many stations.

The aim of this study was to evaluate the performance of methods for estimating  $ET_0$  in southern Malawi, a sparsely gauged area with limited stations observing meteorological data of acceptable quality for a useful length of time. As ET is a significant process in the water balance of this hot and low-rainfall region of Malawi, a more accurate estimation of  $ET_0$  is clearly much needed.

## MATERIALS AND METHODS

### Study region

The study area is located in southern Malawi in south-eastern Africa (Figure 1). Malawi has a total area of 118,484 km<sup>2</sup>, of which 94,080 km<sup>2</sup> is land and 24,404 km<sup>2</sup> is occupied by lakes and rivers. The topography is dominated by the Great Rift valley from north to south of the country which contains Lake Malawi. The landscape around the valley consists of large plateau at an elevation of around 800–1,200 m above sea level (a.s.l.), but with peaks as high as 3,000 m a.s.l. The climate is mild tropical with an austral summer rainy season between November and April and a dry winter season between May and October. Rainfall depends on the position of the Inter-Tropical Convergence Zone (ITCZ) and varies in its timing and intensity from year to year.

Countrywide rainfall varies from 725 mm in the low-lying rift valley to 2,500 mm in the highlands (Ngongondo *et al.* 2011). Temperatures are also controlled by the

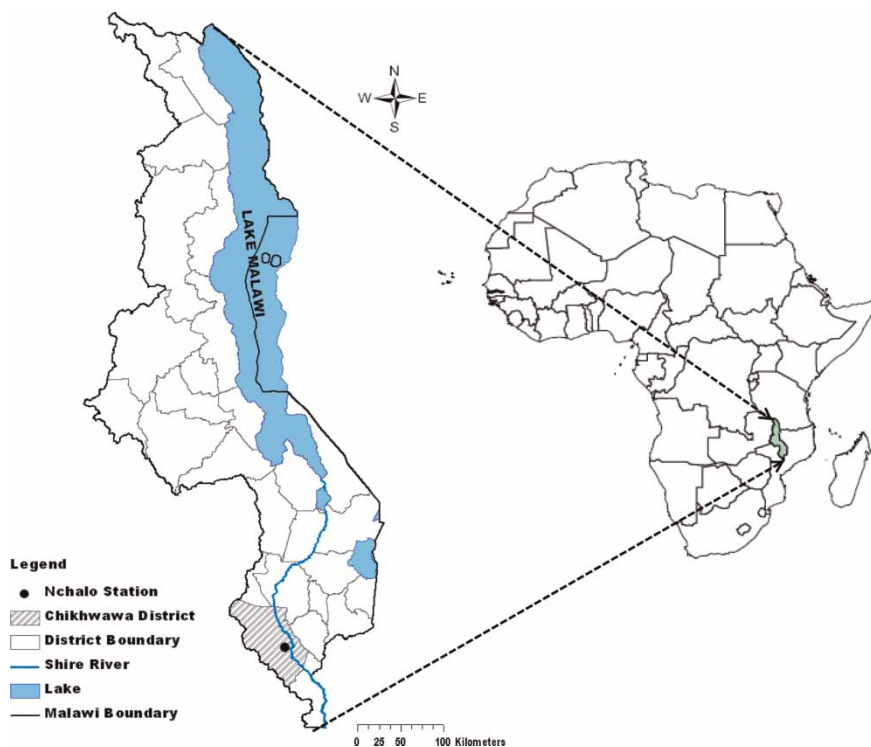


Figure 1 | Map of Malawi showing the location of the Nchalo Sugar Estate Station in Chikhwawa District.

varying altitude and fall within the range 22–27 °C in the summer months. Day temperatures drop to around 18 °C, whereas night temperatures can be as low as 5 °C in the winter months from May to August (Jury & Mwafulirwa 2002). According to Mandeville & Bachelor (1990), average annual runoff expressed as a percentage of the average annual rainfall varies from 4% in the drier parts of plateau areas to 54% in the highlands, where most streams are perennial. Pan evaporation measurements from 38 stations countrywide for the period 1971–1978 showed a mean annual range of 1,500–2,000 mm in the plateau areas, 2,000–2,500 mm along the Lake Malawi shore and the Shire River valley and below 1,500 mm in the cooler high-rainfall areas (van der Velden 1979).

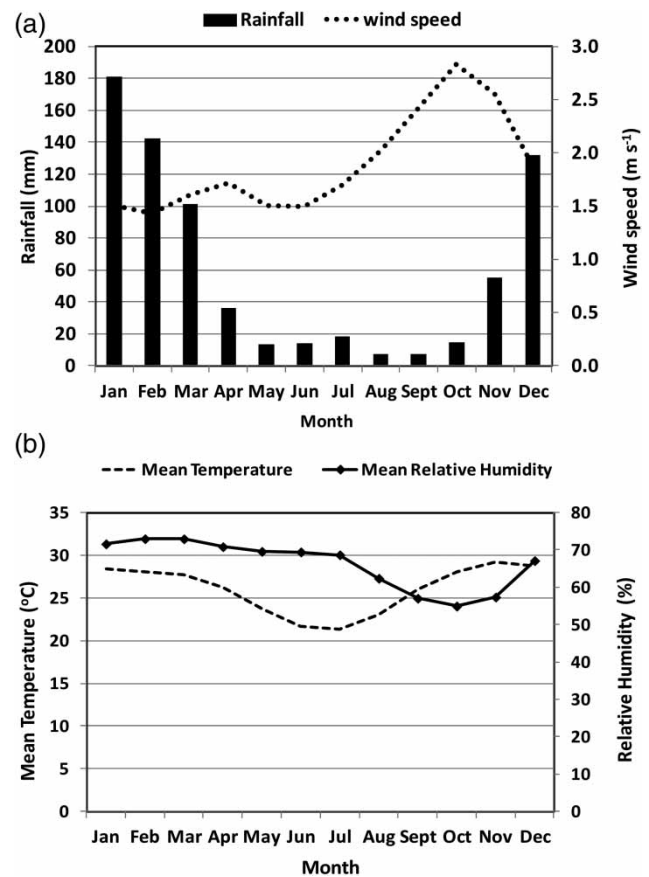
### Data availability

The study used observed daily weather data of maximum and minimum temperature (°C), relative humidity (%), wind speed ( $\text{m s}^{-1}$ ), incoming shortwave solar radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ ) and rainfall (mm) from the Nchalo Illovo Sugar Estate Station for the period 1971–2007. The data were sourced from the Malawi Department of Climate Change and Meteorological Services and Illovo Sugar Company's Nchalo Estate in Chikhwawa District. The station received a mean annual rainfall of 722 mm during this period. Table 1 presents some daily mean values of the climate variables used in computing  $\text{ET}_0$  for the station. The monthly mean variation of rainfall, wind speed, mean temperature and mean relative humidity during the year is shown in Figures 2(a) and 2(b).

The data are of reasonably high quality with missing data accounting for only 0.038% (or 5 days) during the

**Table 1** | Daily mean values of climate variables at the Nchalo Station (1971–2007), altitude 64 m a.s.l., 16.27°S, 34.92°E

$T_{\min}$ (°C)	20.00
$T_{\max}$ (°C)	32.04
$R_s$ ( $\text{MJ m}^{-2} \text{d}^{-1}$ )	21.90
$u_2$ ( $\text{m s}^{-1}$ )	1.89
$\text{RH}_{\max}$ (%)	81.08
$\text{RH}_{\min}$ (%)	51.32
Sunshine (hours)	8.09



**Figure 2** | Nchalo Station (1971–2007): (a) monthly mean rainfall (mm) and mean daily wind speed ( $\text{m s}^{-1}$ ); and (b) monthly mean temperature (°C) and relative humidity.

entire 36-year period. The data were nevertheless subjected to standard quality control procedures using the AnClim software (Stepaneck 2007). The software allows the completion of gaps in the data using single-station testing procedures due to the lack of nearby stations with a similar record length. The data passed this test and outliers were not detected. Missing data were filled with long-term daily averages for similar dates.

### $\text{ET}_0$ methods

The performances of the PM, Hargreaves (HAG, temperature-based) and Priestley–Taylor (PT, radiation-based) methods were evaluated. Data requirements for a particular model and the available data at the station were the main factors in selecting the alternative methods for comparison. The full data PM method (PM1) was used as a standard

against which the other methods were compared. This is considered to be more accurate, even when the majority of its input data must be estimated (Allen et al. 1998). However, it has a relatively large input data requirement. Finally, the parameters of the PT and HAG methods were locally calibrated against the PM1 method. All computations were performed at daily time steps from which monthly mean daily  $ET_0$  were derived.

### The FAO Penman–Monteith method

The PM method (Allen et al. 1998) derives  $ET_0$  as:

$$ET_0 = \frac{0.0408\Delta(R_n - G) + \gamma \frac{900}{(T + 273)} u_2 (e_s - e_a)}{\Delta + \gamma(1 + 0.34u_2)} \quad (1)$$

where  $ET_0$  is the reference evapotranspiration ( $\text{mm d}^{-1}$ );  $R_n$  is the net radiation at the crop surface ( $\text{MJ m}^{-2} \text{d}^{-1}$ );  $\Delta$  is the slope of the saturation vapour pressure function ( $\text{kPa } ^\circ\text{C}^{-1}$ );  $G$  is the soil heat flux ( $\text{MJ m}^{-2} \text{d}^{-1}$ );  $T$  is the average air temperature ( $^\circ\text{C}$ ) at 2 m height;  $u_2$  is the wind speed ( $\text{m s}^{-1}$ ) at 2 m height;  $e_s$  is the saturation vapour pressure ( $\text{kPa}$ );  $e_a$  is the actual vapour pressure ( $\text{kPa}$ );  $e_s - e_a$  is the saturation vapour pressure deficit ( $\text{kPa}$ ); and  $\gamma$  is the psychrometric constant ( $0.0677 \text{ kPa } ^\circ\text{C}^{-1}$ ).  $G$  is considered negligible for computations at daily or lower timescales and was set equal to zero.  $u_2$  was set equal to the global average estimate of  $2 \text{ m s}^{-1}$  in some of the computations.  $R_n$  was estimated following Allen et al. (1998):

$$R_n = R_{\text{ns}} - R_{\text{nl}} \quad (2)$$

$$R_{\text{nl}} = \sigma(T_{\text{max}K}^4 + T_{\text{min}K}^4)(0.034 - 0.14\sqrt{e_a}) \times \left(1.35 \frac{R_{\text{SR}}}{R_{\text{SO}}} - 0.35\right) \quad (3)$$

$$R_{\text{SO}} = (0.75 + 210^{-5}z)R_a \quad (4)$$

$$R_{\text{ns}} = 0.77_{\text{SR}} \quad (5)$$

where  $R_{\text{ns}}$  is the net solar radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ );  $R_{\text{nl}}$  is the net outgoing longwave radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ );  $\sigma$  is the

Stefan–Boltzmann constant ( $4.903 \times 10^{-9} \text{ MJ K}^{-4} \text{ m}^{-2} \text{d}^{-1}$ );  $T_{\text{max}K}$  and  $T_{\text{min}K}$  are the maximum and minimum temperatures in degrees Kelvin, respectively;  $R_{\text{SR}}$  is the observed solar shortwave radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ ); and  $R_{\text{SO}}$  is the clear sky radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ ) at altitude  $z$  above sea level (m).  $R_a$  is the extraterrestrial radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ ) estimated using the procedures in Allen et al. (1998):

$$R_a = \frac{24(60)}{\pi} G_{\text{sc}} d_r [\omega_s \sin(\phi) \sin(\delta) + \cos(\phi) \sin(\delta) \sin(\omega_s)] \quad (6)$$

where  $G_{\text{sc}} = 0.0820 \text{ MJ m}^{-2} \text{min}^{-1}$  is the solar constant,

$$\omega_s(\text{rad}) = \arccos[-\tan(\phi) \tan(\delta)]$$

is the sunset angle at latitude  $\phi$  (rad),

$$d_r(\text{rad}) = 1 + 0.033 \cos\left(\frac{2\pi J}{365} - 1.39\right)$$

is the inverse relative Earth–Sun distance and

$$\delta(\text{rad}) = 1 + 0.409 \sin\left(\frac{2\pi J}{365} - 1.39\right)$$

is the solar declination on a day of the year  $J$  between 1 January and 31 December ( $J = 1, \dots, n$ ;  $n = 365$  or  $366$ ).

$R_{\text{SR}}$  was estimated for cases where it is not observed following Allen et al. (1998):

$$R_{\text{SR}} = K_{\text{RS}} \sqrt{T_{\text{max}} - T_{\text{min}}} R_a \quad (7)$$

where  $R_{\text{SR}}$  is as defined above,  $T_{\text{max}}$  and  $T_{\text{min}}$  are maximum and minimum temperature ( $^\circ\text{C}$ ) and  $K_{\text{RS}}$  is an adjustment coefficient ( $^\circ\text{C}^{-0.5}$ ) that varies from 0.16 for ‘interior’ areas (where the influence of moist air masses are less dominant) to 0.19 (for ‘coastal areas’ where the air masses are strongly influenced by adjacent water bodies). The Nchalo Station is located in a low-lying inland area and the study therefore adopted a  $K_{\text{RS}}$  value of 0.16.

In evaluating the performance of the PM method in data-limited situations, 12 scenarios were considered as shown in Table 2. It was assumed that the most accurate

**Table 2** | Climate variables included in the various scenarios for calculating  $ET_0$  using the PM method, where 'Y' indicates the variable was observed or computed from observations

	PM1	PM2	PM3	PM4	PM5	PM6	PM7	PM8	PM9	PM10	PM11	PM12
$T_{min}$	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
$T_{max}$	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
$T_{dew}$	-	$e_a$ est. from $T_{dew} = T_{min}-3$	-	-	-	$e_a$ est. from $T_{dew} = T_{min}-3$	-	$e_a$ est. from $T_{dew} = T_{min}-3$	-	$e_a$ est. from $T_{dew} = T_{min}-3$	-	$e_a$ est. from $T_{dew} = T_{min}-3$
RH (%)	Y	-	Y	Y	Y	-	Y	-	Y	-	Y	-
$u_2$	Y	Global mean $2 m s^{-1}$	Observed monthly mean	Global mean $2 m s^{-1}$	Observed daily mean	Observed Y	Y	Observed monthly mean	Observed monthly mean	Y	Global mean $2 m s^{-1}$	Global mean $2 m s^{-1}$
$R_{SR}$	Y	Via Allen et al. (1998)	Y	Y	Y	Y	Via Allen et al. (1998)	Via Allen et al. (1998)	Via Allen et al. (1998)	Via Allen et al. (1998)	Via Allen et al. (1998)	Y

$ET_0$  estimates were those derived from PM1. Procedures for estimating the internal variables and other missing weather data are outlined in Equations (2)–(7) following the steps given in Chapter 3 of FAO paper 56 by Allen *et al.* (1998).

### Hargreaves method

The HAG method is a commonly used temperature-based method for estimating  $ET_0$  in areas where meteorological information is scarce. In addition to temperature data which are readily available, the extraterrestrial radiation ( $R_a$ ) required as input variables can be sourced from tables or estimated based on equations for different latitudes and day of the year (Allen *et al.* 1998; Xu & Singh 2009; Igbadun *et al.* 2006).

This study used the HAG  $ET_0$  version by Hargreaves & Samani (1982, 1985), which proposes several improvements to the original equation by Hargreaves (1975).  $ET_0$  is calculated as follows:

$$ET_0 = C_H R_a T_D^{0.5} (T_a + 17.8) \quad (8)$$

where  $C_H = 0.0023$  is the original parameter proposed by Hargreaves & Samani (1982);  $T_D$  is the difference between maximum and minimum daily temperature ( $^{\circ}C$ );  $T_a$  is the mean temperature ( $^{\circ}C$ ); and  $R_a$  is the extraterrestrial radiation expressed in equivalent evaporation units in  $mm d^{-1}$  calculated from Equation (7). The parameter  $C_H$  was also locally calibrated in this study. The HAG model was recommended by Allen *et al.* (1998) as the best alternative to the PM method when only temperature data are available.

### Priestley–Taylor method

This radiation-based method was proposed by Priestley & Taylor (1972) as a simplified version of the combination equation (Penman 1948) for use when surface areas are generally wet.  $ET_0$  is calculated as:

$$ET_0 = \alpha_{PT} \frac{\Delta}{\Delta + \gamma} \frac{R_n}{\lambda} \quad (9)$$

where  $ET_0$  is in  $mm d^{-1}$ ;  $\lambda$  is the latent heat of vapourization ( $2.45 MJ kg^{-1}$ );  $R_n$  is the net radiation in  $MJ m^{-2} d^{-1}$

calculated from Equation (3) and the other terms are as defined in Equation (2). In the PT method, the aerodynamic component in the Penman (1948) equation is removed and instead the energy component is multiplied by a coefficient  $\alpha_{PT} = 1.26$  (Xu & Chen 2005). The coefficient  $\alpha_{PT}$  was also locally calibrated in this study as recommended when applying the PT method at different sites (Castellvi et al. 2001; Xu & Chen 2005; Xu & Singh 2005).  $ET_0$  was estimated using  $R_n$  computed from both observed and estimated  $R_{SR}$  (Equation (7)). The PT method is widely applied due to its acceptable performance in humid regions as well as its limited data requirements (Suleiman & Hoogenboom 2007).

### Evaluation criteria

PM1 was used as the standard for comparison with the various data scenarios and alternative  $ET_0$  estimation methods. The methods were compared using the following indices as performance evaluation criteria: mean bias error (MBE), root mean squared error (RMSE), relative error (RE) and the ratio of the averages of each of the two methods under comparison  $R$  (Xu & Chen 2005; Gavilán et al. 2006):

$$MBE = \frac{\sum_{i=1}^n (y_i - x_i)}{n} \quad (10)$$

$$RMSE = \sqrt{\frac{\sum_{i=1}^n (y_i - x_i)^2}{n}} \quad (11)$$

$$RE = \frac{MBE}{\bar{x}} \times 100 \quad (12)$$

$$R = \frac{\bar{y}_i}{\bar{x}} \quad (13)$$

where  $y_i$  is the estimated  $ET_0$  with mean  $\bar{y}_i$  and  $x_i$  is the PM1  $ET_0$  with mean  $\bar{x}$ . MBE is a measure of under- (over-) prediction for  $MBE > 0$  ( $< 0$ );  $MBE \cong 0$  represents the best estimate. RMSE assesses the model performance based on observed and estimated variables with the best estimates having  $RMSE \cong 0$  (Jacovides & Kontoyiannis 1995). The

best estimates will also have  $R = 1$  and  $MBE = 0$  (or close to these values).

To calibrate each of the alternative models based on their performance against PM1, a linear regression line of the form  $y = bx + a$  was forced through the origin ( $a = 0$ ). The slope  $b$  (the regression coefficient) was used as a factor for adjusting the  $ET_0$  estimates according to PM1, thereby approximating the line with slope  $b = 1$  and  $a = 0$ . The locally calibrated parameters for the HAG and PT methods were obtained by multiplying the slope  $b$  by the original parameters  $C_H$  and  $\alpha_{PT}$ . The period 1971–1997 was used for calibration whereas the performances of the alternative methods with calibrated parameters were tested during 1998–2007. Statistical significance of the two samples was determined using a two tailed  $z$ -test (Haan 2002) for the sample means ( $\bar{x}_1, \bar{x}_2$ ) with known variances ( $\sigma_1^2, \sigma_2^2$ ) under the null hypothesis that the means are not different ( $\bar{x}_1 - \bar{x}_2 = 0$ ) at the significance level  $\alpha = 0.05$ .

## RESULTS AND DISCUSSION

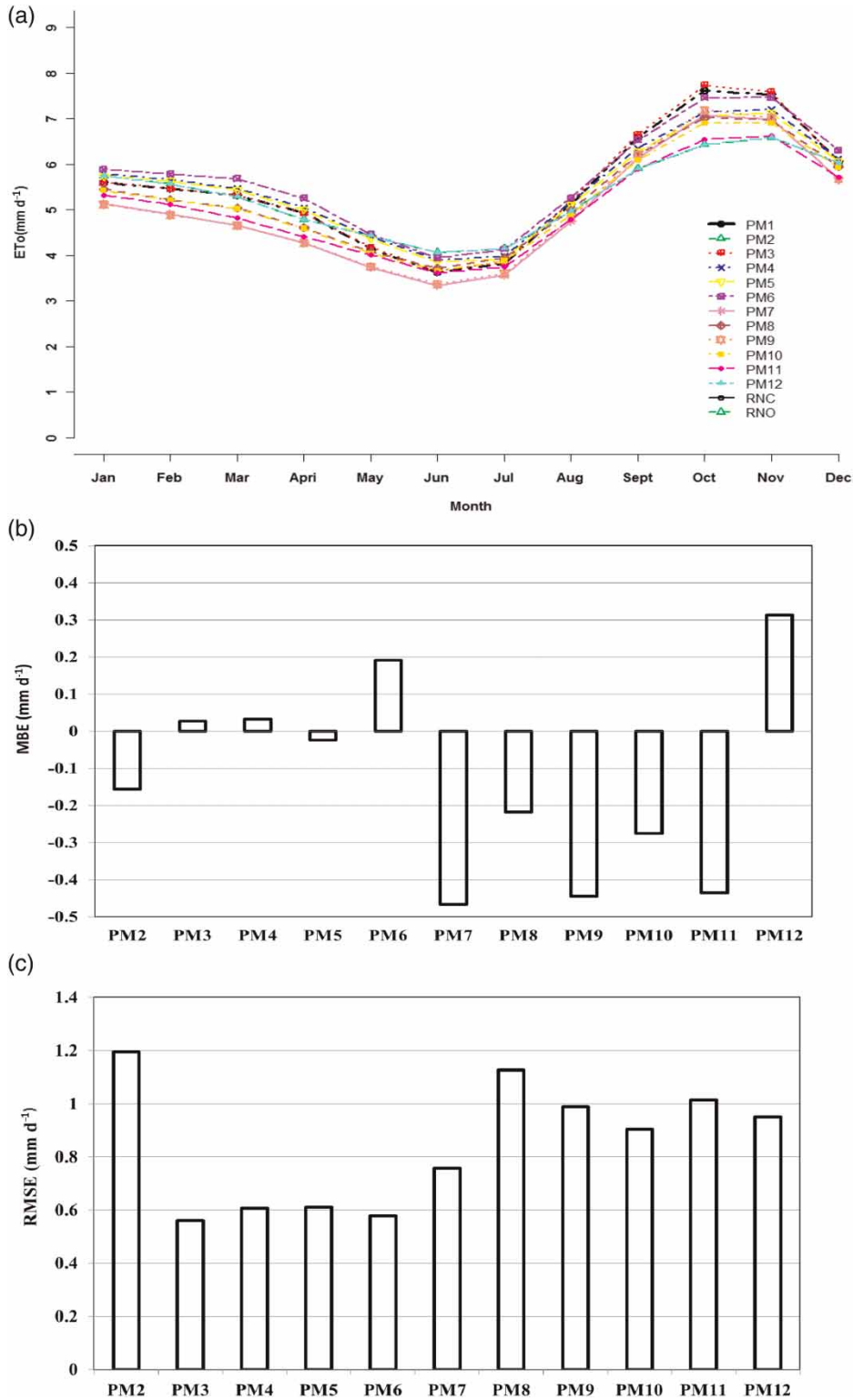
### Performance of the PM method at Nchalo Station

Figure 3(a) shows the seasonal variation of mean monthly  $ET_0$  (expressed in  $\text{mm d}^{-1}$ ) estimated by the 12 data scenarios of the PM method. Figures 3(b) and 3(c) show the RMSE and MBE values for the scenarios. Evaluation of the PM1 method for the various data scenarios at Nchalo Station is presented in Table 3.

### Effect of wind speed $u_2$

Various values of the wind speed  $u_2$  are used in the different data scenarios to compute the PM  $ET_0$  while keeping the other input data constant. PM3 uses the monthly daily mean  $u_2$  (i.e. each month had its mean value for the entire period), whereas PM4 uses the daily mean value for the entire period ( $u_2 = 1.89 \text{ m s}^{-1}$ ) and PM5 uses the global average wind speed from 2,000 stations worldwide ( $u_2 = 2 \text{ m s}^{-1}$ ).

The results shown in Table 3 and Figures 3(b) and 3(c) suggest that the effect of different wind speeds (PM3, PM4 and PM5) on the daily  $ET_0$  was minimal. This is confirmed by their respective low RMSE values (Figure 3(b)) within the



**Figure 3** | (a) Comparison of monthly mean values of the PM method; (b) RMSE for  $ET_0$  estimated by the PM method; and (c) MBE for  $ET_0$  estimated by the PM method for the 12 data scenarios.



**Table 3** | Results of the performance evaluation of the various PM data scenarios against the PM1 method (1971–2007)

Data Scenario	PM1	PM2	PM3	PM4	PM5	PM6	PM7	PM8	PM9	PM10	PM11	PM12
Mean (mm d <sup>-1</sup> )	5.48	5.33	5.51	5.52	5.46	5.67	5.02	5.27	5.04	5.21	5.05	5.80
RE (%)		-2.85	0.50	0.59	-0.45	3.49	-8.50	-3.97	-8.11	-5.01	-7.96	5.70
R		0.97	1.01	1.01	1.00	1.03	0.91	0.96	0.92	0.95	0.92	1.06
Slope <i>b</i>		1.04	0.99	1.00	1.01	0.97	1.09	1.04	1.08	1.06	1.09	0.96
R <sup>2</sup>		0.96	0.99	0.99	0.99	0.99	0.99	0.96	0.98	0.98	0.98	0.98

range 0.56–0.61 mm d<sup>-1</sup>. The MBE values suggest that PM3 and PM4 scenarios slightly overestimated ET<sub>0</sub>, whereas PM5 slightly underestimated it (Figure 3(c) and Table 3). The minor differences were also reflected in high ratio values ( $R \cong 1$ ), slopes ( $b \cong 1$ ) and coefficients of determination ( $R^2 \cong 1$ ). The *z*-tests showed that PM3, PM4 and PM5 were not statistically different from PM1 ( $\alpha = 0.05$ ) in all cases. It is therefore suggested that, in the absence of wind speed data, the PM ET<sub>0</sub> can be estimated satisfactorily using the global average wind speed ( $u_2 = 2 \text{ m s}^{-1}$ ) in the region.

These results agree with other studies in different climatic settings (e.g. Jabloun & Sahli 2008), which have found that wind speed has a relatively small impact on ET<sub>0</sub> with the exception of arid and very windy areas (Martinez-Cob & Tejero-Juste 2004). The PM estimations using the global average wind speed  $u_2 = 2 \text{ m s}^{-1}$  in the studies by Jabloun & Sahli (2008) and Popova *et al.* (2006) also obtained results similar to PM1. From a study in Southern Ontario in Canada, Sentelhas *et al.* (2010) found that using wind speed data from a nearby station yielded PM estimates close to PM1.

### Effect of relative humidity RH (%)

Relative humidity is used to compute the actual vapour pressure ( $e_a$ ), which again is then used to determine the saturated vapour pressure deficit ( $e_s - e_a$ ) in the PM method. When relative humidity data are missing, the actual vapour pressure can be estimated from the dew point temperature ( $T_{\text{dew}}$ ) by setting  $T_{\text{dew}} = T_{\text{min}} - 3$ , where  $T_{\text{min}}$  is the daily minimum temperature (°C) (Allen *et al.* 1998) as in PM6 (Table 2). The performance of PM6 (Table 3 and Figures 3(a)–3(c)) is close to PM1 with  $R^2 = 0.97$ . The RMSE was 0.58 mm d<sup>-1</sup> with the MBE, RE and *R* values

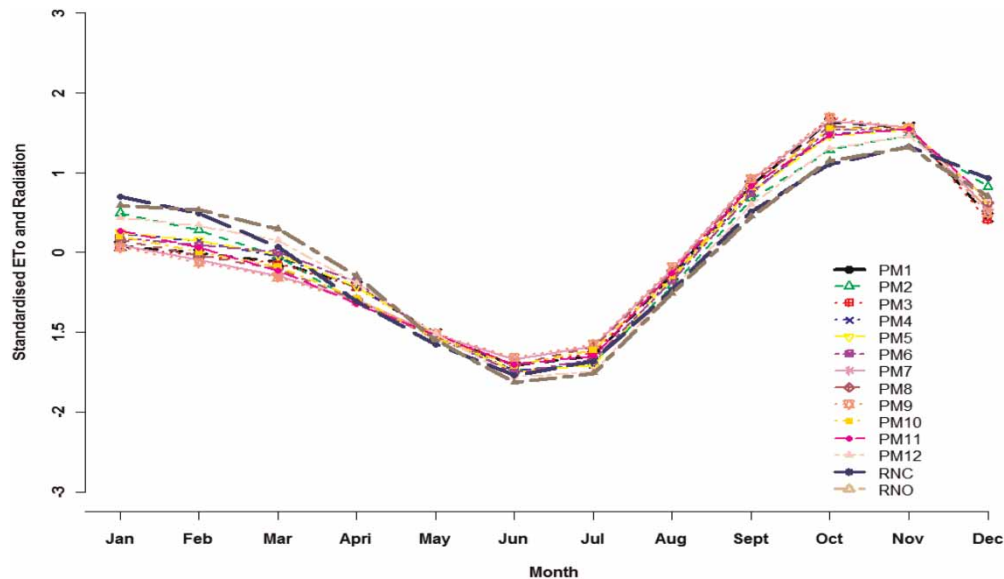
of 0.19 mm d<sup>-1</sup>, 3.49 and 1.03% respectively, suggesting some overestimation. The *z*-test showed that the overestimation was statistically significant at the  $\alpha = 0.05$  level. However, the performance criteria indicate that PM6 is still acceptable and was closer to PM1 compared to those in various studies (e.g. Sentelhas *et al.* 2010).

### Effect of estimated net radiation $R_n$

Net radiation ( $R_n$ ) was computed from both observed and estimated  $R_{\text{SR}}$  as represented by data scenarios PM2, PM7, PM8, PM9, PM10, PM11 and PM12 in Table 2, with various combinations of available or missing wind speed ( $u_2$ ) and vapour pressure deficit ( $e_s - e_a$ ). The results in Table 3 and Figures 3(b) and 3(c) show that the estimated ET<sub>0</sub> has higher RMSE values than in the wind and RH scenarios, ranging from 0.76 mm d<sup>-1</sup> (PM7) to 1.20 mm d<sup>-1</sup> (PM2). The MBE values ranged between -0.47 mm d<sup>-1</sup> (PM7) and 0.31 mm d<sup>-1</sup> (PM12) with slopes ranging from 0.96 to 1.09. All scenarios suggest underestimations, the only exception being PM12. ET<sub>0</sub> estimates from scenarios with estimated  $R_n$  were statistically different from the PM1 ( $\alpha = 0.05$ ). The influence of radiation ( $R_{\text{SR}}$ ) on the annual pattern of ET<sub>0</sub> was further investigated by standardizing the monthly means as follows:

$$x = \frac{y - \bar{y}}{s} \quad (14)$$

where  $x$  is the standardized value of either observed or estimated  $R_{\text{SR}}$  or ET<sub>0</sub>( $y$ ) with mean  $\bar{y}$  and standard deviation  $s$ . Figure 4 presents standardized values of monthly mean ET<sub>0</sub> and  $R_{\text{SR}}$  showing the effect of observed (RNO) and estimated (RNC) net radiation on the PM ET<sub>0</sub>. The monthly daily mean variation pattern for both RNC and RNO in



**Figure 4** | Standardized FAO-PM monthly mean  $ET_0$ , observed RNO and calculated RNC.

Figure 4 agrees well, especially during the dry season from May to October (Figure 4). For most months in the rainy season (November to April), the RNC underestimated the RNO ( $R^2 = 0.97$ , slope  $b = 0.85$ ).

#### Comparison of PM1 with HAG and PT methods

The performance of the daily PM1 and the limited data scenario PM2 were compared with the PT and HAG methods

(Table 4). Since the PM method is accepted as the more precise method, even where all input variables are estimated, PM2 (with temperature as the only observed input) was included for comparison. The evaluation indices MBE, RMSE, RE and  $R$  in Table 4 show that PM2 performed better against PM1 than both the HAG and PT methods. The performance indices also show that the PT2 method, with observed  $R_{SR}$  and the original parameter ( $\alpha = 1.26$ ), produced more accurate estimates than PM1 ( $R^2 = 0.98$ )

**Table 4** | Performance evaluation of the daily PM2, HAG and PT methods against PM1

Method	PM2	HAG	PT1	PT2	HAGCAL	PT1CAL	PT2CAL
For the whole period 1971–2007							
MBE ( $\text{mm d}^{-1}$ )	-0.16	-0.53	-0.75	-0.06			
RMSE ( $\text{mm d}^{-1}$ )	1.20	1.27	1.39	0.88			
RE (%)	-2.85	-9.72	-13.65	-1.07			
$R$	0.97	0.91	0.86	0.99			
$R^2$	0.96	0.96	0.96	0.98			
Slope	1.04	1.11	1.16	1.01			
After calibration 1998–2007							
MBE ( $\text{mm d}^{-1}$ )	-0.20	-0.56	-0.78	-0.08	-0.03	-0.04	-0.07
RMSE ( $\text{mm d}^{-1}$ )	1.58	1.78	2.09	0.97	1.24	1.21	0.78
RE (%)	-3.50	-10.13	-14.18	-1.39	-0.64	-0.71	-1.33
$R$	1.04	1.11	1.16	1.01	1.00	1.00	1.00

as compared to the PM2, PT1 and HAG methods. The method slightly underestimated the PM1  $ET_0$  (by less than 1%) with an RE of only -1.07% and MBE and RMSE values of -0.06 and 0.88 mm d<sup>-1</sup>, respectively. The slope  $b = 1.01$  and the locally calibrated PT parameter for daily  $ET_0$  estimations can then be derived from:

$$\alpha_{PT} = b \times 1.26 = 1.27 \quad (15)$$

The calibrated  $\alpha_{PT}$  is approximately equal to the normal original value. This suggests that if  $R_{SR}$  is observed, the PT method would be a good estimator for PM1. Despite the more accurate estimates there is a need for local calibration of the  $\alpha_{PT}$  parameter even where  $R_{SR}$  is observed, as the  $z$ -test showed that the PT estimates with observed  $R_{SR}$  and the original parameter were statistically different from PM1 ( $\alpha = 0.05$ ).

The PT1 method, with the original parameter  $\alpha = 1.26$  and estimated  $R_{SR}$ , however resulted in an underestimation of the PM by 14% ( $R = 0.86$ ) with an average RE value of -13.65% and relatively high MBE and RMSE values of -0.74 and 1.37 mm d<sup>-1</sup>, respectively. The  $z$ -test confirmed that these values were statistically different from PM1

( $\alpha = 0.05$ ). Berengena & Gavilán (2005) found a similar range of underestimation using the PT in a highly advective semi-arid part of southern Spain. The regression coefficient (slope) was  $b = 1.16$  ( $R^2 = 0.96$ ), from which a locally calibrated  $\alpha_{PT}$  of 1.46 can then be derived for daily  $ET_0$  estimations.

The  $\alpha_{PT}$  coefficient of 1.26 represents minimum advection conditions without edge effects and is suitable for  $ET_0$  conditions without advective effects (Pereira & Villa Nova 1992; Eaton et al. 2001). The value of  $\alpha_{PT}$  also depends on season and location relative to large water bodies (Castellvi et al. 2001). Under strong advective conditions,  $\alpha_{PT}$  can have values up to 1.57 (Chuanyan et al. 2004); in arid and semi-arid areas, Jensen et al. (1990) reported values up to 1.74 and Tabari & Talaei (2011) found values up to 2.14 in Iran. For deep and large lakes, Eaton et al. (2001) reported values up to 2.32 and Viswanadham et al. (1991) reported  $\alpha_{PT}$  values up to 3.12. Our result of an adjusted  $\alpha_{PT}$  of 1.46 (with estimated  $R_{SR}$ ) is therefore typical of rather dry areas. The  $\alpha_{PT}$  parameter showed monthly variations however, as shown in Table 5 (where the monthly performance indices of both PT methods are also presented).

**Table 5** | Monthly statistics of PT against FAO1 for Nchalo Station with calibrated  $\alpha_{PT}$  values

Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
From observed $R_{SR}$												
MBE (mm d <sup>-1</sup> )	0.59	0.62	0.49	-0.17	0.26	0.14	-0.23	-0.40	-0.38	-0.80	0.11	-1.18
RMSE (mm d <sup>-1</sup> )	0.79	0.79	0.69	-0.17	0.07	0.14	0.62	0.83	-0.38	1.31	0.11	2.73
RE (%)	10.41	11.35	9.25	0.58	-0.01	0.94	-5.92	-7.95	-5.78	-10.64	1.51	-15.76
$R$	1.12	1.11	1.32	1.11	1.13	0.62	1.14	0.98	1.04	0.89	1.05	0.49
Slope $b$	0.91	0.90	0.92	0.97	1.00	1.03	1.06	1.08	1.11	1.12	1.07	1.11
$R^2$	0.99	0.99	0.99	0.99	0.99	0.98	0.98	0.98	0.98	0.98	0.98	0.88
$\alpha_{PT}$	1.12	1.11	1.13	1.19	1.23	1.26	1.30	1.33	1.37	1.37	1.32	1.37
From estimated $R_{SR}$												
MBE (mm d <sup>-1</sup> )	-0.12	-0.18	-0.42	-0.17	-1.28	0.14	-0.59	-0.99	-0.99	-1.63	-0.55	-1.32
RMSE (mm d <sup>-1</sup> )	1.18	1.07	1.06	-0.17	1.63	0.14	0.99	1.33	-0.99	2.07	-0.55	1.93
RE (%)	-2.02	-3.34	-7.97	0.58	-14.76	0.94	-15.45	-19.42	-15.13	-21.68	-7.29	-17.62
$R$	1.06	0.97	1.00	0.72	1.11	0.71	0.96	0.69	0.81	0.78	0.84	0.85
Slope $b$	1.03	1.02	1.09	1.19	1.17	1.17	1.18	1.23	1.25	1.27	1.22	1.06
$R^2$	0.96	0.97	0.97	0.97	0.97	0.97	0.96	0.97	0.97	0.97	0.97	0.95
$\alpha_{PT}$	1.30	1.29	1.38	1.50	1.48	1.47	1.49	1.56	1.58	1.61	1.54	1.34

From the monthly values in Table 5, the least accurate estimates in both cases were found in October which had the largest absolute values of MBE, RMSE and RE and  $R$  values. The most accurate estimates were seen in January, which has the lowest absolute values of MBE, RMSE and RE. The adjusted  $\alpha_{PT}$  varied from 1.12 to 1.37 for the observed  $R_{SR}$  estimates and from 1.29 to 1.61 for the estimated  $R_{SR}$ .

Similarly, for the  $ET_0$  computed with the HAG method, it is shown that using the original parameter  $C_H = 0.0023$  resulted in an underestimation of the PM1 by 9% ( $R = 0.91$ ) with  $MBE = -0.53 \text{ mm d}^{-1}$ ,  $RMSE = 1.27 \text{ mm d}^{-1}$  and  $RE = -9.72\%$ . The  $z$ -test confirmed that these values were statistically different from PM1 ( $\alpha = 0.05$ ). Regression coefficient (slope)  $b = 1.11$  implying that, at the daily time-step, the HAG parameter has to be adjusted as:

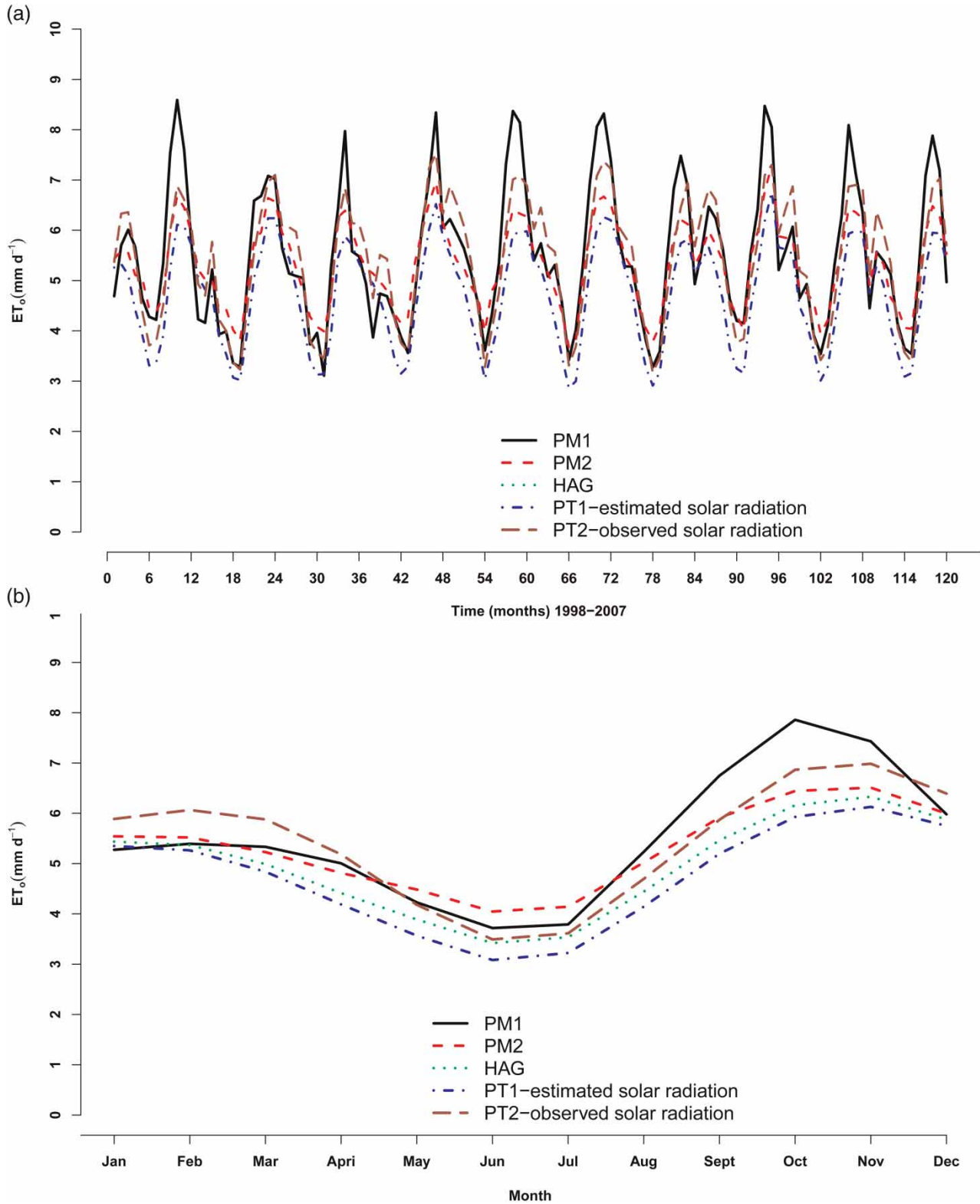
$$C_H = b \times 0.0023 = 0.0026 \quad (16)$$

In contrast to results from this study, the HAG method overestimated PM1 at most of the inland stations in Tunisia used in the study by Jabloun & Sahli (2008). Nchalo Station is located in an area that is dry and hot for most of the year, and the HAG method is known to underestimate  $ET_0$  in such conditions (Xu & Singh 2002). Table 6 shows the monthly performance statistics of the HAG method using a calibrated  $C_H$  for each month. Similar to the PT method, October was found to have the highest values of MBE and RMSE indicating less accuracy in the month. The calibrated  $C_H$  lies within the range 0.0023–0.0028.

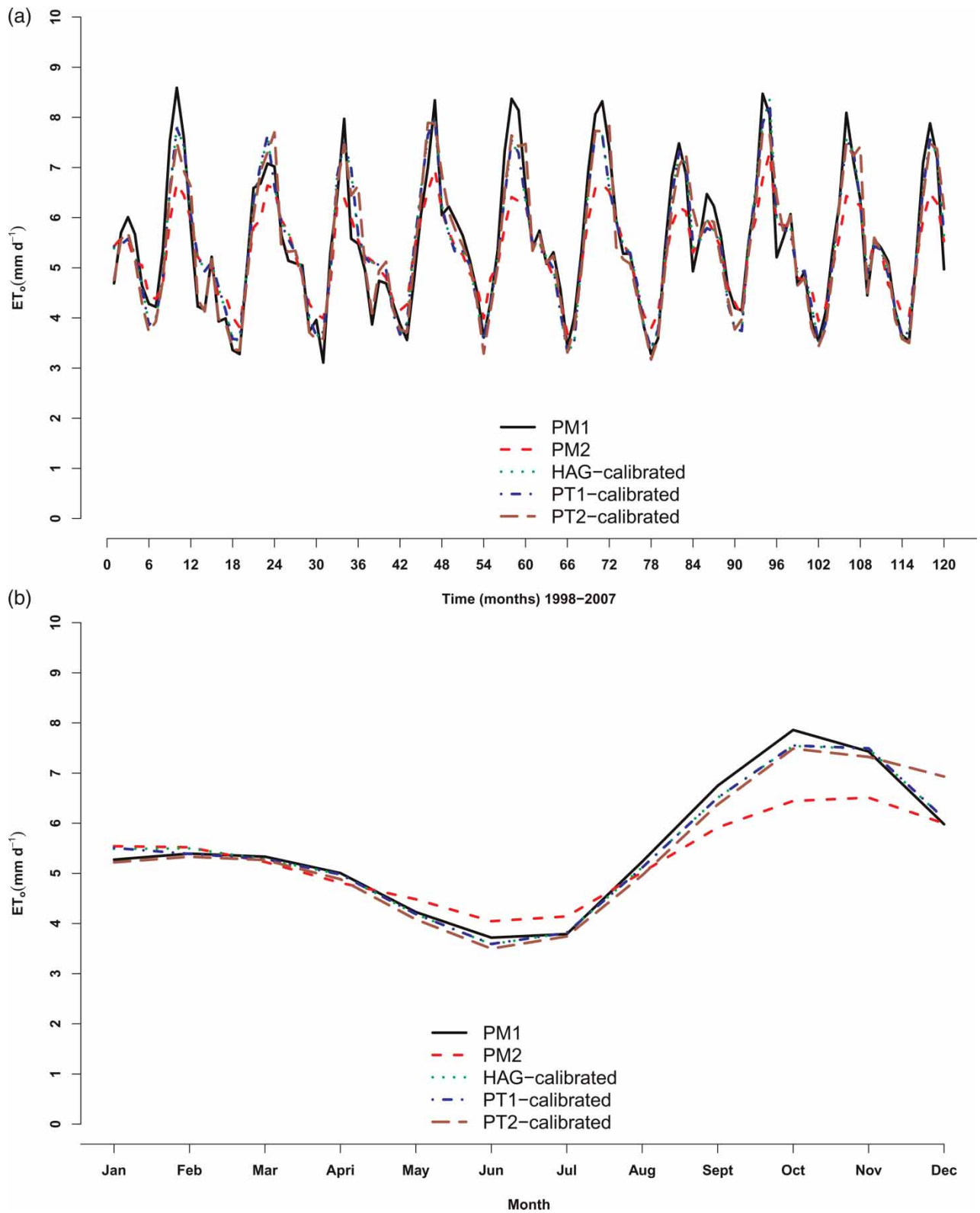
Figure 5(a) shows the monthly  $ET_0$  by the PT and HAG methods without local calibration as compared to PM1 and PM2 from 1998 to 2007. In addition, the monthly long-term means during the period are shown in Figure 5(b). All approaches including PM2 considerably underestimate PM1. However, the PT2 approach with observed  $R_{SR}$  is somewhat better although it overestimates  $ET_0$  in the summer (January–April), a finding similar to Trajkovic & Kolakovic (2009). Trajkovic & Živković (2008) attributed such overestimates to the effect of low wind speed, also suggested in Figure 2. As Figures 6(a) and 6(b) show, there is a significant improvement in the  $ET_0$  estimates using calibrated parameters. PT1 deviated the most and has the largest absolute values of MBE, RMSE, RE and slope

Table 6 | Monthly statistics of the HAG method against the FAO1 for Nchalo Station with calibrated  $C_H$  values

Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
MBE ( $\text{mm d}^{-1}$ )	-0.01	-0.08	-0.27	-0.17	-1.00	0.14	-0.28	-0.71	-0.72	-1.41	-0.38	-1.12
RMSE ( $\text{mm d}^{-1}$ )	1.15	1.02	0.98	-0.17	1.00	0.14	0.84	1.15	-0.72	1.90	-0.38	1.79
RE (%)	-0.25	-1.40	-5.07	0.58	-7.23	0.94	-7.40	-13.96	-11.04	-18.73	-5.04	-14.98
$R$	1.09	0.99	1.04	0.75	1.25	0.77	1.07	0.72	0.85	0.81	0.87	0.88
Slope $b$	1.01	1.02	1.06	1.13	1.08	1.05	1.08	1.15	1.19	1.22	1.18	1.04
$R^2$	0.96	0.97	0.97	0.97	0.97	0.97	0.96	0.97	0.97	0.97	0.97	0.96
$C_H$	0.0023	0.0024	0.0024	0.0026	0.0025	0.0024	0.0025	0.0027	0.0027	0.0028	0.0027	0.0024



**Figure 5** | (a) Comparison of  $ET_0$  and (b) long-term monthly mean  $ET_0$  computed from PM1, PM2 and PT1, PT2 and HAG methods (1998–2007).



**Figure 6** | (a) Comparison of PM1 and PM2 and (b) long-term monthly mean  $ET_0$  of PM1, PM2 with calibrated HAG and PT methods.

(Table 4). Without local calibration, the PT2 method still approximates PM1 much better than any other approach (it has the lowest absolute values of MBE, RMSE and RE), although the  $R$  value suggests that it overestimated the daily PM1 by about 15% (Figure 5(b)). The  $z$ -tests for the HAG and PT estimates with calibrated parameters showed that these estimates were not statistically different from the PM1  $ET_0$  ( $\alpha = 0.05$ ).

## CONCLUSIONS

The performance of the PM  $ET_0$  method was evaluated for 12 different data scenarios and alternative methods at the Nchalo Sugar Estate in the Lower Shire River basin in southern Malawi. The study found that using different expressions for the wind speed ( $u_2$ ) and actual vapour pressure ( $e_a$ ) did not significantly affect the PM  $ET_0$  estimates. However, when net radiation is estimated using the FAO-56 procedures (Allen et al. 1998), the PM method significantly underestimated  $ET_0$  ( $\alpha = 0.05$ ) as compared to the full data  $ET_0$ . Among the alternative  $ET_0$  methods, both the HAG and PT methods significantly underestimated PM1  $ET_0$  and both required local calibration. However, the performance of the PT method with observed  $R_{SR}$  and without local calibration provided the closest estimates. The HAG and PT approaches with locally calibrated monthly parameters considerably improved  $ET_0$  estimates, with their performance better than PM2 with estimated variables. The results, despite being based on only one climatic station, may provide some key insights into the ability of commonly used  $ET_0$  methods in other regions of Malawi and the southern Africa region when data are limited.

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