

Errata¹

On p. 318, first paragraph, line 23 should read:

At a sufficiently high applied stress intensity factor of K_{Ib} , the branched cracks will continue to propagate, and thus complete successful crack branches [16].

Equation (1a) should read:

$$\sigma_{\theta\theta} = \frac{K_I}{\sqrt{2\pi}} B_I \left[\left((S_1^2 - S_2^2) - (1 + S_1^2)\cos 2\theta \right) \frac{\cos \frac{\theta_1}{2}}{\sqrt{r_1}} \right. \\ \left. + \frac{4S_1 S_2}{1 + S_2^2} \cos 2\theta \frac{\cos \frac{\theta_2}{2}}{\sqrt{r_2}} - 2S_1 \sin 2\theta \left(\frac{\sin \frac{\theta_1}{2}}{\sqrt{r_1}} - \frac{\sin \frac{\theta_2}{2}}{\sqrt{r_2}} \right) \right]$$

$$+ \frac{K_{II}}{\sqrt{2\pi}} B_{II} \left[-2S_1 \sin 2\theta \frac{\cos \frac{\theta_1}{2}}{\sqrt{r_1}} + \frac{(1 + S_2^2)^2}{2S_2} \sin 2\theta \frac{\cos \frac{\theta_2}{2}}{\sqrt{r_2}} \right. \\ \left. + ((S_2^2 - S_1^2) + (1 + S_1^2)\cos 2\theta) \frac{\sin \frac{\theta_1}{2}}{\sqrt{r_1}} \right. \\ \left. - (1 + S_2^2)\cos 2\theta \frac{\sin \frac{\theta_2}{2}}{\sqrt{r_2}} \right] + \frac{\sigma_{ox}}{2} (1 - \cos 2\theta) \quad (1a)$$

Equation (1b) should read:

$$S_1^2 = 1 - \frac{c^2}{c_1^2}; \quad S_2^2 = 1 - \frac{c^2}{c_2^2} \quad (1b)$$

On p. 319, paragraph two, the last line should read:

With the predetermined $r_c = 1.3$ mm, the measured branching angle of $\theta_c = 52$ deg for the blunt crack tip was successfully predicted by computing K_{IQ} and σ_{ox} using a static finite element procedure which is described in detail in reference [10].

¹For "Dynamic Crack Curving and Branching in Line-Pipes" by M. Ramulu, A. S. Kobayashi, and B. S.-J. Kang, published in the November 1982 issue of the JOURNAL OF PRESSURE VESSEL TECHNOLOGY, Vol. 104, pp. 317-322.