IN SITU, DOPPLER RADAR, AND VIDEO OBSERVATIONS OF THE INTERIOR STRUCTURE OF A TORNADO AND THE WIND–DAMAGE RELATIONSHIP

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Observations inside a tornado, integrated with fine-resolution rapid-scan Doppler on Wheels data, and real-time observations of damage, reveal for the first time the three-dimensional structure of a tornado near the ground and help evaluate the enhanced Fujita scale.

THERE ARE FEW NEAR-GROUND OBSERVATIONS INSIDE TORNADOES.

Tornadoes cause substantial loss of life and property every year, primarily in the central regions of North America. In 2011, several hundred people lost their lives and over 20 billion dollars (all values are in current U.S. dollars) of damage occurred as the result of several tornado outbreaks that impacted populated regions (Lott et al. 2012; FEMA 2012). Verification of near-surface tornado wind models (Lewellen 1976; Church et al. 1979; Rotunno 1979; Davies-Jones 1986; Lewellen et al. 1997; Lewellen et al. 2000; Lewellen and Lewellen 2007a,b; Snow 1982; Fiedler and Rotunno 1986) and the relationship between these winds and structural damage requires reliable measurements near the ground, in the core flow region of tornadoes. In recent years, mobile Doppler radars have been central to mapping the three-dimensional wind structure in many tornadoes from as low as 30 m above ground level (AGL) to above 1 km AGL. These have allowed the documentation of the evolution and structure of tornadic winds including the prevalence of axial downdrafts aloft, low-level convergence, and the existence of multiple vortices (Wurman et al. 1996; Wurman and Gill 2000; Bluestein et al. 2003, 2004; Wurman and Alexander 2005; Wurman and Samaras 2004; Bluestein et al. 2007; Wurman et al. 2007a,b,c; Wurman 2002; Kosiba et al. 2008; Lee and Wurman 2005; Tanamachi et al. 2007; Wurman and Kosiba 2008; Wurman et al. 2008; Kosiba and Wurman 2010; Wurman et al. 2010; Wurman and Kosiba 2013, manuscript submitted to Wea. Forecasting). However, the structure of tornadic winds below ~30 m AGL has not been well quantified. Radar measurements, with few exceptions (Wurman...
and Alexander 2005; Wurman et al. 2007a; Kosiba et al. 2008; Kosiba and Wurman 2012), seldom extend much below 30 m AGL because of radar beam spreading and intervening terrain, flora, and manmade structures. The rare radar measurements that do exist in the 4–30-m AGL region reveal little reduction in wind speeds between 100 and 200 m AGL and the lowest observed levels (Wurman et al. 2007a).

Measurements of tornadic winds are challenging to obtain since tornadoes are small, difficult to predict, short-lived, and do not propagate along easily forecast tracks. Additionally, obtaining in situ measurements is extremely difficult since the interior environment of tornadoes is characterized by intense winds and rapidly moving airborne debris hazardous to instrumentation and observers. Infrequent near-surface (1–3 m AGL) wind data obtained at the edges of tornadoes suggest only a modest drop in ground-relative $V_g$ and tornado-relative $V_t$ wind speeds below the lowest frequently radar-observed levels (~100 m AGL) (Wurman et al. 2007a). These occasional 1–3-m AGL observations have been inconclusive regarding the intensity of radial wind speeds, $V_r$, with some observations suggesting nearly pure tangential flow $V_t$ with little or no spiraling inflow ($V_t << V_g$) and others suggesting intense inflow with $V_t > V_g$. This may be due to variations among tornadoes, azimuthal variations, or even localized and/or transient inflow jets in individual tornadoes. Since the in situ measurements alone result in only one-dimensional slices immediately near the ground, inferring three-dimensional vortex structure is problematic. While these data have revealed tantalizing information concerning the interior and immediate surroundings of tornadoes, they have not previously allowed the reconstruction of the near-surface three-dimensional winds.

**LITTLE FIELD DATA SUPPORTING WIND–DAMAGE RELATIONSHIPS.** In addition, the relationship between tornadic winds and damage is poorly understood. Recently the operational model used to infer peak tornado wind speeds from observed damage has been substantially modified and renamed the enhanced Fujita (EF) scale, modifying the wind gust speeds assumed to cause different intensities of damage (Wind Science and Engineering Center 2006; McDonald et al. 2004; Potter 2007; Doswell et al. 2009; Edwards et al. 2013). While this wind–damage relationship is used officially by the National Weather Service to estimate wind speeds, the new wind–damage relationships are based on “expert elicitations” and post-tornado damage surveys rather than empirical evidence relating specific damage events occurring during a tornado to measured winds in different locations within a tornado. Up until now, there has existed no direct intercomparision between anemometer-measured winds and real-time documentation of damage within a tornado. Model simulations (Fouts et al. 2003; Selvam and Millett 2003; Kuai et al. 2008; Haan et al. 2010) and occasional comparisons of radar-measured winds to damage (Wurman and Alexander 2005) have questioned some of the unverified assumptions of these damage–wind speed relationships, including the underlying assumption that damage is caused by the peak 3-s duration winds at 10 m AGL, without accounting for changes in the wind direction, speed, cumulative effects of longer duration intense winds, or the effects of impacts from airborne debris (e.g., breaking windows and/or doors, permitting wind to enter structures, resulting in upward wind loading on roofs). Accurate verification and quantification of the relationship between tornadic winds and damage requires direct comparisons between observed damage and measured winds in actual tornadoes.

**INTEGRATED WIND, VIDEO, AND RADAR INSIDE TORNADO REVEAL 3D STRUCTURE.** Just after 2152 UTC (hereinafter all times are UTC) on 5 June 2009, a tornado formed in Goshen County, Wyoming. It was observed by multiple instruments deployed for the second phase of the Verification of the Origins of Rotation in Tornadoes Experiment (VORTEX2) (Wurman et al. 2012; Kosiba et al. 2013; Markowski et al. 2012a,b; Wakimoto et al. 2011, 2012; Atkins et al. 2012), for its entire lifecycle until it dissipated at 2230 (Fig. 1). The tornado was given an EF-2 rating by the National Weather Service based partially on preliminary Doppler on Wheels (DOW) (Wurman et al. 1997; Wurman 2001; Wurman et al. 2008) observations. Peak winds in the tornado were measured at about 2214, at which time Rapid-Scan DOW (RSDOW) measurements revealed Doppler velocities $V_D$ of 72 m s$^{-1}$ at 30 m AGL.1 The DOWs (Fig. 2, bottom) are a network of mobile Doppler radars that have pioneered the finescale

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1 This measurement is near the EF-3/EF-4 threshold. Even though the observations were at 30 m AGL, it is likely, based on evidence in other tornadoes (Wurman et al. 2007a) and the evidence presented here, that the intensity of radar-observed winds at 30 m AGL is close, within 10%–20%, to that of standard-height 10-m AGL winds. This RSDOW measurement was not available to the National Weather Service at the time they made their EF-2 damage intensity rating.
observations of tornado structure and other small-scale and rapidly evolving phenomena (e.g., Wurman et al. 1996; Marquis et al. 2007; Wurman and Winslow 1998). Briefly, the DOWs operate at a wavelength near 3.2 cm, transmit narrow, ~0.9° wide beams, and scan quickly both vertically and horizontally to collect volumetric data. The Rapid-Scan DOW (RSDOW) (Wurman et al. 2008) transmits six simultaneous vertically stacked beams to provide rapid, 7-s, volumetric updates. Returned signals in all DOWs are processed to provide Doppler velocity, radar reflectivity, and other quantities. A detailed description of the DOW data collection, scanning strategy, deployments, and data processing used during this storm is discussed by Kosiba et al. (2013). In addition to the VORTEX2 instrumentation, the instrumented and armored Tornado Intercept Vehicle (TIV) (Wurman et al. 2007a) (Fig. 2, top) targeted the tornado. The TIV is a truck, modified and armored to facilitate the IMAX-format documentary filming inside tornadoes and supports a mast with an RM Young 5103 anemometer at 3.5 m AGL as well as other meteorological instrumentation. TIV wind and other meteorological data were recorded on a Campbell Scientific CR1000 data logger at 1-s intervals while video was collected from several vehicle-mounted and handheld cameras, as well as an IMAX-format film camera. Combined TIV and DOW observations provided the unique opportunity to integrate radar and in situ wind and video data to address outstanding questions related to the low-level tornadic wind structure and wind–damage relationships.

RSDOW data revealed the tornado crossed Four Corners Road at 41.62872°N, 104.34386°W at 2211:29.
and a propagation velocity $V_p$ of 7.5 m s$^{-1}$ toward 110° (east southeastward) (Fig. 3). An animation of the RADARW radar imagery during this period is available online at [www.cswr.org/BAMS-goshen.html](http://www.cswr.org/BAMS-goshen.html). Less than a minute earlier, at 2210:46, the TIV deployed on Four Corners Road, at 41.62840°N, 104.34386°W, in the path of the tornado. The terrain along the tornado track well west and at least 1 km east of the TIV, including the study period, was relatively flat and quite open although it became hilly to the east (Fig. 1). Video imagery taken from the TIV reveals a landscape dominated by grass. “Low grass, steppe” is associated with short roughness lengths and hence well-defined and kinematically based metric, defining the inside of a tornado as the region enclosing the maximum difference in velocity. But these measurements are only available rarely, perhaps in 1% of tornadoes. Damaging winds, lofted debris, and condensation funnel, but these definitions are problematic since they depend on ground conditions, atmospheric pressure dropped about 2,000 Pa (20 mb) to a minimum at 2211:25. TIV-measured wind speed and pressure reached relative minimums within few seconds of the independently DOW-measured time of closest approach of the center of tornado circulation, providing confidence in the spatial and temporal accuracy and navigation of the DOW and TIV data.

TIV observations during the passage of the tornado resulted in a transect of $V_g$ through a chord of the tornado, passing as close as 35 m from the center of circulation (Fig. 4). This permitted the calculation of the principal horizontal components of the tornado wind field, $V_p$ and $V_g$, from $35 < R < 120$ m, where $R$ is the distance from the center of rotation, using the DOW-measured $V_g = 7.5$ m s$^{-1}$ toward 110°. Profiles of $V$ (total tornado-relative velocity), $V_p$ and $V_g$ were created during both the approach and retreat of the center of the tornado (Fig. 6). The radius of maximum $V_g$, RMV, was 100 m, similar to the DOW-measured $R_g$ above the TIV, with $V_g = 50$ m s$^{-1}$. The radius of maximum $V_p$, RMVT, was 65 m, meaning that peak $V_p$ was outside the circle of peak $V_g$. Asymmetry was evident, with maximum $V_p = 40$ m s$^{-1}$ in the southeast sector and $V_g = 30$ m s$^{-1}$ in the southwest sector. In the southwest sector, strong inward $V_p = -40$ m s$^{-1}$ at $R = 100$ m decreased roughly linearly to $-15$ m s$^{-1}$ at $R = 35$ m, consistent with a Burgers–Rott wind profile (Burgers 1948; Rott 1958), resulting in

2 Doppler velocity errors are difficult to quantify and can be caused by many factors, including reflectivity weighting resulting in misrepresentative “mean” Doppler velocities, nonterminal velocity scatterers such as debris (Dowell et al. 2005), sidelobe contamination, and underlying noise in the measurements. Discussion of these is beyond the scope of this paper. Based on spatial and temporal continuity, it is likely that individual Doppler values are accurate within 5% or $\pm2$–3 m s$^{-1}$.

3 The DOWs were deployed at lower elevations than the TIV. The DOW7 antenna was at 1,488 m MSL (above mean sea level) and the Rapid-Scan DOW antenna was at 1,501 m MSL, while the ground elevation at the TIV was 1,531 m MSL. Therefore, the center of the lowest radar beams crossed over the TIV at approximately 20 m AGL. However, velocities in these lowest beams were often contaminated by ground clutter returns and data from 90 to 100 m AGL were used in some calculations.

4 The anemometer manufacturer states that wind speed accuracy is 1% and directional accuracy is 3° (www.youngusa.com/Brochures/05103%280106%29.pdf).

5 There is no accepted definition for the outer boundary of a tornado, so it is difficult to specify when the TIV and its anemometer were “inside” versus “outside” the tornado. Visual observers frequently define the outer boundary of a tornado as either the edge of the debris cloud or condensation funnel, but these definitions are problematic since they depend on ground conditions, atmospheric visibility, proximity to the tornado, lighting, and the humidity of the air flowing into the tornado, not just the kinematic structure. DOW measurements, when collected from close enough ranges to resolve the tornadic flow, result in a well-defined and kinematically based metric, defining the inside of a tornado as the region enclosing the maximum difference in velocity. But these measurements are only available rarely, perhaps in 1% of tornadoes. Damaging winds, lofted debris, and condensation can occur well outside the region enclosed by maximum velocity. Conversely, in rapidly propagating and/or weaker tornadoes, little or no damage may occur on the weak (left relative to $V_g$) side of the path of the center of the tornado where $V_p$ generally opposes $V_g$, resulting in less intense $V_p$.

6 The Burgers–Rott model provides a solution to the axisymmetric angular momentum equation by assuming the inward radial advection of angular momentum is balanced by the outward radial diffusion of angular momentum by viscosity, $\nu = G(1 – e^{-2ar^2/(2H)})/(a^2 H)$, where $\nu = -aR$ for $R < 65$ m, $a = 0.45$ s$^{-1}$, $G = 38,000$ m$^2$s$^{-1}$, and $n = 1,800$ m$^2$s$^{-1}$, where $a$ is constant, $G$ is circulation, and $n$ is viscosity. To reproduce decreasing winds outside RMV, $\nu = -0.64\nu_0$ for $R > 65$ m (constant pitch spiraling wind). This profile approximately matched observed $V_p$ and $V_g$ at the TIV (Fig. 6), although there are deviations due to both asymmetries in the tornado structure and the dynamical difference in the flow regime at 3.5 m AGL compared to that assumed in the model. No claim is made that the balance assumed in the Burgers–Rott model is suggested by the 3.5-m anemometer data.
the observed RMV > RMVT. The comparison with a Burgers–Rott profile is intended to be approximate. The aforementioned asymmetries are not represented in the modeled profiles and the available data did not permit a detailed analysis of these asymmetries. The measured pressure deficit was somewhat less than predictions based on cyclostrophic balance using the observed $V_t$ profiles, probably due to unbalanced and transient flow near the ground.

RSDOW observations every 7 s revealed a periodicity in tornado intensity, with amplitude of ~4 m s$^{-1}$ and peak energy at periods of 66 and 108 s (Fig. 7). This is consistent with long wavelength, upstream-propagating Rossby-type waves slowly revolving about the tornado at 6–10 m s$^{-1}$, not short wavelength multiple-vortex type phenomena that would complete orbits in ~20 s (e.g., Wurman 2002; Nolan and Montgomery 2002; Wurman and Kosiba 2013, manuscript submitted to Wea. Forecasting). No multiple vortices were observed visually (Wakimoto et al. 2011; Atkins et al. 2012), and while peak $V_g$ was higher in the southwest sector of the tornado (2211:43 in Fig. 5), values of $V$ were very similar at comparable $R$ in both sectors (Fig. 6). While variations in surface roughness, lofted debris, and other conditions could cause modulation in low-level wind intensity (e.g., Lewellen et al. 2008), the observed oscillatory behavior is present from 2210 to 2213, during which the tornado is crossing relatively flat and homogeneously grassy terrain (Fig. 1).

Models of tornado flow (Lewellen 1976; Davies-Jones 1986; Lewellen et al. 1997; Lewellen et al. 2000; Lewellen and Lewellen 2007a,b; Snow 1982; Fiedler and Rotunno 1986) predict that within the RMV tornadoes may contain updrafts, downdrafts, or both. Radar observations suggest updrafts or downdrafts may be present (Wurman et al. 1996; Wurman and Gill 2000; Bluestein et al. 2003; Wurman 2002; Kosiba et al. 2008; Lee and Wurman 2005; Tanamachi et al.}

![Fig. 3. (left) Radar reflectivity (dBZ) and (right) Doppler velocity ($V_d$) in the Goshen County, Wyoming, tornado at (top) 2211:23, (middle) 2211:34, and (bottom) 2212:03 5 Jun 2009 as observed by the Rapid-Scan DOW radar as the tornado crosses over the TIV (yellow dot) and pole 100S (red dot). The center of rotation of the tornado, surrounded by an approximately 105-m region between maxima in $V_d$ (black dots and circles, labeled with seconds after 2211:00), crosses 35 m north-northeast of the TIV at 2211:31, resulting in a transect of the core flow region (red arrow) from 2211:18 to 2211:43. A moderate-intensity (yellow and brown) reflectivity debris ring surrounding tornado is clearly visible, as is higher reflectivity (red) associated with rain and hail observed at the TIV before and after the tornado’s passage. Black tick marks are spaced at 200-m intervals.](http://journals.ametsoc.org/bams/article-pdf/94/6/835/3741983/bams-d-12-00114_1.pdf)
2007; Kosiba and Wurman 2010) and that downdrafts penetrating as low as the lowest radar-observed level may predominate (Alexander and Wurman 2008). To evaluate the updraft/downdraft structure in this tornado near the surface, the vertical component of wind velocity $W$ at 7 m AGL (twice the TIV anemometer height) was derived from the vertical momentum equation using $V_r$ and $V_t$ and assuming mass conservation, incompressibility, and $W(0 \text{ m AGL}) = 0 \text{ m s}^{-1}$. Upward motion of $\sim 7 \text{ m s}^{-1}$ was calculated from $35 < R < 120 \text{ m}$, although there was considerable spread, between $-1$ and $+14 \text{ m s}^{-1}$ for $R < 55 \text{ m}$ (Fig. 6). This observation of $W << V$ is consistent with video evidence that revealed predominantly horizontal motion of small debris, primarily grass, within a few meters AGL.

RSDOW data were interpolated to a Cartesian grid [using a Barnes (1964) scheme with $\kappa = 0.0016 \text{ km}^{-2}$ and grid spacing = 20 m] in order to derive the axisymmetric three-dimensional winds ($V_r$, $V_t$, and $W$) aloft in and near the tornado using the ground-based velocity track display (GBVTD) method, which was originally developed to analyze hurricane vortices (Lee et al. 1999) and has since been extended to resolve tornadic structure (Bluestein et al. 2003; Lee and Wurman 2005; Bluestein et al. 2007; Tanamachi et al. 2007; Kosiba and Wurman 2010). This revealed maximum $V_t$ near $40 \text{ m s}^{-1}$ with RMVT = $150 \text{ m}$, greater than RMVT calculated from anemometer data (Fig. 8). This difference was likely due either to the widening and weakening of the tornado between the ground and the lowest radar-observation level used in the GBVTD analysis, and/or to spatial smoothing in the GBVTD analysis. Aloft, the GBVTD-derived winds revealed an axial downdraft with peak $W$ of $\sim 10 \text{ m s}^{-1}$ and weak outflow/divergence inside the RMVT, which was in contrast to the strong inflow measured near the ground. Recall that in situ video evidence obtained by the TIV, below the lowest GBVTD level, indicated predominantly horizontal inward-spiraling near-surface winds, and analysis of anemometer data revealed modest upward motion at 7 m AGL.\(^7\)

The temporal variability of the profiles of $V_r$ and $V_t$ is about $5 \text{ m s}^{-1}$. These may be manifestations of asymmetries in tornado structure, which may be better or more poorly resolved by the radar at different times, actual tornado evolution, or errors.

\(^7\) The Barnes analysis was extrapolated below the lowest radar observation level, and a boundary condition of $W = 0$ at the ground was imposed. With no evidence that the 3.5-m AGL TIV observations were representative well above the surface, and the likelihood that the observed inflow was shallow, these observations were not interpolated upward. Different boundary conditions could affect the GBVTD-retrieved $W$. 

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**Fig. 4.** Schematic illustration of transect of tornado by the TIV. The tornado, with a radius of maximum winds of 100 m, propagates toward 110° at 7.5 m s\(^{-1}\), with the center of circulation passing 35 m north-northeast of the TIV, resulting in measurements through a chord of the tornado as shown. Wind barbs show measurements of $V_r$ at 3.5 m AGL with pennants indicating 50 m s\(^{-1}\), full barbs 10 m s\(^{-1}\), and half barbs 5 m s\(^{-1}\).

**Fig. 5.** TIV-measured wind speeds inside tornado every 1 s (blue), averaged for 3 s (red). Modeled winds at the TIV (black) and at pole 100S (green). Peak RSDOW $V_r$ (yellow). Zoomed in video image of pole 100S snapping at 2211:38.
in the GBVTD analysis. The overall consistency of the retrieved bulk structure provides confidence in the validity of the analysis.

During the transect, peak $V_d$ at 20–90 m AGL ranged from 45 to 52 m s$^{-1}$ (Fig. 5), less intense than TIV-measured peak $V_g$, suggesting that the most intense $V_g$ was likely between 3.5 and 20 m AGL. However, due to spatial smoothing in the radar data, these observations are also consistent with nearly constant $V_g$ from 3.5 to 90 m AGL, as found previously (Wurman et al. 2007a). Critically, for the overwhelming majority of analyses of tornadoes, which employ radar data only from >30 m AGL and lack contemporaneous in situ data, wind speeds at ~10 m AGL are not substantially less than those measured at the lowest radar-observed levels.

A three-dimensional model of this tornado’s structure was created using the combined anemometer, video, and DOW data from this study (Fig. 9). Strong inward-spiraling near-surface inflow approached the tornado center and then rose at a moderate, approximately constant speed. Aloft, an axial downdraft penetrated to below 100 m AGL, and inflow was much weaker and did not approach the center of circulation. This reconstruction is consistent with the range of structures predicted in tornadoes (Lewellen 1976; Davies-Jones 1986; Howells et al. 1988; Church and Snow 1993; Lewellen et al. 1997) and observed by radar (Wurman et al. 1996; Wurman and Gill 2000; Wurman and Alexander 2005; Bluestein et al. 2007; Wurman et al. 2007a; Tanamachi et al. 2007; Kosiba et al. 2008; Kosiba and Wurman 2010), although the axial downdraft intensity is substantially smaller than previously observed (Wurman et al. 1996; Wurman and Gill 2000; Kosiba et al. 2008; Kosiba and Wurman 2010). Significantly, this “divided” vertical structure suggests that the largest winds occur between the surface and the height of the downdraft (Fiedler and Rotunno 1986; Church and Snow 1993) and therefore it is likely that the maximum wind speed occurred between the radar-observed and anemometer-observed levels. Potentially interesting structural features in the corner flow region between 3.5 and 30 m AGL were not resolved in this study and are not represented in the deduced three-dimensional model.

**Comparisons of Winds and Damage.** The time history of $V_g$ at all near-ground points impacted by the tornado was calculated by fitting a modified Burgers–Rott vortex
wind profile (Burgers 1948; Rott 1958) of $V_r$ and $V_t$ to the TIV transect data (Fig. 5). This allowed for the temporal evaluation of $V_g$ as the tornado damaged a line of wire-connected wooden electrical transmission poles, including one adjacent to the TIV (pole A), one 100 m to the south (pole 100S) (Figs. 3 and 5), and a pole 200 m south of the TIV (pole 200S) (not shown). The value of $V_g$ at pole 100S increased to a maximum of 56 m s$^{-1}$ at 2211:38 as the wind direction veered from south to west northwesterly. Video revealed that pole 100S snapped at 2211:38, near the time of maximum $V_g$ at pole 100S, dragging the poles farther to the south (e.g. Pole 200S). Pole A also snapped at 2211:38, nearly simultaneously with pole 100S, when measured-TIV winds were $V_g = 49$ m s$^{-1}$ from the west-northwest, but that location experienced more intense winds after pole A snapped. Pole A may have been very near failure and dragged down by the added stress caused by the falling wires connected to pole 100S or it may have failed independently. Pole A had survived TIV-measured winds of 51 m s$^{-1}$ from the southwest several seconds earlier, at 2211:18. (An excerpt from the video of the poles snapping is available online at www.cswr.org/BAMS-goshen.html.)

The EF scale (Wind Science and Engineering Center 2006; McDonald et al. 2004; Potter 2007; Edwards et al. 2013) suggests that wooden electrical transmission line poles should fail at an “expected” wind speed of 53 m s$^{-1}$, with the lower bound of all expert elicitations being 44 m s$^{-1}$. Pole 200S experienced peak wind gusts of only 39 m s$^{-1}$ at the time it failed, substantially lower than these EF-implied destruction thresholds (and only slightly above the EF-scale expected wind speed associated with the “threshold of visible damage” at 37 m s$^{-1}$). Pole 200S is seen in the video to have been dragged down by wires connecting it to pole 100S and not destroyed directly by the local peak wind gusts themselves. Pole A snapped at a wind speed, $V_g = 49$ m s$^{-1}$, below the EF-scale expected prediction, but winds exceeded the expected threshold after damage was complete. Pole 100S survived the EF-scale expected wind speed of 53 m s$^{-1}$, then failed at 56 m s$^{-1}$, which is below the “upper bound” wind speed of 63 m s$^{-1}$. The EF-scale descriptive document (Wind Science and Engineering Center 2006; McDonald et al. 2004; Potter 2007; Edwards et al. 2013) suggests that wooden electrical transmission line poles should fail at an “expected” wind speed of 53 m s$^{-1}$, with the lower bound of all expert elicitations being 44 m s$^{-1}$. Pole 200S experienced peak wind gusts of only 39 m s$^{-1}$ at the time it failed, substantially lower than these EF-implied destruction thresholds (and only slightly above the EF-scale expected wind speed associated with the “threshold of visible damage” at 37 m s$^{-1}$). Pole 200S is seen in the video to have been dragged down by wires connecting it to pole 100S and not destroyed directly by the local peak wind gusts themselves. 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Pole 100S survived the EF-scale expected wind speed of 53 m s$^{-1}$, then failed at 56 m s$^{-1}$, which is below the “upper bound” wind speed of 63 m s$^{-1}$. The EF-scale descriptive document (Wind Science and Engineering Center 2006; McDonald et al.
Center 2006) states very generally that there are “factors . . . which can cause a deviation (either lower or higher) from the expected wind speed for a DOD [degree of damage].” However, in many circumstances it is difficult to determine whether structural failure was concurrent with the occurrence of the maximum wind speeds, or occurred earlier, as in the case of the failure of pole A, or even later. Similarly, it is difficult to distinguish between a failure due to a combination of factors, such as wind and dragging experienced by pole 200S, and a failure due to only locally occurring wind. The video and wind velocity observations in this case show that of the three poles, only pole 100S failed unambiguously due to wind. The current observations document variability in the failure wind speeds for different poles, different damage potential caused by varying wind directions, and/or complex failure modes such as one pole dragging down another, as well as structural failure preceding peak winds.

Additionally, the EF-scale expected value for “broken cross members” is 44 m s\(^{-1}\), and the upper bound is 51 m s\(^{-1}\). These wind speeds were well exceeded at pole A and pole 100S, but neither pole experienced broken cross members prior to pole collapse. Finally, it is important to note that peak DOW radar-observed wind speeds of 72 m s\(^{-1}\), over 20 m s\(^{-1}\) stronger than observed by radar during the damage event, occurred about 200 s later near 2214 during a time when the tornado was impacting only open grassland more than 1 km east of the line of poles (Fig. 1), causing no documented damage. More intercomparisons between measured winds and cotemporal damage are needed to evaluate the EF scale’s wind speed values, and the application of the EF scale’s wind–damage relationship to accurately relate structural damage to peak wind gust intensity.

**SUMMARY AND CONCLUSIONS.** This unique integration of in situ wind measurements, finescale mobile radar measurements, and visual/video evidence has allowed the three-dimensional structure of a tornado, aloft and very near the ground, and the mechanisms by which it caused damage, to be characterized in unique detail. Near-surface convergence to very near the center of rotation, peak tornado and ground-relative winds outside the RMW, and an axial downdraft not penetrating to the surface have been revealed. Observed asymmetries, however, cause deviations from the simple deduced model, and quasiperiodic modulation of intensity is documented. Horizontal wind speeds between the lowest radar-observed levels (~30 m AGL) and 3.5 m AGL were similar, and therefore it was assumed that these were approximately constant between observation levels.

Complexities in the mechanisms and the time history of damage have illuminated limitations of the operationally employed EF wind-damage scale. Specifically, three nearly identical structures failed at substantially different wind speeds in this tornado, and cross-member damage, predicted at the observed wind speeds, did not occur. One structure failed before peak winds were experienced at that location. Moreover, radar-observed tornado intensity peaked after the occurrence of documented damage, a well-known limitation of damage-intensity-based wind estimation methods. Additional radar and in situ observations in tornadoes in the region <30 m AGL (Kosiba and Wurman 2012) will be critical in refining knowledge concerning low-level tornado structure, and the relationship among wind speed, direction, and duration and observed damage.
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