

Development of daily rainfall erosivity model for Kelantan state, Peninsular Malaysia

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ABSTRACT

The study was conducted to develop a rainfall erosivity model for tropical climates to estimate daily rainfall erosivity and determine the most effective power law relationship between rainfall erosivity and daily precipitation. Thirty minute resolution rainfall data recorded in 55 stations of a state in Peninsular Malaysia were analysed. Using three precipitation limits of 0.1, 5.0 and 12.7 mm, the behaviour of rainfall on average annual rainfall erosivity gave ranges of 10,264–54,284, 8,151.5–48,301 and 4,958–39,938 MJ mm ha⁻¹ h⁻¹ y⁻¹ respectively. It was found that the number of individual events, occurring within a day, were more in the area compared other types of events for all precipitation limits (0.1, 0.5 and 12.0 mm). Spatio-temporal variation of monthly coefficient values of power law relationship was found with the highest R² in the range of 0.93–0.94 for 0.1 mm precipitation limit. Out of 55 stations, 15 were selected for model development and assessment. On the basis of importance of smaller events, a 0.1 mm precipitation limit was selected for the proposed model. The proposed model was found good for monthly and annual rainfall erosivity estimation apart from few limitations. Furthermore, the validity of the proposed model was checked for different parts of the area.

Key words | daily rainfall erosivity model, precipitation, rainfall erosivity, RUSLE R-factor, soil erosion, tropical climate

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INTRODUCTION

Prevention of soil loss from erosion due to the impact of rainfall and changing rainfall patterns is one of the most important global issues in soil conservation. These changes in precipitation are largely located in the tropics and hence are probably associated with convection (Tan *et al.* 2015). The increased precipitation causes detachments of the individual soil particles and their transportation along the slope to rivers and reservoirs. Rainfall erosivity is a predominant factor referring to

the kinetic energy of a raindrop's impact and the rate of associated runoff (Wischmeier & Smith 1978). Therefore, it is essential to obtain an accurate estimate of rainfall erosivity in tropical climates for the assessment of soil erosion risk.

The Universal Soil Loss Equation (USLE) devised by Wischmeier & Smith (1978) and the Revised Universal Soil Loss Equation (RUSLE) proposed by Renard *et al.* (1997) for the United States are widely used models to estimate

annual soil loss by both interrill and rill erosion. These include six factors such as rainfall erosivity, soil erodibility, slope steepness, slope length, cover-management, and support practice. These factors are dynamic in nature which results in heterogeneous spatial patterns of soil loss. However, RUSLE requires regional values to be developed for each factor based on local data and conditions if used outside the United States (Wischmeier 1984).

The rainfall erosivity (R) factor is considered as the most important factor in estimation of soil loss due to its high temporal variability. The R factor was derived from more than 8,000 plot years by Wischmeier (1984) and can be quantified by the product of total kinetic energy of rainfall (E) and its peak 30 minute intensity (I_{30}) which computes all individual erosive storm events. An individual rainfall event was defined as a period of rainfall with at least six preceding and six succeeding non-precipitation hours (Xie *et al.* 2016).

Therefore, the main disadvantage to compute RUSLE is the requirement of high spatial and temporal (maximum 30 minutes) rainfall data series for the determination of the R factor, and these data are not generally available. However, kinetic energy can also be used for the calculation of the R factor and varies for different climates. The kinetic energy can be calculated for any region by using very high temporal resolution data (1 min, 5 min) but such data is generally not available. Alternatively, kinetic energy and intensity relationship can be used which need 30 min rainfall data to calculate the kinetic energy of an event. Salles *et al.* (2002) listed all the kinetic energy and intensity relationships developed for different locations which can be used in the absence of very high temporal resolution data for a particular location.

Apart from event based R factor calculation, other statistical models were also developed by researchers for different climates to calculate erosivity which use commonly available data, such as daily rainfall (Richardson *et al.* 1983; Yu & Rosewell 1996a; Petkovič & Mikoš 2004; Angulo-Martínez & Beguería 2009; Ali 2015; Xie *et al.* 2016) and monthly rainfall (Renard & Freimund 1994; Yu & Rosewell 1996b; Ferro *et al.* 1999; de Santos Loureiro & de Azevedo Coutinho 2001; Mikoš *et al.* 2006; Diodato & Bellocchi 2007; Ochoa-Cueva *et al.* 2015). Xie *et al.* (2016) mentioned three aspects of the R factor that may be useful for soil erosion estimation: (1) average

annual rainfall erosivity for predicting average annual soil loss, (2) seasonal distribution curve of rainfall erosivity and (3) event or daily rainfall erosivity. They also stressed the importance of event or daily rainfall erosivity in their related past studies and developed statistical models for the successful estimation of erosion index EI_{30} from the daily rainfall amounts. Due to the lack of long-term event-based rainfall data, these statistical models are very useful and widely used to calculate daily erosivity. However, both event and daily rainfall amounts are not similar (Bullock *et al.* 1990) because daily rainfall amount includes only one event, multiple events, or only part of an event (Richardson *et al.* 1983; Xie *et al.* 2016).

Angulo-Martínez & Beguería (2009) estimated the R factor for the Mediterranean climate by using five daily models, viz. the exponential model by weighted least squares (Richardson *et al.* 1983), the Yu and Rosewell model, the modified Yu and Rosewell model and three monthly models, viz. precipitation intensity indices, the modified Fournier index and the F index (Ferro *et al.* 1999) in which they found that the Yu and Rosewell model for daily and precipitation intensity indices for a monthly R factor gave the best results as compared to the other models. Xie *et al.* (2016) also found superiority of the Yu and Rosewell over the Richardson exponential model. All these models have some regional factors which vary for different climates and these must be determined accurately to develop an accurate rainfall erosivity model.

The tropical climate has high precipitation throughout the year. The orographic precipitation is also well-known and has been identified and studied across the world (Karnieli & Osborn 1988; Goldreich 1994; Michaud *et al.* 1995; Al-Ahmadi & Al-Ahmadi 2013). Therefore, the regional factor values will definitely vary in high precipitation and elevation regions. An attempt was made by Yu *et al.* (2001) to estimate the R factor for tropical climates by using event-based data for the Yu and Rosewell model but the disadvantages of this model is that the limited rainfall stations and less temporal data (2 years only) were used which may not be accurate for the region (Yu & Rosewell 1996a). Other studies also use event-based data to calculate soil erosion by RUSLE in tropical climates, such as Shamshad *et al.* (2008), Leow *et al.* (2011) and Kamaludin *et al.* (2013), while some estimate rainfall

erosivity by including orographic effect such as for the Mediterranean climate (Diodato & Bellocchi 2007) and the semi-arid climate (Nearing et al. 2015).

Previous research focused on event-based, daily and monthly precipitation data to calculate erosivity for climates other than tropical. Limited attempts were made to calculate regional factors for the tropical climate models which are suitable for commonly available data such as daily precipitation. The purpose of this study is to develop a daily rainfall erosivity model for a region of tropical climate by using 30 minute rainfall intensity data which will be helpful to calculate accurate average annual rainfall erosivity using RUSLE in the absence of high resolution data. Therefore, to achieve this goal, the study was conducted with the following steps: (i) use of high spatial and temporal data (30 min) data to calculate the *R* factor, (ii) to calculate monthly regional factors from power law relationship for Kelantan state, Peninsular Malaysia, and finally (iii) to develop a monthly power law relationship between erosivity and daily rainfall amount for the region.

STUDY AREA AND DATA

Study area

The study was conducted in Kelantan state, in the north eastern part of Peninsular Malaysia between latitudes 4°33' and 6°14' north, and longitudes 101°19' and 102°39' east with an area of approximately 15,000 km². The northern part is bounded by the South China Sea and higher elevations are on the south, south-east and south-west sides (Figure 1).

The elevation ranges from 0 to the highest point of 2,187 m named as Mt. Tahan. The area is divided into upstream (Gua Musang), midstream (Kuala Krai, Jeli, Tanah Merah and Machang) and downstream (Pasir Mass, Pasir Puteh, Kota Bharu, Bachok and Tumpat), as shown in Figure 1. The climate is tropical, humid with average temperature ranges from 20 to 30°C. The period from November to January receives maximum rainfall, while June and July are the driest months. According to the Malaysian Meteorological Department, the wind strength is generally light and variable, however, there are yearly periodic changes in the wind flow patterns and based on this, the season is divided

into four, namely, the southwest monsoon, northeast monsoon and two shorter periods of inter-monsoon seasons. The state is affected by the north-eastern monsoon wind accompanied by heavy precipitation beginning early November and ending in March. The easterly or north-easterly winds of 10 to 20 knots can sometimes reach 30 knots or more as a result of the strong surges of cold air from the north. Masseran & Razali (2016) mentioned that the winds which blow across the South China Sea bring heavy rain, especially to the eastern and southern coasts of Peninsular Malaysia as well as the central part of the Titiwangsa Ranges. This rain causes flooding, especially in November and December, in the east coast states. Average annual rainfall of the area is 3,017 mm while average daily annual wind speed is 1.50 m/s. The average monthly rainfall from November to January is 418 mm with a maximum of 576 mm in December.

Data

Thirty minute intensity data from 55 stations were obtained from the Department of Irrigation and Drainage, Malaysia. Distribution of the number of rain gauges in upstream, mid-stream and downstream are 16, 17 and 22, respectively. Out of the 55 stations, 25 are relatively new, which have the data recorded from 2005 onwards. Some records of the precipitation data have been replaced by the nearby station data due to non-availability of the original data of the reporting station because of system failure at that station. Thirty minute records, measured from the current day at 12:00 am up to the next day at 12:00 am, for each station from January 2005 to December 2015, were selected.

As per the rule of RUSLE an event is considered erosive if the cumulative rainfall is greater than 12.7 mm. The precipitation limit 0.1 mm, 5.0 mm and 12.7 mm were taken into account in this study to estimate the *R* factor because precipitation is recorded almost throughout the year in tropical climates, hence, every small event may be playing an important role in soil erosion by keeping the soil moist. For cross-validation, a 70:30 ratio of calibration (40) and validation (15) stations were randomly selected in such a way as to represent the entire study area. Validation stations were for model development while the 40 calibration stations were for model parameter development. The details of calibration and validation stations are shown in Tables 1 and 2 respectively.

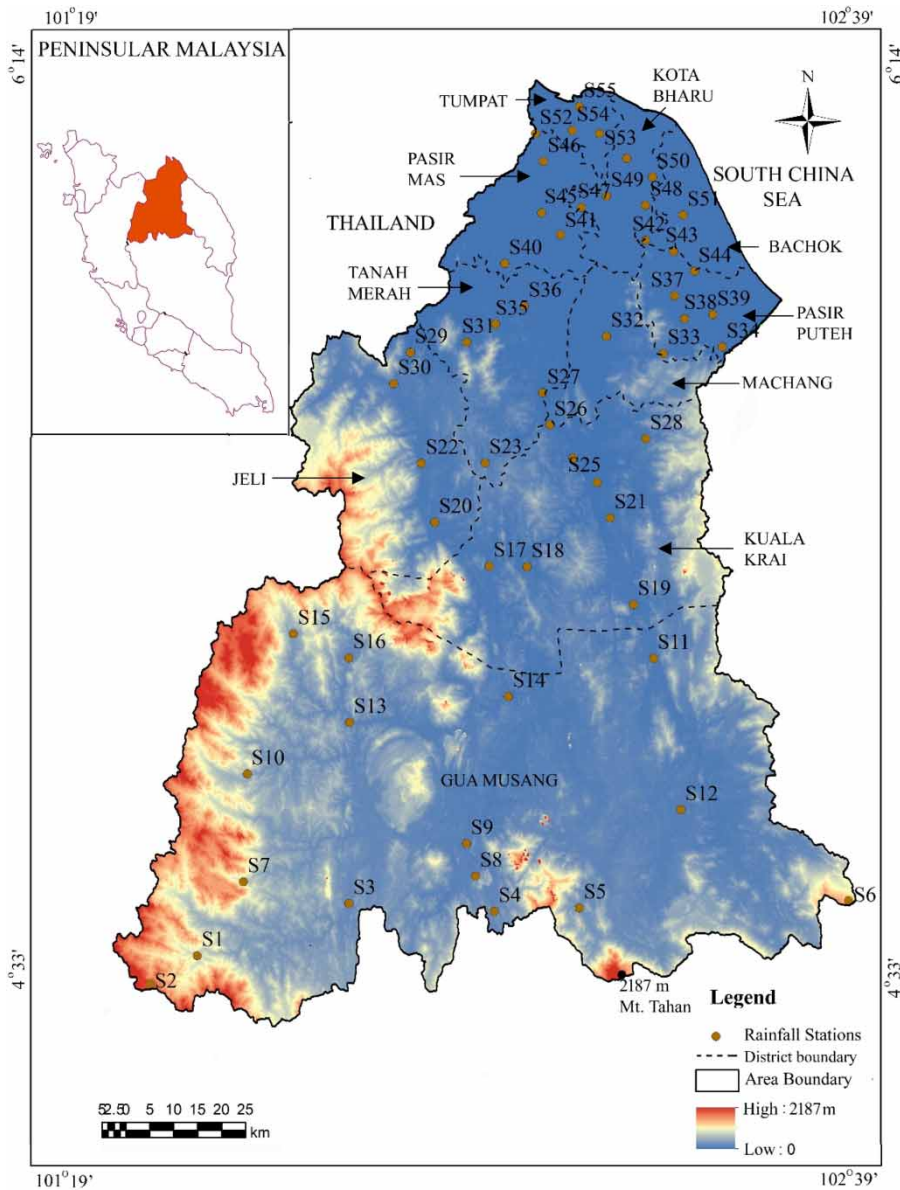


Figure 1 | The study area with distribution of 55 stations with 30 min resolution of rainfall data.

METHODS

Rainfall erosivity estimation

Daily rainfall erosivity index (EI_{30}) values were calculated using 30 min rainfall intensity data for the period 2005–2015. The events were separated on the basis of a dry period or a day. If the duration between two events is

equal to or greater than a dry period then the events were considered as two events. The dry periods of the data were calculated on the basis of ‘minimum dry period duration (MDPD)’ which is 6 h in this study (Wischmeier & Smith 1978). Xie et al. (2016) mentioned the four types for the occurrence of an erosive event in a daily time period. In this study, the following three types were considered: (1) only one erosive event occurs which begins and ends in

Table 1 | Details of calibration stations in the study area

Station no.	Station name	Lat. (° N)	Long. (° E)	Elev. (m)	No. of erosive events	Annual rainfall (mm)		
						0.1	5	12.7
S2	Lojing	4.60	101.40	1,707	1,853	2,593.7	2,431.1	1,988.8
S3	Blau	4.77	101.76	224	1,294	1,885.3	1,784.9	1,498.5
S4	Ldg. Mentara	4.76	102.02	173	1,726	2,429.9	2,274.2	1,942.1
S6	Gunung Gagau	4.76	102.66	976	2,007	4,261.5	4,122.9	3,723.2
S7	Hau	4.81	101.57	689	1,823	2,300.8	2,126.6	1,670.2
S8	Redip	4.82	101.98	371	1,801	2,429.9	2,275.6	1,887.3
S10	Chabai	5.00	101.58	372	1,536	2,362.5	2,236.2	1,931.2
S11	Lebir, paloh	5.21	102.30	84	1,717	2,641.1	2,498.9	2,167.9
S13	Gemala	5.10	101.76	147	1,431	1,926.1	1,800.9	1,521.8
S14	B. Polis Bertam	5.15	102.05	67	1,593	2,071.7	1,932.1	1,604.1
S15	Gob	5.25	101.66	274	1,810	2,534.9	2,375.7	1,982.9
S18	Kuala Gris	5.38	102.08	115	1,680	2,495.0	2,357.4	2,004.4
S19	Laloh	5.31	102.28	44	1,633	2,421.4	2,290.1	1,952.1
S20	Kuala Balah	5.45	101.91	64	288	2,988.4	2,852.0	2,510.9
S22	Keb.L. Bungor	5.56	101.89	39	1,772	3,211.1	3,083.2	2,732.6
S23	Ulu Sekor	5.56	102.01	102	1,794	3,068.0	2,934.4	2,576.6
S24	Kuala Nal	5.57	102.16	35	1,630	2,788.8	2,662.8	2,326.0
S26	Kerilla	5.68	102.11	32	1,798	3,208.8	3,080.0	2,739.0
S27	Chenulang	5.60	102.29	75	167	3,575.1	3,432.3	3,080.3
S28	Gemang Bahru	5.76	101.87	53	1,893	3,606.9	3,467.2	3,123.8
S30	Durian Daun	5.78	101.97	25	1,837	3,552.1	3,420.8	3,070.0
S31	Jps Machang	5.79	102.22	10	1,640	3,429.1	3,311.1	2,986.3
S33	Wakaf Raja	5.77	102.43	29	1,704	3,415.1	3,292.2	2,991.8
S34	P. B. Merbau	5.81	102.02	41	1,756	3,478.0	3,355.3	3,022.2
S36	I.B.Tiga Daerah	5.86	102.34	16	663	3,244.6	3,116.5	2,705.2
S37	Cherang Tuli	5.82	102.36	28	1,648	3,327.3	3,200.3	2,884.4
S39	Tandak	5.92	102.03	6	1,712	4,571.3	4,458.2	4,140.4
S40	I.B. Uban	5.97	102.14	20	1,650	3,030.0	2,903.7	2,611.5
S41	P. Melor	5.96	102.29	8	1,541	3,102.5	2,977.3	2,681.7
S42	Serdang	5.94	102.34	3	586	3,167.2	3,042.4	2,732.4
S43	Tok Ajam	5.90	102.38	3	1,585	3,236.4	3,111.2	2,807.1
S45	R. K. Meranti	6.10	102.11	17	1,498	3,151.7	3,025.2	2,727.0
S46	P. Kubor	6.02	102.18	19	1,596	3,168.7	3,050.6	2,743.0
S47	Peringat	6.02	102.29	13	1,822	2,993.2	2,865.3	2,570.6
S48	C. Tiga Pendek	6.04	102.22	21	1,535	2,824.6	2,698.8	2,398.6
S49	Binjai	6.08	102.30	7	1,563	3,045.6	2,920.6	2,627.9
S50	Teratak Pulai	6.01	102.36	8	1,553	3,086.1	2,956.4	2,656.3
S52	Kg. Kebakat	6.15	102.21	19	591	2,942.3	2,823.0	2,540.5
S53	C. Ampat	6.16	102.16	6	1,564	2,707.4	2,580.3	2,256.9
S54	K. Tumpat	6.20	102.17	7	591	2,601.5	2,469.0	2,203.7

Table 2 | Details of validation stations in the study area

Station no.	Station name	Lat. (°N)	Long. (°E)	Elev. (m)	No. of erosive events	Annual rainfall (mm)		
						0.1	5	12.7
S1	Brook	4.68	101.48	624	1,612	2,143.2	1,992.4	1,612.1
S5	Upper Chiku	4.77	102.17	214	1,801	3,062.4	2,928.1	2,582.4
S9	Gua Musang	4.88	101.97	92	1,666	2,338.1	2,196.1	1,859.0
S12	Aring	4.94	102.35	99	1,673	2,679.3	2,544.7	2,198.9
S16	Pasik	5.21	101.76	166	1,686	2,248.3	2,095.7	1,741.9
S17	Dabong	5.38	102.02	41	1,652	2,358.5	2,225.2	1,890.3
S21	Lepan Kabu	5.46	102.23	66	1,639	2,582.7	2,443.8	2,113.6
S25	Men. T. K. Krai	5.53	102.20	38	1,640	2,758.3	2,624.4	2,269.1
S29	Jeli	5.70	101.84	107	1,818	3,263.6	3,133.1	2,771.1
S32	Telusan	5.76	102.32	64	1,734	3,420.6	3,288.3	2,945.6
S35	Bendang Nyior	5.84	102.07	11	1,650	3,187.0	3,070.7	2,762.4
S38	P. Pasir Puteh	5.83	102.42	9	1,476	2,921.3	2,802.2	2,512.3
S44	R. P.Repek	6.01	102.10	21	1,583	3,151.7	3,025.2	2,727.0
S51	Kuala Jambu	6.15	102.10	3	1,372	2,635.4	2,519.1	2,261.9
S55	Kota Bharu	6.11	102.26	8	1,400	2,156.1	2,040.0	1,779.9

the same day, in which case:

$$R_{day} = EI_{50} \quad (1)$$

where R_{day} is the rainfall erosivity of the day, (2) more than one erosive events occurs within a day, in which case:

$$R_{day} = \sum_{i=1}^n E_i \cdot (I_{50})_i \quad (2)$$

where n is the number of events in the day, E_i and $(I_{50})_i$ are the total rainfall energy and the maximum 30 min intensity, respectively for the i th event, (3) only a part of a erosive event occurs in a day, in which case:

$$R_{day} = (E_{day})_d \cdot I_{50} \quad (3)$$

where $(E_{day})_d$ is the rainfall energy achieved by the part of rainfall that occurred in the d th day and I_{50} is the maximum 30 min intensity for the entire event. The fourth type of erosive event was not considered because only a few events were falling into this category which was not significant for R factor estimation. Note that if any event continues

from day 1 to day 2, it is considered as a separate day in this study.

The RUSLE model to calculate the average annual rainfall erosivity is:

$$R = \frac{1}{y} \sum_{j=1}^y \sum_{k=1}^{m_j} (EI_{50})_k \quad (4)$$

where y is the number of years of the record, m_j is the number of erosive events for a given year j , and EI_{50} is the rainfall erosivity index of a single event k . The R ($\text{MJ mm ha}^{-1} \text{h}^{-1} \text{y}^{-1}$) factor is the average value of the annual cumulative EI_{50} over the specified period. I_{50} is the maximum rainfall intensity in a 30 min period during the event (mm h^{-1}). The total storm kinetic energy (E) is calculated using the following equation (Renard & Freimund 1994):

$$E = \sum_{r=1}^p e_r v_r \quad (5)$$

where e_r is the unit rainfall kinetic energy for the r th 30 min in ($\text{MJ ha}^{-1} \text{mm}^{-1}$) and v_r is the rainfall volume (mm) during a time period r which is 30 min in this study. It is clear from Equation (5) that accurate estimation of R

depends on the accurate estimation of kinetic energy and it varies according to geographic locations. The kinetic energy and rainfall intensity relationship for any region can be determined from pluviograph or breakpoint data but for some areas, especially in developing countries, spatial and temporal coverage of pluviograph data is usually limited (Yu *et al.* 2001). Therefore, in the breakpoint data sparse environment, the developed e_r and rainfall intensity relationships which belong to similar climatic conditions would give better results. Various equations were used to calculate e_r for different climates (Salles *et al.* 2002) but the equation developed by Onaga *et al.* (1988) for Okinawa Island in Japan, with nearly similar wet and humid climatic conditions and previously used in Malaysia (Shamshad *et al.* 2008), has been chosen for this study in order to estimate the kinetic energy of rainfall. The relation is given as:

$$e_r = 0.0981 + 0.106 \times \log_{10} i_r \quad (6)$$

where i_r is the rainfall intensity during the time interval (mm h^{-1}). Rainfall intensity for a particular increment of a rainfall event is calculated using the relation:

$$i_r = \frac{\Delta v_r}{\Delta t_r} \quad (7)$$

where Δv_r is the change in rainfall volume (mm) and Δt_r is the duration of increment over which rainfall intensity is considered to be constant in hours (h). Furthermore, two most widely used kinetic energy and rainfall intensity relationships (Foster *et al.* 1981; Renard & Freimund 1994) were also considered to compute the kinetic energy. The equations are:

$$e_r = 0.29[1 - 0.72 \exp(-0.05i_r)] \quad (8)$$

$$e_r = 0.119 + 0.0873 \times \log_{10} i_r \quad (9)$$

The results of these two equations were compared with the results obtained from the proposed Equation (6) to show its effectiveness to estimate R in tropical climates of the study area.

Daily rainfall erosivity model

The model uses the power law equation originally proposed by Richardson *et al.* (1983):

$$R_{day} = \alpha P_d^\beta + \epsilon \quad (10)$$

where P_d (mm) is the daily rainfall depth, calculated from 30 min intensity data, α and β are empirical parameters and ϵ is a random, normally distributed error. Parameter estimation after the logarithmic transformation of Equation (10) is achieved by minimizing the sum of square errors. While the randomly distributed error (ϵ) was calculated by the equation:

$$\epsilon = \sum_{d=1}^D (E_o - E_p) \quad (11)$$

where E_o and E_p are the observed and predicted cumulative rainfall intensity for each day d , respectively and D is the total number of days of the study period. The model was developed for each month of the study period by including the precipitation limits of 0.1, 5 and 12.7 mm. The significance of selecting the limits will be discussed later under Results and discussion.

Model development and assessment

Out of the 55 stations, 15 stations were randomly selected as validation for model development and the remaining for calibration to develop model parameters. The cross-validation analysis was carried out to determine the difference between calibration and validation stations results. The process for which is as follows:

1. Regional parameter values (α and β) are estimated for 40 calibration stations (parameter set A) and for 15 validation stations (parameter set B) for each month.
2. Daily R factor is estimated for calibration stations using parameter set B and parameter and daily R factor is estimated for validation stations using parameter set A.
3. The estimated daily R factors so obtained are compared with the observed values and daily errors were calculated. Coefficient of determination (R^2) was also calculated during parameter estimation for each month.

In the proposed model, maximum intensity is not used. Hence, the error between observed and predicted values would be different in the events of less precipitation with high intensity than the events of high precipitation with low intensity. To evaluate the model efficiency, the validation statistics commonly used by Yu *et al.* (2001), Petkovšek & Mikoš (2004), Bennett *et al.* (2013) and Xie *et al.* (2016) for the goodness-of-fit and error statistics were selected. These are:

1. Nash and Sutcliffe efficiency coefficient (*NS*) (Nash & Sutcliffe 1970),
2. symmetric mean absolute percentage error (*SMAPE*),
3. mean absolute error (*MAE*) and mean bias error (*MBE*).

NS was calculated by Equation (12) which indicates how close the scatters of predicted values are to the line of best fit (Angulo-Martínez & Beguería 2009):

$$NS = 1 - \frac{\sum_{i=1}^N (O_i - P_i)^2}{\sum_{i=1}^N (P_i - P_m)^2} \quad (12)$$

where O_i and P_i are observed and predicted values of daily R respectively, P_m is the mean of observed R values and N is number of days. An efficiency of $NS = 1$ corresponds to a more accurate model while $NS = 0$ indicates the model predictions are as accurate as the mean of the observed data. An efficiency $NS < 0$ indicates that the observed mean is a better predictor than the model. *SMAPE* is an accuracy measure based on percentage which reflects the deviation of the predicted values from the observed one (Xie *et al.* 2016). It was calculated as follows (Armstrong 1985):

$$SMAPE = \frac{1}{N} \sum_{i=1}^N \left| \frac{O_i - P_i}{(O_i + P_i)/2} \right| \quad (13)$$

MBE and *MAE* were calculated as follows:

$$MBE = \frac{1}{N} \sum_{i=1}^N (P_i - O_i) \quad (14)$$

$$MAE = \frac{1}{N} \sum_{i=1}^N |P_i - O_i| \quad (15)$$

MBE is an indicator of prediction bias while *MAE* is a measure of average error (Angulo-Martínez & Beguería

2009). *NS*, *SMAPE*, *MBE* and *MAE* were calculated for each validation station during the model development.

RESULTS AND DISCUSSION

Data summary and event type determination

The thresholds of 0.1, 5.0 and 12.7 mm daily precipitations were taken individually as the minimum values of erosive event. For each threshold, the average annual rainfall value over a period of 10 years is taken for each station. Average annual rainfall for minimum limits of 0.1, 5.0 and 12.7 mm ranged from 1,885, 1,784 and 1,498 to 4,571, 4,458 and 4,140 mm, respectively. Average annual erosivity for the same limits varied from 10,264, 8,151 and 4,958 to 54,284, 48,301 and 39,938 MJ mm ha⁻¹ h⁻¹ y⁻¹, respectively.

For erosive events calculation, most of the days were of Type I in all the precipitation limits. A total of 84,283, 39,499 and 17,306 erosive events for 0.1, 5.0 and 12.7 mm respectively were used in the study; 24,402, 11,151 and 4,765 erosive events belong to the 15 validation stations while 59,881, 28,348 and 12,541 belong to the calibration stations for 0.1, 5.0, and 12.7 mm precipitation limits respectively. For the limit of 0.1 mm, taking the average percentage over 55 stations, 78.3% erosive events were found to be of Type I, followed by Type II (5.9%) and Type III (15.7%). For the 5.0 mm limit, the average percentages are: Type I (92.6%), Type II (4.1%) and Type III (3.3%). For 12.7 mm limit, the average percentages are: Type I (95.9%), Type II (2.4%) and Type III (1.8%). The high values of Type I for the limit of 0.1 mm is looking low in terms of the values of Type I for the limits of 5 and 12.7 mm because these values are in terms of percentage. An example to understand this calculation is shown in Table 3.

All stations have similar percentage distributions in terms of event types. The majority being of Type I at all stations shows the importance of individual events (Figure 2).

A decline of 44.6 and 54.6% was observed in Type I, when limits changed from 0.1 to 5.0 and 5.0 to 12.7 mm respectively. The percentage declines seen in Type II were 67.1 and 90.2 when the limits were increased from 0.1 to

Table 3 | An example of station S1 for the calculation of event's type in percentage

Precipitation limit (mm)	Type I		Type II		Type III		Total number of events
	No. of events	Percentage	No. of events	Percentage	No. of events	Percentage	
0.1	1,270	78.8	121	7.5	221	13.7	1,612
5.0	663	95.0	22	3.2	13	1.9	698
12.7	209	98.6	0	0.0	3	1.4	212

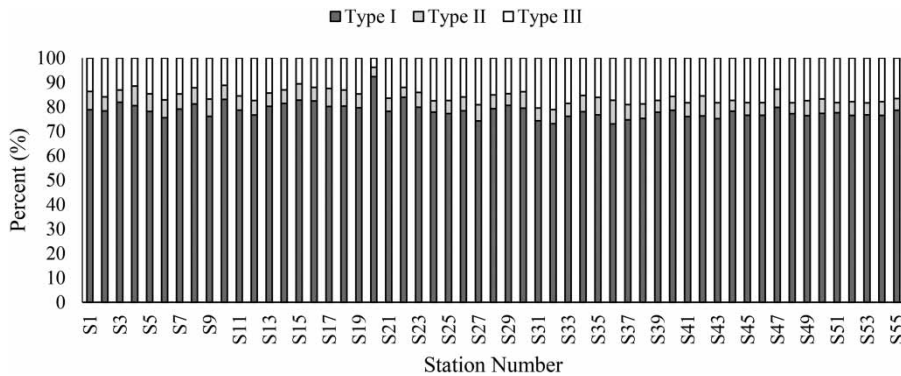


Figure 2 | Three types of erosive events for 55 stations. Type I belongs to an event which begins and finishes in the same day, Type II is when there is more than one event in a day and Type III is when only a part of an event occurs in a day.

5.0 and 5.0 to 12.7 mm respectively. Type III revealed smaller differences in percentage declines of 74.9 and 76.8% when the limits were raised from 0.1 to 5.0 and 5.0 to 12.7 mm. Since the decline in Type II and Type III events is more than Type I events, it shows that the area has small duration (Type I) events even for 5.0 and 12.7 mm limits (Table 4).

This indicates the individual power precipitation and high erosive capacity events within a short time interval that would increase the chances of flash flood.

It should also be noted that smaller events (less than 5.0 mm) which comes under 0.1 mm as the minimum precipitation limit, maintains the moisture in the soil and hence decreases the infiltration capacity of soil. This increases in the surface runoff which could raise the possibility of flash floods in the area.

Table 4 | The type of erosive events with their precipitation limits

Precipitation limit (mm)	Type I (%)	Type II (%)	Type III (%)
0.1	78.3	5.9	15.7
5.0	92.6	4.1	3.3
12.7	95.9	2.4	1.7

The month wise average of observed *R* factor values for all stations obtained by using Equations (6), (8) and (9) were compared to determine the difference between them. *R* factor values determined by using Equation (8) were slightly higher than the other two *R* factor values except in the month of September and November while the *R* factor values from Equations (6) and (9) showed similar results except in the month of November (Figure 3). The high *R* factor values were observed in the month of November

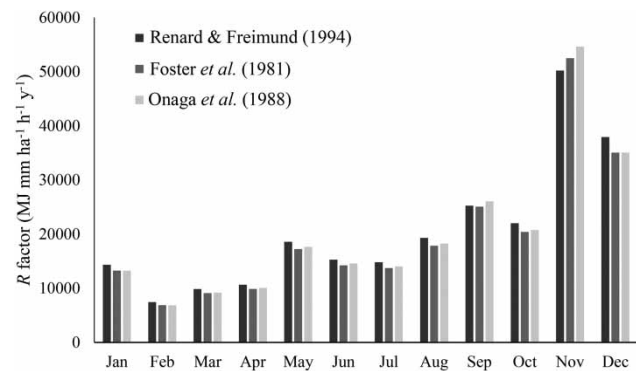


Figure 3 | The observed *R* factor comparison between three kinetic energy and rainfall intensity equations.

and December due to high rainfall with high intensity. As Equation (6) belongs to a wet and humid climate similar to the study area, it can be concluded that Equation (8) has showed slight overestimation for this particular climate while Equation (9) showed almost similar results.

Daily rainfall erosivity calculation and parameters estimation

Daily rainfall erosivity during the study period for each station was calculated as per the described methodology for the precipitation limits of 0.1, 5.0 and 12.7 mm. The data was then separated month wise. The distributions of average monthly rainfall erosivity and precipitation with all the three limits for all the stations are shown in Figures 4–6 which shows a similar pattern except for November and December which are showing the highest rainfall erosivity at the precipitation limit of 0.1 mm. The values have declined for 5.0 mm (23.2 and 30.5% respectively) and 12.7 mm limits (51.7 and 61.7% respectively). This shows that small events play an important role in maintaining soil moisture in November

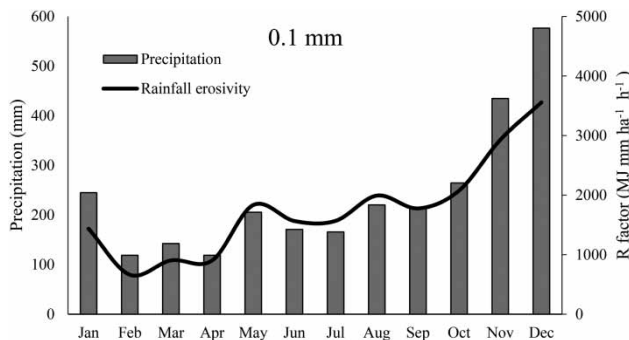


Figure 4 | Monthly distribution of R factor and precipitation limit of 0.1 mm.

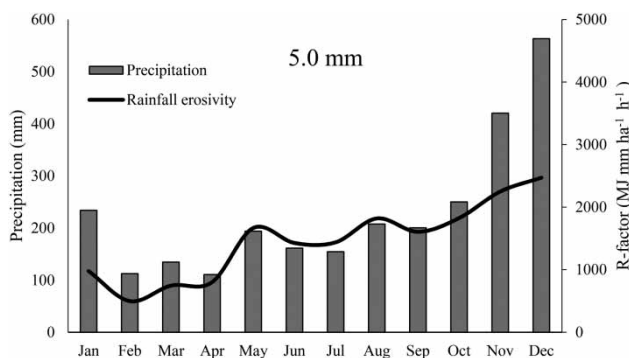


Figure 5 | Monthly distribution of R factor and precipitation limit of 5.0 mm.

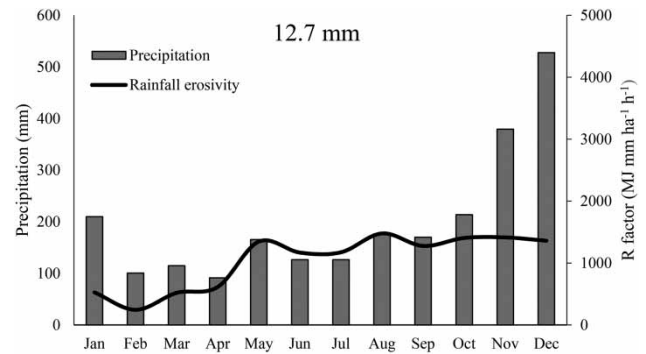


Figure 6 | Monthly distribution of R factor and precipitation limit of 12.7 mm.

and December which could result in high soil erosion during high intensity rainfall.

Minimum average precipitation was recorded in April with values of 127.6, 121.4 and 106.9 mm for 0.1, 5.0 and 12.7 mm respectively while December experienced the maximum with values of average precipitation, i.e. 579.3, 567.9 and 531.0 mm for 0.1, 5.0 and 12.7 mm respectively. November comes second in terms of high average precipitation, followed by February. February generally has low precipitation throughout the month with few events of high intensity rainfall in a short period of time. The maximum 30 min intensity values were observed in October (164 mm/h) followed by January (161 mm/h) and December (137.2 mm/h) which are very few in the study period.

The monthly α and β values for all stations were calculated using Equation (9) with precipitation limits of 0.1, 5.0 and 12.7 mm. Figures 7–9 show the box-and-whisker plots for the overall behaviour of the monthly distributions of α and β values for the precipitation limits of 0.1, 5.0 and 12.7 mm. The length of each box indicates the interquartile range with the median (middle line) and the whiskers are 25th and 75th percentiles.

Monthly distributions of β values were quite consistent for all the precipitation limits (0.1, 5.0 and 12.7 mm) while α values have large variations from January to February and November to December for precipitation limits of 5.0 and 12.7 mm and small variations for the limit of 0.1 mm for all the months. The average ranges of monthly α , β and R^2 values for all stations are shown in the supplementary data, Tables S1–S3 (available with the online version of this paper).

The variations in the monthly α and β values from January to February may be due to the lower occurrence of

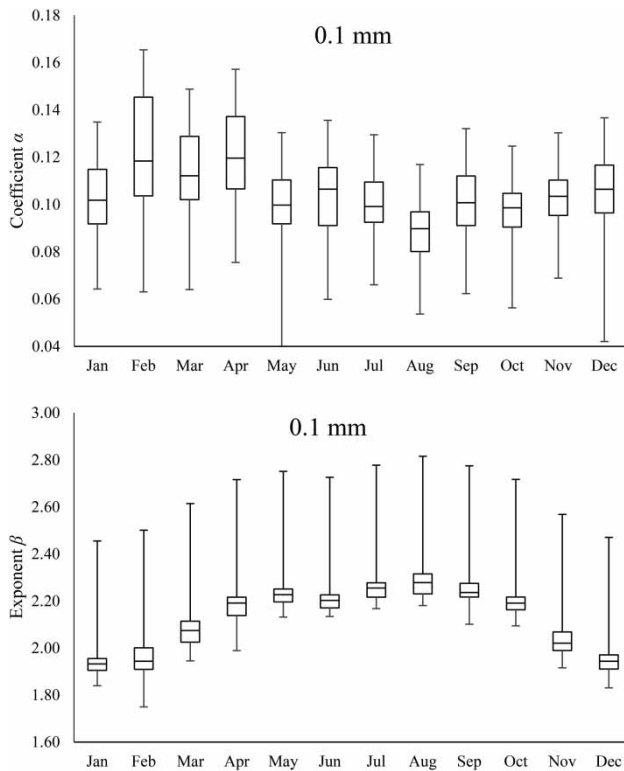


Figure 7 | Monthly distribution of exponent β and coefficient α from the power law relationship for precipitation limit of 0.1 mm.

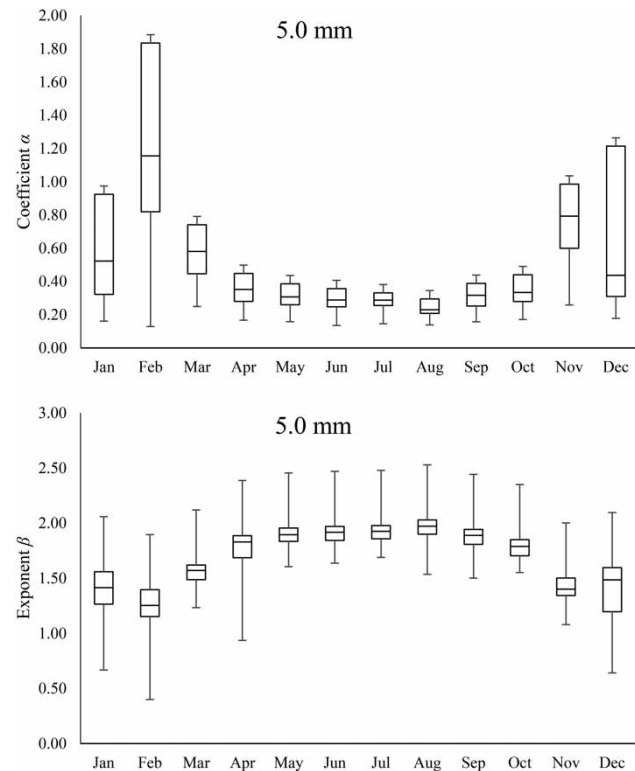


Figure 8 | Monthly distribution of exponent β and coefficient α from the power law relationship for precipitation limit of 5.0 mm.

precipitation with high I_{50} values. Both parameters show significant spatio-temporal behaviour within the study period. Many studies (Richardson *et al.* 1985; Bagarello & D'Asaro 1994; Yu & Rosewell 1996a; Petkovšek & Mikoš 2004; Xie *et al.* 2016) have minimized the influence of β by keeping β constant throughout the year or throughout the study period because of its greater influence as compared to α on the estimations and sensitivity to calibration errors (Angulo-Martínez & Beguería 2009). However, our results show that both α and β parameters vary significantly which supports the hypothesis that a model incorporating such variations could yield better results. Therefore, in this study, both the parameters will be used as variables for each month in the model development.

Model calibration and validation

Because of the spatial and temporal behaviour of parameters α and β , the best monthly values for each station were obtained by applying linear regression on values

from the same month for all the years and for all precipitation limits. For instance, all daily January R factor and precipitation values of 2005, 2006, 2007 and up to 2015 were separated and one best value of α and β for January were obtained by applying linear regression on this set of data for a particular station. The same procedure was applied for every month for each station so that every station obtained the best monthly values of α and β . In model calibration and validation, the so obtained best monthly parameters α and β values of 40 and 15 stations respectively for each month in the precipitation limit of 0.1, 5.0 and 12.7 mm were used in the daily rainfall erosivity estimation. In terms of under- and overestimation of the daily rainfall erosivity, both sets of parameters showed mixed results. At the precipitation limit of 0.1 mm, October showed the lowest average error (1.3% underestimation) while November experienced the highest average error of 48.3% in underestimation of the calibration (average 10% underestimation). In the validation, the lowest average error was found in September (1.1% overestimation) and the highest

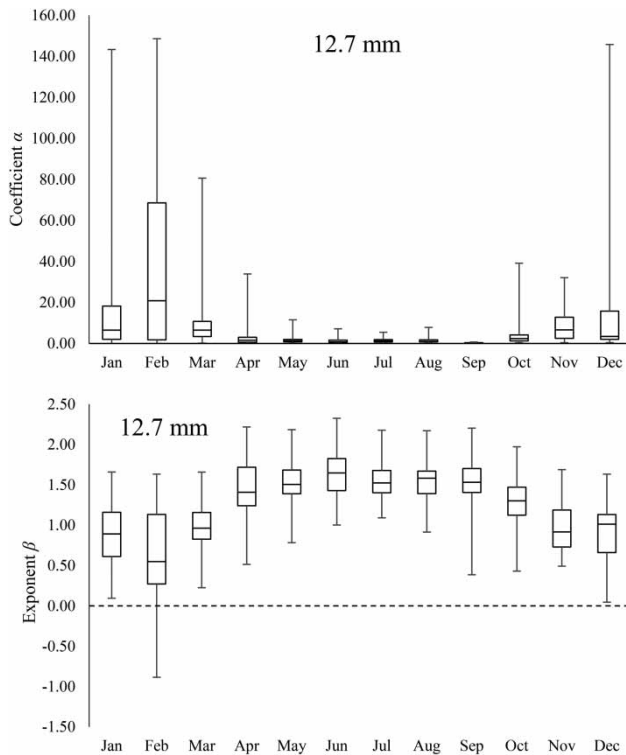


Figure 9 | Monthly distribution of exponent β and coefficient α from the power law relationship for precipitation limit of 12.7 mm.

in February (44.3% overestimation) with an overall average error of 4.7% overestimation. The average error of 161.8 and 305.1% underestimation in calibration, while 46.1 and

40.2% underestimation in validation, were calculated for the precipitation limit of 5 and 12.7 mm respectively. Large errors are due to the low precipitation and high I_{30} of some particular events. The closest estimation in validation was observed for February with 4.8% and January with 2.8% overestimation in the precipitation limits of 5 and 12.7 mm respectively. The results of monthly average values of parameters α and β with R^2 for validation stations for all precipitation limits are shown in Table 5.

Model assessment

The rainfall erosivity model (Equation (10)) generates reasonable approximations of average monthly R factor, especially for the precipitation limit of 0.1 mm. For validation stations, at precipitation limit 0.1 mm, the best average NS were for the months of July (0.88) followed by June (0.86) and May (0.85) while the best average $SMAPE$ were for August (1.32) followed by May (1.33) and July and September (1.35 for both). Worst average NS and $SMAPE$ for this limit was for November (0.28) and February (1.65) respectively. In the precipitation limits of 5.0 and 12.7 mm, the best and worst average values of NS was for August (0.57) and November (-5.06) and worst values for August (0.16) and December (-4.87). The model works well for both average MBE and MAE at precipitation limit

Table 5 | Monthly average regional parameter values of α and β with R^2 for 15 validation stations

Month	0.1 mm			5.0 mm			12.7 mm		
	α	β	R^2	α	β	R^2	α	β	R^2
Jan	0.1044	1.9329	0.93	0.6245	1.3673	0.66	9.1867	0.7744	0.37
Feb	0.1301	1.9296	0.94	1.1787	1.2484	0.70	29.548	0.4992	0.26
Mar	0.1194	2.0683	0.93	0.7159	1.4924	0.68	7.9305	0.9124	0.40
Apr	0.1179	2.1817	0.94	0.3621	1.8185	0.79	2.2038	1.3312	0.59
May	0.1006	2.2235	0.93	0.2826	1.9221	0.84	1.0075	1.5745	0.66
Jun	0.1075	2.1943	0.94	0.2926	1.9133	0.83	1.1672	1.5446	0.67
Jul	0.1053	2.2295	0.94	0.2779	1.9187	0.83	1.0447	1.5609	0.66
Aug	0.0888	2.2708	0.94	0.2572	1.9435	0.83	1.2088	1.5256	0.67
Sep	0.1002	2.2341	0.94	0.3169	1.8765	0.83	1.2349	1.5144	0.69
Oct	0.1033	2.1713	0.94	0.3365	1.8016	0.75	2.403	1.2941	0.51
Nov	0.1059	2.0195	0.93	0.8407	1.3861	0.65	9.5513	0.8203	0.36
Dec	0.0983	1.9439	0.93	0.6267	1.3755	0.68	7.9069	0.8091	0.39

0.1 mm, which is low for all the months except November to February. These high values are due to the role of high intensity rainfall in observed values for precipitation limit of 0.1 while for the limit of 5.0 and 12.7 mm, the very high values are due to less number of events with higher intensity. However, model efficiency for calibration stations was not good in comparison to validations stations. Overall, it can be concluded from the results that the model estimation

for validation stations was good with the precipitation limit of 0.1 mm (Tables 6 and 7 respectively). The monthly *NS*, *MBE*, *MAE* and *SMAPE* values of 15 validation stations for all precipitation limits are shown in the supplementary data (Tables S4–S7, available online).

The model efficiency in estimating seasonal variation and average annual erosivity of the other two aspects of *R* factor (Xie et al. 2016) were also checked for validation

Table 6 | Model efficiency results of validations stations

Months	NS			MBE			MAE			SMAPE			
	P(mm)	0.1	5.0	12.7	0.1	5.0	12.7	0.1	5.0	12.7	0.1	5.0	12.7
Jan		0.70	-1.14	-0.90	37.93	165.41	411.42	60.37	165.41	411.42	1.59	1.92	2
Feb		0.57	0.12	-2.89	107.36	255.77	417.10	126.08	255.77	417.10	1.65	1.86	2
Mar		0.68	0.00	-1.83	20.66	143.32	278.62	54.23	143.32	278.62	1.46	1.78	2
Apr		0.68	-0.04	-0.98	10.34	150.32	271.83	47.09	150.32	271.83	1.41	1.70	2
May		0.85	0.17	-0.77	4.52	152.99	267.35	37.86	152.99	267.35	1.33	1.67	2
Jun		0.86	-0.30	-1.18	3.18	146.22	268.20	36.91	146.22	268.20	1.39	1.58	2
Jul		0.88	0.01	-0.12	11.67	137.88	292.56	34.13	137.88	292.56	1.35	1.52	2
Aug		0.84	0.57	0.16	12.68	154.44	290.93	39.55	154.46	290.93	1.32	1.49	2
Sep		0.82	-0.85	-2.24	13.80	174.80	310.82	54.15	174.84	310.82	1.35	1.44	2
Oct		0.64	0.11	-0.38	20.29	146.45	282.44	56.90	146.49	282.44	1.36	1.43	2
Nov		0.28	-5.06	-2.24	-17.71	205.93	384.92	194.23	205.97	384.92	1.45	1.42	2
Dec		0.75	-1.72	-4.87	75.18	158.59	303.83	104.51	158.62	303.83	1.40	1.40	2

Table 7 | Model efficiency results of calibration stations

Month	NS			MBE			MAE			SMAPE		
	0.1 mm	5.0 mm	12.7 mm	0.1 mm	5.0 mm	12.7 mm	0.1 mm	5.0 mm	12.7 mm	0.1 mm	5.0 mm	12.7 mm
Jan	0.63	-3.54	-11.09	38.88	157.09	290.60	64.91	157.09	290.60	1.60	1.90	2.00
Feb	0.45	-3.62	-12.98	-6.80	204.16	248.41	163.77	204.16	248.41	1.62	1.83	2.00
Mar	0.68	-1.26	-4.62	21.17	138.39	263.65	59.01	138.39	263.65	1.46	1.77	2.00
Apr	0.76	0.44	-0.31	11.16	164.15	281.78	41.77	164.16	281.78	1.41	1.71	2.00
May	0.82	0.75	0.53	3.37	217.75	347.54	44.58	217.75	347.54	1.32	1.67	2.00
Jun	0.82	0.62	-0.14	-7.14	300.54	413.78	45.74	300.54	413.78	1.32	1.61	2.00
Jul	0.84	0.56	0.00	-2.09	181.72	318.39	39.78	181.72	318.39	1.34	1.50	2.00
Aug	0.86	0.72	0.26	5.21	204.04	333.72	42.94	204.06	333.72	1.31	1.53	2.00
Sep	0.84	-0.23	-3.84	-11.01	231.07	369.44	62.90	231.11	369.44	1.33	1.45	2.00
Oct	0.64	0.13	-1.45	11.64	198.11	315.32	61.12	198.22	315.32	1.38	1.43	2.00
Nov	-0.33	-15.68	-12.28	-108.34	181.66	282.95	300.69	181.72	282.95	1.43	1.38	2.00
Dec	0.09	-6.98	-9.05	-78.01	200.98	291.06	257.46	201.18	291.06	1.43	1.34	2.00

stations which were not good in comparison to event or daily *R* factor (Table 8).

As mentioned earlier, the precipitation limit 0.1 mm was considered for the proposed model because of the importance of small events in the study area which may be helpful in maintaining soil moisture and therefore high soil erosion will result from a high intensity rainfall. The proposed model using the precipitation limit of 0.1 mm is given as follows:

$$R_j = \frac{1}{Y} \sum_{y=1}^Y \sum_{i=1}^D (\alpha_j P_i^{\beta_j}) \tag{16}$$

where *j* is index of month, *D* is number of days in a month, *i* represents index of day, *y* is index of years and *Y* is number of years. The estimated average annual rainfall erosivity for the 15 validation stations using the model show a similar pattern to the observed rainfall erosivity (Figure 10).

The best prediction was from station number S9 in which the observed and estimated average annual *R* factor values were 15,874 and 15,641 MJ mm ha⁻¹ h⁻¹ y⁻¹ respectively. The worst prediction was made for station number S21 in which the observed and estimated average annual values were 19,352 and 15,692 MJ mm ha⁻¹ h⁻¹ y⁻¹

respectively. The average error for all the validation stations is found as 7.8% overestimation.

The monthly α and β values for the power law function were highly correlated (Figure 11) and the relationship of exponent β and coefficient α from the model of Equation (9) was derived from the 180 months of data (from the 15 validation stations) which is given by:

$$\log(\alpha) = 1.22 - 0.94 \times \beta \quad R^2 = 0.91 \tag{17}$$

However, Equation (17) is not similar to those from previous studies, such as Yu (1998), Zhang et al. (2002) and Xie et al. (2016), because of climatic differences. Richardson et al. (1983) suggested the average value of β as 1.81 because no discernible spatial patterns in variation of β was found between stations. In this study, as discussed above, the spatio-temporal variation was found in the values of β . The average value of β for this study is 14.5% higher than the proposed value (1.81) while the average value of α (0.11) is 74% lower than the proposed value of α (0.41) for the warm season (Richardson et al. 1983) and 7.4% lower than the average value of α (0.18) for the cool season. While previous studies assumed that the coefficient β remained constant throughout the year (Angulo-Martínez & Beguería 2009),

Table 8 | Model efficiency results of average annual and seasonal rainfall erosivity for validation stations

Year	NS			MBE			MAE			SMAPE			
	P(mm)	0.1	5.0	12.7	0.1	5.0	12.7	0.1	5.0	12.7	0.1	5.0	12.7
2005		0.42	0.37	0.47	15.61	5,371.96	9,722.13	89.59	6,725.50	9,722.13	1.50	1.00	2.00
2006		0.28	0.33	0.45	-136.80	8,248.39	17,516.83	209.03	9,812.16	17,516.83	1.49	0.99	2.00
2007		0.52	0.33	0.44	35.75	5,392.97	11,070.50	90.55	6,859.10	11,070.50	1.43	0.99	2.00
2008		0.53	0.33	0.45	38.98	5,043.86	11,208.14	89.71	6,520.80	11,208.14	1.43	0.99	2.00
2009		0.56	0.33	0.44	65.01	7,141.39	13,472.05	120.31	8,597.15	13,472.05	1.44	1.03	2.00
2010		0.51	0.38	0.49	14.65	3,740.68	8,454.43	63.91	5,214.65	8,454.43	1.48	0.98	2.00
2011		0.52	0.33	0.45	40.01	4,851.97	10,205.66	90.68	6,378.75	10,205.66	1.44	0.97	2.00
2012		0.46	0.30	0.45	27.92	4,333.47	9,478.69	91.53	5,954.89	9,478.69	1.41	1.02	2.00
2013		0.45	0.41	0.53	49.47	5,823.86	11,501.69	95.41	7,284.37	11,501.69	1.46	1.00	2.00
2014		0.53	0.25	0.36	107.97	11,007.90	18,846.00	167.82	12,324.98	18,846.00	1.44	1.02	2.00
2015		0.34	0.38	0.51	-4.92	1,937.69	5,892.87	55.86	3,588.59	5,892.87	1.46	0.98	2.00
Season													
Nov–Feb		0.66	0.29	0.43	74.30	15,623.36	27,133.93	107.54	15,623.36	27,133.93	1.50	1.99	2.00
Mar–Oct		-1.49	0.42	0.53	-48.65	3,071.55	4,374.99	57.13	3,071.55	4,374.99	1.49	1.98	2.00

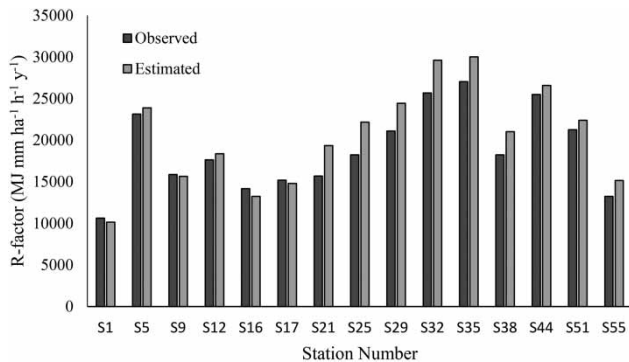


Figure 10 | Comparison between observed rainfall erosivity with estimated rainfall erosivity for the proposed model which have precipitation limit of 0.1 mm at 15 validation stations.

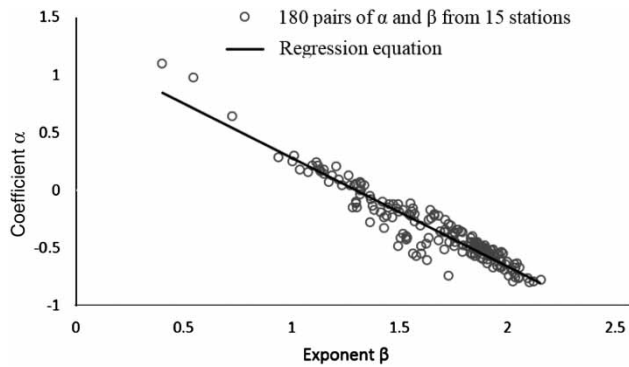


Figure 11 | Relationship between coefficient α and exponent β by Equation (10) for 180 month/station combinations used from 15 validation stations.

the results showed monthly variation of β with standard deviation of 0.12. The lower values of α (with standard deviation of 0.01) against the proposed values of α for the warm and cool season indicates less influence of variation of coefficient α throughout the year on the proposed model, whereas the variation in the values of β throughout the year has more influence on R factor estimation due to its higher standard deviation than α which may be the cause of high rainfall erosivity in the area. Furthermore, the influence of exponent β is greater than that of coefficient α (Angulo-Martínez & Beguería 2009).

To check the results of the proposed model for this study, rainfall erosivity was estimated for all the districts of the area in which the number of stations range from 16 (Gua Musang) to 1 (Machang) (Figure 1). The previously developed model (Yu et al. 2001) was also included to compare the results of the proposed model. From the proposed

model, the best estimation of average annual R factor was 16,773 MJ mm ha⁻¹ h⁻¹ y⁻¹ (observed) and 16,746 MJ mm ha⁻¹ h⁻¹ y⁻¹ (estimated) for the district Gua Musang (16 stations) while the worst prediction was for Machang (one station). The overall average error of the proposed model is 8.2% overestimation while the previously developed model was estimated with 32.8% overestimation as shown in Figure 12.

It was found that 15% overestimation from the area are due to overestimation of the average R factor in February (40%), November (30%) and December (15%) because of high precipitation in November and December, but high rainfall intensity in February each year. The overall results of the proposed model and previously developed model for the study area are shown in Table 9.

It can be concluded that the proposed model works well for all the months except February, November and December in estimating the average annual R factor.

Although the study was carried out for Kelantan state of Peninsular Malaysia since the conditions used are for a general tropical climate region, the proposed model may be applied in any other region of similar climatic conditions. The study for the area of similar climatic conditions should be carried out by using the same average monthly α and β values as given in Table 5 with daily precipitation limits greater than 0.1 mm to check the results of estimating average annual rainfall erosivity. The limitation of the model is that it depends on the precipitation values while the observed R factor depends on

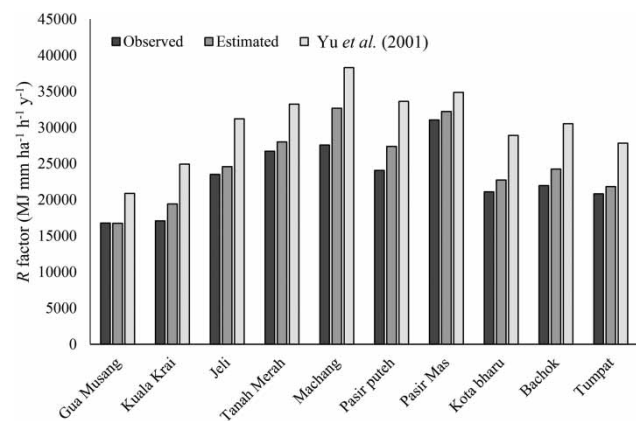


Figure 12 | Rainfall erosivity estimation by the proposed model and previously used model of all the districts of study area.

Table 9 | The overall results of proposed model and Yu et al. (2001) model in estimation of *R* factor for study area

States	Observed (MJ mm ha ⁻¹ h ⁻¹ y ⁻¹)	Estimated (MJ mm ha ⁻¹ h ⁻¹ y ⁻¹)	Error (%)	Yu et al. (2001) (MJ mm ha ⁻¹ h ⁻¹ y ⁻¹)	Error (%)
Gua Musang	16,772	16,746	-0.2	20,883	24.5
Kuala Krai	17,080	19,428	13.7	24,929	45.9
Jeli	23,519	24,583	4.5	31,207	32.6
Tanah Merah	26,719	28,013	4.8	33,232	24.3
Machang	27,576	32,664	18.4	38,299	38.8
Pasir Puteh	24,057	27,388	13.8	33,629	39.7
Pasir Mas	31,054	32,226	3.7	34,872	12.2
Kota Bharu	21,096	22,733	7.7	28,904	37.0
Bachok	21,968	24,255	10.4	30,533	38.9
Tumpat	20,820	21,827	4.8	27,844	33.7
Average	23,067	24,987	8.2	30,434	32.8

both the precipitation and the intensity of the rainfall. The proposed model can overestimate for values of high daily precipitation with low rainfall intensity and vice versa. Future work thus may include the improvement of this model to incorporate the effects of daily intensity of rainfall.

How to apply the proposed model to other places

The *R* factor for the proposed model can be calculated on a daily, monthly and annual basis. To apply the proposed model to other places, only daily precipitation data is needed. The regional parameter (α and β) values of 0.1 mm precipitation limit of all months will be used in *R* factor calculation which are given in Table 5. Examples of daily, monthly, annual and average annual *R* factor calculations from the proposed model are as follows:

1. *For daily R factor calculations:* For instance, to calculate the *R* factor of 1st January, the 1st January precipitation value and the January regional parameters values are put in Equation (16).
2. *For monthly R factor calculations:* For instance, to calculate the *R* factor for the month of February of a year, daily *R* factor of each day of this month are calculated (on similar lines as given in (i)) and summed up to obtain the monthly *R* factor of February for the specified year. For average monthly *R* factor calculations, the average of

monthly *R* factor values of February for a specified number of years will be taken.

3. *For annual R factor calculations:* The monthly calculations of all the months of a year will be calculated as per the procedure of (ii) with their respective regional values from Table 5. After monthly calculation, the sum of all the months will be the annual *R* factor.
4. *For average annual R factor calculations:* Suppose *Y* number of years are included to calculate the average annual *R* factor. The average of *R* factor values of January for *Y* number of years will be taken. Similarly, the average of February, March and so on up to December *R* factor will be taken. Finally, the average monthly *R* factor values will be summed up to calculate the average annual *R* factor.

CONCLUSIONS

A total of 84,283, 39,499 and 17,306 erosive events for 0.1, 5.0 and 12.7 mm respectively from 30 min resolution rainfall data from 55 rain gauges located in the northeastern part of Peninsular Malaysia were used to analyse the empirical relationship between rainfall erosivity and daily precipitation. The study shows the dominance of individual (Type I) events in a day in the area which are 78.3, 92.5 and 95.8% for precipitation limits of 0.1, 5.0 and 12.7 mm respectively while the remaining days

with erosive rainfall are the parts of Type II and Type III erosive events.

The values of coefficients α and β of the power law relationship were calculated by minimizing the sum of minimum square error and the spatio-temporal variations of both α and β values were found. Therefore, in the model development, α and β were taken as variables instead of constant values. Validation was carried out using 15 out of 55 stations using the average values of α and β for each month. R^2 of the validated stations ranged from 0.93 to 0.94, 0.64 to 0.84 and 0.41 to 0.70 for precipitation limits of 0.1, 5.0 and 12.7 mm respectively for all the months. During the model development, mixed results were obtained including both the overestimations and the underestimations of the rainfall erosivity for all precipitation limits. On the basis of the number of individual events, *NS*, *SMAPE*, *MBE* and *MAE* results, the 0.1 mm precipitation limit was selected for the proposed model. The average value of α was found to be lower than the average value of α for warm and cool season (proposed by a previous study) which indicates less significance of α as compared to β in the estimation of rainfall erosivity. The average value of β was found to be higher than that proposed in a previous study which may be the cause of high rainfall erosivity estimation in the area. Furthermore, the proposed model was compared to the previously developed model for similar climatic conditions and the estimation results from the proposed model were found to be better for most of the months, except for a little overestimation in February, November and December.

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REFERENCES

- Al-Ahmadi, K. & Al-Ahmadi, S. 2013 [Rainfall-altitude relationship in Saudi Arabia](#). *Adv. Meteorol.* **2013**, 1–14.
- Ali, J. 2015 Development of daily rainfall erosivity model for Dehradun, Uttarakhand, India. *Int. J. Curr. Eng. Technol.* **5** (5), 3222–3227.
- Angulo-Martínez, M. & Beguería, S. 2009 [Estimating rainfall erosivity from daily precipitation records: a comparison among methods using data from the Ebro Basin \(NE Spain\)](#). *J. Hydrol.* **379** (1), 111–121.
- Armstrong, J. S. 1985 *Long-range Forecasting: From Crystal Ball to Computer*, 2nd edn. Wiley, New York.
- Bagarello, V. & D'Asaro, F. 1994 [Estimating single storm erosion index](#). *Trans. ASAE* **37** (3), 785–791.
- Bennett, N. D., Croke, B. F., Guariso, G., Guillaume, J. H., Hamilton, S. H., Jakeman, A. J., Marsili-Libelli, S., Newham, L. T., Norton, J. P., Perrin, C. & Pierce, S. A. 2013 [Characterising performance of environmental models](#). *Environ. Model. Softw.* **40**, 1–20.
- Bullock, P., Dejong, E. & Kiss, J. 1990 An assessment of rainfall erosion potential in southern Saskatchewan from daily rainfall records. *Can. Agric. Eng.* **32** (1), 17–24.
- de Santos Loureiro, N. & de Azevedo Coutinho, M. 2001 [A new procedure to estimate the RUSLE EI 30 index, based on monthly rainfall data and applied to the Algarve region, Portugal](#). *J. Hydrol.* **250** (1), 12–18.
- Diodato, N. & Bellocchi, G. 2007 [Estimating monthly \(R\) USLE climate input in a Mediterranean region using limited data](#). *J. Hydrol.* **345** (3), 224–236.
- Ferro, V., Porto, P. & Yu, B. 1999 [A comparative study of rainfall erosivity estimation for southern Italy and southeastern Australia](#). *Hydrol. Sci. J.* **44** (1), 3–24.
- Foster, G. R., McCool, D. K., Renard, K. G. & Moldenhauer, W. C. 1981 Conversion of the universal soil loss equation to SI metric units. *J. Soil Water Conserv.* **36** (6), 355–359.
- Goldreich, Y. 1994 [The spatial distribution of annual rainfall in Israel – a review](#). *Theor. Appl. Climatol.* **50** (1–2), 45–59.
- Kamaludin, H., Lihan, T., Ali Rahman, Z., Mustapha, M., Idris, W. & Rahim, S. 2013 [Integration of remote sensing, RUSLE and GIS to model potential soil loss and sediment yield \(SY\)](#). *Hydrol. Earth Syst. Sci. Discuss.* **10** (4), 4567–4596.
- Karnieli, A. & Osborn, H. B. 1988 Factors affecting seasonal and annual precipitation in Arizona. In: *Paper Presented at the Hydrology and Water Resources in Arizona and the Southwest*. Arizona-Nevada Academy of Science, Tucson, Arizona, USA, pp. 7–18.
- Leow, C. S., Ghani, A. A., Zakaria, N. A. & Abidin, R. Z. 2011 [Development of rainfall erosivity isohyet map for Peninsular](#)

- Malaysia. In: *3rd International Conference on Managing Rivers in the 21st Century: Sustainable Solutions for Global Crisis of Flooding, Pollution and Water Scarcity*. River Engineering and Urban Drainage Research Centre (REDAC), Universiti Sains Malaysia, Penang, Peninsular Malaysia, pp. 748–756.
- Masseran, N. & Razali, A. M. 2016 Modeling the wind direction behaviors during the monsoon seasons in Peninsular Malaysia. *Renew. Sustain. Energy Rev.* **56**, 1419–1430.
- Michaud, J., Auvine, B. A. & Penalba, O. C. 1995 Spatial and elevational variations of summer rainfall in the southwestern United States. *J. Appl. Meteorol.* **34** (12), 2689–2703.
- Mikoš, M., Jošt, D. & Petkovšek, G. 2006 Rainfall and runoff erosivity in the alpine climate of north Slovenia: a comparison of different estimation methods. *Hydrol. Sci. J.* **51** (1), 115–126.
- Nash, J. E. & Sutcliffe, J. V. 1970 River flow forecasting through conceptual models part I – A discussion of principles. *J. Hydrol.* **10** (3), 282–290.
- Nearing, M. A., Unkrich, C. L., Goodrich, D. C., Nichols, M. H. & Keefer, T. O. 2015 Temporal and elevation trends in rainfall erosivity on a 149 km² watershed in a semi-arid region of the American Southwest. *Int. Soil Water Conserv. Res.* **3** (2), 77–85.
- Ochoa-Cueva, P., Fries, A., Montesinos, P., Rodríguez-Díaz, J. A. & Boll, J. 2015 Spatial estimation of soil erosion risk by land-cover change in the Andes of Southern Ecuador. *Land Degrad. Dev.* **26** (6), 565–573.
- Onaga, K., Shirai, K., Yoshinaga, A. & Rimwanich, S. E. 1988. *Rainfall Erosion and how to Control its Effects on Farmland in Okinawa*. Land Conservation for Future Generations. Department of Land Development, Bangkok, pp. 627–639.
- Petkovšek, G. & Mikoš, M. 2004 Estimating the R factor from daily rainfall data in the sub-Mediterranean climate of southwest Slovenia/Estimation du facteur R à partir de données journalières de pluie dans le climat sub-méditerranéen du Sud-Ouest de la Slovénie. *Hydrol. Sci. J.* **49** (5), 869–877.
- Renard, K. G. & Freimund, J. R. 1994 Using monthly precipitation data to estimate the R-factor in the revised USLE. *J. Hydrol.* **157** (1), 287–306.
- Renard, K. G., Foster, G. R., Weesies, G., McCool, D. & Yoder, D. 1997 *Predicting Soil Erosion by Water: A Guide to Conservation Planning with the Revised Universal Soil Loss Equation (RUSLE)*, Vol. 703. US Government Printing Office, Washington, DC, pp. 1–403.
- Richardson, C., Foster, G. & Wright, D. 1983 Estimation of erosion index from daily rainfall amount. *Trans. ASAE* **26** (1), 153–0156.
- Salles, C., Poesen, J. & Sempere-Torres, D. 2002 Kinetic energy of rain and its functional relationship with intensity. *J. Hydrol.* **257** (1), 256–270.
- Shamshad, A., Azhari, M., Isa, M., Hussin, W. W. & Parida, B. 2008 Development of an appropriate procedure for estimation of RUSLE EI 30 index and preparation of erosivity maps for Pulau Penang in Peninsular Malaysia. *Catena* **72** (3), 423–432.
- Tan, J., Jakob, C., Rossow, W. B. & Tselioudis, G. 2015 Increases in tropical rainfall driven by changes in frequency of organized deep convection. *Nature* **519** (7544), 451–454.
- Wischmeier, W. H. 1984 The USLE: some reflections. *J. Soil Water Conserv.* **39** (2), 105–107.
- Wischmeier, W. H. & Smith, D. D. 1978 *Predicting Rainfall Erosion Losses – A Guide to Conservation Planning*. USDA, Science and Education Administration, Hyattsville, Maryland, USA.
- Xie, Y., Yin, S. Q., Liu, B. Y., Nearing, M. A. & Zhao, Y. 2016 Models for estimating daily rainfall erosivity in China. *J. Hydrol.* **535**, 547–558.
- Yu, B. 1998 Rainfall erosivity and its estimation for Australia's tropics. *Aust. J. Soil Res.* **36** (1), 143–166.
- Yu, B. & Rosewell, C. 1996a Rainfall erosivity estimation using daily rainfall amounts for South Australia. *Soil Res.* **34** (5), 721–733.
- Yu, B. & Rosewell, C. 1996b Technical notes: a robust estimator of the R-factor for the universal soil loss equation. *Trans. ASAE* **39** (2), 559–561.
- Yu, B., Hashim, G. & Eusof, Z. 2001 Estimating the R-factor with limited rainfall data: a case study from Peninsular Malaysia. *J. Soil Water Conserv.* **56** (2), 101–105.
- Zhang, W. B., Xie, Y. & Liu, B. Y. 2002 Rainfall erosivity estimation using daily rainfall amounts. *Sci. Geogr. Sinica* **22** (6), 705–711.

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