Flow-through electrosorption process for removal of 2,4-D pesticide from aqueous solutions onto activated carbon cloth fixed-bed electrodes

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ABSTRACT

Wastewater treatment systems have great importance in dealing with increasing environmental pollution. In this study, a specially designed and constructed flow-through electrochemical cell was used to enhance the electrosorptive removal capacity of 2,4-Dichlorofenoxyacetic acid (2,4-D) pesticide from aqueous solutions onto high area activated carbon cloth (ACC) fixed-bed electrodes. The change in concentration of 2,4-D during the electrosorption process was followed by an online UV–Vis spectrophotometric system. Effects of operational parameters such as volumetric flow rate, applied potential and existence of Na2SO4 salt on electrosorption of 2,4-D were examined. Optimum values were found to be 10 mL·min⁻¹ for volumetric flow rate and +900 mV for the applied potential to polarize ACC. Maximum capacity of 729 mg·gACC⁻¹ has been achieved for removal of 2,4-D pesticides.

Key words | 2, 4-D pesticide, activated carbon cloth, electrosorption, flow-through, water treatment

INTRODUCTION

Releasing various organic and inorganic pollutants into the ecosystems has been exponentially increased during the past several decades due to growing social civilization, industrialization and technology (Ghodbane et al. 2008; Michalski & Ficek 2016). Dyes, pesticides and acids containing charged or ionizable groups in their molecules are considered as important water pollutants. Separation techniques such as precipitation, adsorption and filtration or destructive techniques including ozonation and electrochemical reactions are extensively used in removal of pollutants from wastewaters (Sun et al. 2016). Adsorption is probably the most widely used one among these. However, the adsorption process has major drawbacks, such as slow removal rate originating from the diffusion limitations and short lifetime of most adsorbents due to low regeneration capacities (Niu & Conway 2003; Bayram & Ayranci 2010). On the other hand, limitations of adsorption can be eliminated by applying certain potential or current to high surface area electrodes. This potential-induced adsorption is generally termed as electrosorption which appears to be a promising technique for the removal of pollutants more effectively, especially by utilizing high specific surface area carbon electrodes (Ania & Béguin 2007). The basic principle in electrosorption is that the electrical double layer at the electrode surface is charged and/or discharged. No Faradaic process takes place in electrosorption. Another important advantage of electrosorption over usual adsorption process is the possibility of in-situ regeneration of the adsorbent without consuming much energy (Duan et al. 2013). Besides, performance of electrosorption process can also be affected by the characteristics and forms of electroadsorbent used in electrosorption. The diffusion limitation can be minimized with the use of electrosorbents having quasi-three-dimensional structure such as cloth, foam, felt and some other porous materials (Peng et al. 2015). This increases the overall rate of adsorption/electrosorption process. Activated carbon cloth (ACC), one of such quasi-three-dimensional adsorbent materials, has the additional advantage of mechanical integrity so that it can be designed as a stable electrode to carry out electrosorption processes for the removal of pollutants from wastewaters (Ania & Béguin 2007; Bayram & Ayranci 2012; Gineys et al. 2017).

The type of reactor used for treatment of wastewaters is another important factor that affects the removal efficiency. Batch type reactors are often used for laboratory studies but are less convenient for practical applications. Flow-through
fixed-bed reactor systems improve the mass transport of pollutants which are usually present at low concentrations in water streams. Additionally, fixed-bed columns are commonly used in industry due to their simple operation. Ban et al. (1998) studied the treatment of industrial wastewaters with the application of electrosorption/electrodesorption process using granular activated carbon pack-bed electrodes. In their study, electrosorption isotherms of aromatic organic compounds were derived under various conditions and compared with the ones derived from flow-through column systems. Two flow-through electrochemical cell designs were proposed by Ban et al. (1998). They found carbon fibers to be more effective than granular activated carbons as fixed-bed electrodes in removal of aromatic organic molecules. Woodard et al. (1986) reported a study about the use of flow-through system with carbon fiber electrodes for electrosorption of low molecular weight organic molecules, amino acids, a peptide and a protein.

In the present study, a specially designed flow-through electrochemical cell was used to enhance removal efficiency of organic molecules from aqueous solutions onto high specific surface area ACC fixed-bed electrodes by electrosorption. 2,4-Dichlorofenoxyacetic acid pesticide (2,4-D) was selected as the model pollutant molecule due to its dense usage in agriculture. 2,4-D concentration was followed by on-line UV-Vis spectrophotometric method. Operational parameters such as volumetric flow rate, applied potential and the presence of Na2SO4 were investigated for their effects on electrosorption.

The originality of the present work arises mainly from the use of specially designed flow-through electrochemical cell, inclusion of single piece ACC as fixed-bed electrode in this cell, the overall small size of the flow-through electrochemical cell and finally monitoring the pollutant concentration by online spectrophotometric method.

**EXPERIMENTAL SECTION**

**Materials**

The ACC material used as fixed-bed electrode was purchased from Spectra Corp. (MA, USA) with a code of Spectracarb 2225. The ACC was washed repeatedly with warm deionized water before it was used in the electrosorption process. Washing procedure, physicochemical and electrochemical properties of ACC were described previously (Bayram & Ayranci 2010). 2,4-D and Na2SO4 were purchased from Aldrich with a mass fractional purity of at least 0.99 and used without further purification. Ultra pure water was produced from 18.2 MΩ Milli-Q UV (Millipore) water system.

**Description of flow-through electrolytic cell**

Electrosorption experiments were carried out by using the specially designed flow-through electrolytic cell which is schematically shown in Figure 1. The main body of the electrolytic cell was constructed from Teflon material (I). The flow channel drilled through the Teflon body has an inner diameter of 1.5 cm. There is a stainless steel mesh half-way through the channel acting as base for fixed-bed electrode and providing a homogeneous potential distribution upon establishing the electrical contact with ACC. A threaded Teflon plug (II) having a hole of 0.8 cm was screwed through the flow channel. In this way, two pieces of circular ACC are pressed between the plug and stainless steel mesh. The total mass of ACC pieces was 40 ± 0.2 mg. The pressed ACC in contact with a Pt wire acted as the fixed-bed working electrode (WE). The reference electrode (RE) was a Ag/AgCl electrode from bioanalytical systems (BAS, MF2030, USA). It was introduced into the channel through a hole in a perpendicular position. An O-ring prevented any leakage from the hole of RE. A piece of coiled Pt wire was fitted to outlet part (III) of the cell as a counter electrode (CE).

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**Figure 1** | Scheme of flow-through electrolytic cell. Teflon body (I), threaded Teflon plug (II) and outlet part (III).
Procedure for the on-line spectrophotometric analysis of electrosorption

The diagram in Figure 2 illustrates the layout for the continuous flow electrosorption process with an on-line spectrophotometric analysis system.

Besides the specially designed flow-through electrolytic cell, the system contains a UV-Vis spectrophotometer (Varian Cary 100) with a quartz flow cell (Helma), a peristaltic pump and a potentiostat/galvanostat (Gamry Instruments Inc.). The adsorbate solution is placed in a beaker over a magnetic stirrer in this system and it flows first to the electrosorption cell then to the quartz flow cell of the spectrophotometer through a silicon tubing (0.2 cm i.d.) with the help of the peristaltic pump. Flow-through electrolytic cell was operated in up-flow plug mode. ACC fixed bed electrode was provided by the potentiostat/galvanostat through the connection of three electrodes of the electrolytic cell. A flow rate of 10 mL·min⁻¹ allowed the solution to travel in 1.5 s from original beaker to the electrolytic cell and in about 3 s to the spectrophotometer cell. The total volumes were about 2 mL for tubings and 4 mL for the flow channel. The temperature for all experiments was 25°C. On-line absorbance measurements, leading to concentration determinations, were carried out at the selected wavelength of 280 nm for 2,4-D. It is to be noted that a control experiment without any 2,4-D was also carried out and no signal was received from the spectrophotometer originating from ACC or medium.

RESULTS AND DISCUSSION

Electrosorptive behavior of 2,4-D

Electrosorption is a non-Faradaic process. Thus, it is important to check the electrochemical stability of an adsorbate within the polarization potential range studied. In order to determine the electrochemical stability window and avoid the electrochemical by-products of 2,4-D, cyclic voltammetric studies were carried out in aqueous solutions of 0.01 M Na₂SO₄ with and without 0.01 M 2,4-D at a potential scan rate of 5 mV·s⁻¹ using Ag/AgCl as RE, 20±1 mg ACC as WE and a Pt wire as CE. Voltammograms are shown in Figure 3.

The absence of any noticeable change in the voltammograms upon inclusion of 0.01 M 2,4-D shows the capacitative behavior of ACC originating from the electrosorption/desorption of 2,4-D.

Batch operation mode is more convenient for observing the adsorption/electrosorption behaviors of an adsorbate. In this study, electrosorption of 20 mL 2.1×10⁻⁴ M 2,4-D in 0.01 M Na₂SO₄ solution onto 20±1 mg ACC was carried out using a specially designed V-shaped electrolytic cell with in-situ UV-vis concentration measurements as described in our previous studies (Ayranci & Bayram 2005; Bayram & Ayranci 2010). First, adsorption data were recorded on open circuit (OC) condition until equilibrium (first 85 min), followed by electrosorption under +900 mV polarization for the next 50 min. Results are shown in Figure 4.

It is seen that positive polarization of ACC by applying +900 mV potential causes an increase in adsorption, deduced from the further decrease in concentration of 2,4-D after OC adsorption. In the case of OC adsorption, solution is acidic (pH 4.28) due to the partial ionization of
2,4-D. This pH is smaller than pH_PZC of ACC and causes the carbon surface to be positively charged (Bayram & Ayranci 2014). On the other hand, analytical calculations based on pKa (2.77) of 2,4-D showed that at an initial concentration of $2.0 \times 10^{-4}$ M and natural pH of 4.65 in 0.01 M Na$_2$SO$_4$ solution, 2,4-D is found predominantly in anionic form (98% anionic, 2% neutral). So, the electrostatic attractions between these anionic 2,4-D species and positively charged surface as well as the dispersion interactions between 2,4-D molecules and ACC surface are possibly responsible from the observed OC adsorption behavior. After polarization, positive charge density of ACC surface is further increased, resulting in rearrangement of water dipoles and strength of their electrostatic adsorption (Niu & Conway 2003). So, electrostatic interaction between anionic form of 2,4-D and ACC surface is mainly responsible from the electrosorptive, as well as OC adsorptive behavior.

Potential dependence of electrosorption

Investigation of the influence of applied potential on the electrosorption rate and capacity is crucial for the accurate design and modeling of electrosorption processes. For this purpose, a series of experiments on electrosorption kinetics were carried out until equilibrium by applying varying potentials at room temperature. The initial 2,4-D concentration of about $2.0 \times 10^{-4}$ M in 0.01 M Na$_2$SO$_4$ solution, ACC electrode mass of 40.0 ± 0.2 mg and volumetric flow rate of 10 mL·min$^{-1}$ were kept constant in this series in order to see the effect of mainly the applied potential. The effect of applied potential on the rate and extent of adsorption can be seen from Figure 5. OC adsorption data was also included in this figure for comparison.

It can be clearly seen that polarization causes dramatic changes in the rate and extent of adsorption. In electrosorption process, the charge of ACC is determined by the direction and magnitude of applied potential. The positive charge loaded onto ACC is expected to be the highest at +900 mV and the influence of applied potential on electrosorption is observed to be the highest at this potential from the breakthrough curves in Figure 5.

In some cases, electrochemical by-products may be more toxic than the original molecule. Since electrosorption is a non-Faradaic process, it is important to confirm the structural integrity of 2,4-D electrosorbed onto ACC fixed bed electrodes. For this purpose, an electrosorption experiment, described in our previous study (Bayram & Ayranci 2010), has been performed in cyclic mode using the ACC saturated with 2,4-D at +900 mV polarization as fixed-bed electrode. During electrosorption process, −900 mV potential was applied to the saturated ACC electrodes while fresh 0.01 M Na$_2$SO$_4$ solution was cycling with volumetric flow rate of 10 mL·min$^{-1}$ in the system and scanning-kinetic spectra were recorded in 2 min intervals. Results are shown in Figure 6. The inset in this figure represents the concentration-time profile by converting the absorbance data to concentration using the calibration relation at 230 nm.

Absence of observable shift in absorbance bands clearly confirms the structural integrity of 2,4-D and absence of undesired electrochemical reactions.
In a dynamic system, concentration-time profiles are generally known as breakthrough curves and are used for determining the capacity of the adsorbent and adsorbate concentrations in a water stream at any time. For industrial applications, adsorption columns are used in the process up to its saturation time, $t_S$, at which the effluent concentration reaches the feed concentration. Parameter $t_S$ is linked by a linear relationship to the saturation volume ($V_s$), which is the volume treated during the process up to $t_s$. The interpretation of the operation and performance of the fixed-bed may be evaluated by characteristic parameters determined from the breakthrough curves and graphical integration of Equation (1)

$$X_s = \frac{\int_0^{V_s} (C_0 - C)dv}{m}$$  \hspace{1cm} (1)$$

where $C_0$ is the initial concentration of solute and $c$ is the concentration at any time, $m$ is the mass of the ACC fixed bed electrode. Thus, the adsorption/electrosorption capacities at the saturation point ($X_s$) can be used for interpretation of the performance of the electrosorption process and ACC fixed-bed electrodes. $X_s$ may also be defined as the ratio of the quantity of the solute adsorbed at the saturation point to the mass of ACC and can be used in quantifying the results. The calculated parameters for OC adsorption and electrosorption of 2,4-D onto ACC fixed-bed electrodes are given in Table 1.

Table 1: Parameters calculated for OC adsorption and electrosorption of 2,4-D onto ACC fixed-bed electrodes

<table>
<thead>
<tr>
<th>Polarization/ mV</th>
<th>$X_s$ / mg·gACC$^{-1}$</th>
<th>$V_s$ / L</th>
<th>$t_s$ / min.</th>
</tr>
</thead>
<tbody>
<tr>
<td>$-900$</td>
<td>291</td>
<td>1,1</td>
<td>110</td>
</tr>
<tr>
<td>$-300$</td>
<td>331</td>
<td>1,4</td>
<td>140</td>
</tr>
<tr>
<td>OC adsorption</td>
<td>409</td>
<td>1,8</td>
<td>180</td>
</tr>
<tr>
<td>+300</td>
<td>587</td>
<td>1,8</td>
<td>180</td>
</tr>
<tr>
<td>+900</td>
<td>729</td>
<td>2,1</td>
<td>210</td>
</tr>
</tbody>
</table>

compared to that under OC, proving the existence of lesser electrostatic attractions between charged ACC and ionized form of the 2,4-D pesticide.

Capacity for OC adsorption conducted in batch mode (Figure 4) can be calculated from the initial and equilibrium concentrations, molecular weight of 221.04 g·mol$^{-1}$ for 2,4-D and mass of ACC used in batch mode. It can then be used as a rough base for comparing the batch and flow-through modes. The calculated capacity for batch mode is 32 mg·gACC$^{-1}$ which is much smaller than that of the OC adsorption value of flow-through mode (Table 1). The huge difference between the two modes can be attributed to the improved mass transfer of 2,4-D in flow-through mode and to the quasi-three-dimensional structure of ACC electrode. Comparing the results with the literature studies performed on the removal of 2,4-D from aqueous solutions shows the improvements brought out with the present study. In the study of Deng et al. (2009) capacity for 2,4-D was calculated as 320 mg·g$^{-1}$ using biomass. In another study, capacity of 238 mg·g$^{-1}$ was obtained using activated carbons in a batch type reactor (Hameed et al. 2008). Recently, maximum removal capacity of 296 mg·g$^{-1}$ was reported for adsorption of 2,4-D onto few layer graphene adsorbent in a batch type reactor (Kamaraj et al. 2017). The maximum capacity achieved in the present study is quite high compared to those reported in literature for removal of 2,4-D from aqueous solutions. This achievement can be attributed to the enhanced attraction of 2,4-D by the polarized ACC fixed-bed electrodes and improved mass transfer rate by the flow regime.

Influence of volumetric flow rate

Change in concentration of 2,4-D with time during the course of electrosorption at $+900$ mV polarization and at different volumetric flow rates is shown in Figure 7.

A huge decrease in removal (increase in residual concentration) is observed as volumetric flow rate is increased.
from 10 to 30 mL·min\(^{-1}\). The flow rate of 10 mL·min\(^{-1}\) seems to give the highest removal rate. At the highest studied flow rate of 30 mL·min\(^{-1}\) \(X_S\) value decreases by a factor of 8.6 (from 729 to 84 mg·g\(^{-1}\)ACC) compared to the electrosorption at 10 mL·min\(^{-1}\). It is known that the electrosorption is an electrical double layer process. In that respect, the observed decrease in removal capacity with increasing flow rate can be attributed to the slimming of the electrical double layer which is formed on ACC surface in solution by the increased flow regime.

**Effect of Na\(_2\)SO\(_4\) on electrosorption of 2,4-D**

Industrial wastewaters usually contain different types of salts beside organic pollutants. In order to study the effect of an example electrochemically inert salt, Na\(_2\)SO\(_4\), on electrosorption of 2,4-D, experiments have been performed at optimum conditions of \(+900\) mV polarization and 10 mL·min\(^{-1}\) volumetric flow rate in \(2.0 \times 10^{-4}\) M 2,4-D solutions with and without 0.01 M Na\(_2\)SO\(_4\). Results are shown in Figure 8.

It can visually be seen that the existence of Na\(_2\)SO\(_4\) in aqueous solution of 2,4-D strongly affects the electrosorption of 2,4-D onto ACC fixed-bed electrodes. The increased capacity observed with Na\(_2\)SO\(_4\) can be ascribed to a salting-out effect (Conway 1981). The salting-out effect originates from association of water molecules with the ions of Na\(_2\)SO\(_4\) leaving less free water available for dissolution of organic species. The contribution of Na\(_2\)SO\(_4\) to the formation of electrical double layer formed on ACC also enhances the electrosorption through lengthening the charge field effect.

**CONCLUSIONS**

A flow-through electrosorption process was successfully applied for the removal of 2,4-D from aqueous solutions using a specially designed electrolytic cell in which an ACC fixed-bed electrode was polarized. Electrosorptive behavior of 2,4-D was correlated with the electrostatic interactions and dispersion forces between polarized ACC and 2,4-D species in solution. Improvements in electrosorption capacity were succeeded by adjusting volumetric flow rate and applied potentials. Maximum removal capacity of 729 mg·g\(^{-1}\)ACC for 2,4-D was achieved. Similar high removal capacities are expected for other ionizable, preferably aromatic, pesticide molecules which will lead the application of the present flow-through electrosorption process to real wastewaters.

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