


A resilience assessment framework for critical infrastructure networks' interdependencies

Maryam Imani  and Donya Hajjalizadeh

ABSTRACT

Critical infrastructures (CIs) provide essential services to the society. As infrastructures are becoming more interdependent, there is an increasing need for better management of their interactions and interdependencies. Interdependencies among CI can cause cascading failures and, hence, amplify negative consequences due to these failures. This can also affect CIs' service restoration rate and consequently reduce their resilience in coping with these hazardous events. The common challenge currently faced by CI asset owners is the lack of robust resilience-informed business planning and management strategies in response to interdependent assets' failures due to low-probability/high-impact hazards. This is of particular importance as CI owners and managers are investing more on improving the resilience of their assets in response to extreme environmental hazards. This study has approached CI nexus from the interdependency management point of view. It has developed an integrated resilience assessment framework to identify and map interdependency-induced vulnerabilities in critical infrastructure networks. This framework can potentially support effective management of the interdependencies in CI networks. The findings have been reflected in mapping the connection between the changes in resilience due to interdependency-induced failures and the cost of intervention scenarios, providing means of exploring shared intervention strategies.

Key words | asset management, critical infrastructure, infrastructure nexus, interdependency, resilience, vulnerability

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INTRODUCTION

Critical infrastructures (CIs), including water, energy and transport networks, provide essential services to society. As infrastructures are becoming more interdependent, there is an increasing need for better management of these interactions and interdependencies (Bloomfield *et al.* 2009). CIs' criticality means it is vital that these systems are resilient to any type of disturbances in the sense that they have an ability to resist failures and/or quickly resume their functionality when events occur (Mattioli & Levy-Bencheton 2014). Therefore, the pursuit of infrastructure resilience requires the reduction of failure probabilities, minimisation of negative consequences when failures do occur, and reduction in recovery time. The centralised nature of urban infrastructure and the interconnectedness between services implies that damage at any point in the system can have knock-on effects through the connections in the system and other infrastructure systems (Guthrie & Konaris 2012). Additionally, the

importance of protecting infrastructure from threats lies not only in its critical role of sustaining infrastructure, but also in its role of helping communities and the economy to rebuild themselves post-disruptions (Wang *et al.* 2010).

The continuity of operation and service in CI should be guaranteed with high design, operation and maintenance standards and a robust decision-making mechanism in place, following disturbing conditions at any scale. The UK government has published a POSTnote (The Parliamentary Office of Science & Technology 2010) and recognised short-term hazards, long-term climate change, and interdependencies as three issues surrounding the resilience of the core infrastructures. However, the common challenge currently faced by CI asset owners and managers is the lack of a robust resilience-informed business planning and management strategies in response to interdependent assets' failures due to low-probability/high-impact hazards.

To overcome the interdependency-induced challenges in CI networks and promote their resiliency, it is necessary to gain an understanding of interdependency relations in order to be able to incorporate resilience thinking into decision making. This could be facilitated through a robust interdependency modelling and analysis method. A number of approaches, from physical to functional and economic, have been proposed by different scholars in relation to CI's interdependencies modelling and analysis (Rinaldi *et al.* 2001; Glass *et al.* 2003; Casalicchio *et al.* 2004; Zimmerman 2004; Dudenhoeffer *et al.* 2006; Pye & Warren 2006; Rigole & Deconinck 2006; Schmitz *et al.* 2007) and (Xiao *et al.* 2008; Bloomfield *et al.* 2009; Solano 2010; Zhang & Peeta 2011). For example, the study conducted by Satumtira & Dueñas-Osorio (2010) categorised the interdependency modelling approaches according to mathematical method, modelling objective, scale of analysis, quality and quantity of input data, targeted discipline and end user type. Ouyang (2014) categorises the infrastructure interaction modelling approaches into six broad types of empirical, agent based, system dynamics based, economic theory-based, and network-based approaches.

Drawing on the above approaches, the available decision support systems (DSS) (e.g. iRoad, Neptune, etc.) rely on risk/vulnerability measures while interdependencies and their resilience in response to extreme hazards are overlooked. Several factors are involved in limiting the adoption of a resilience-informed decision making in the context of CI networks interconnectedness and interdependencies management such as high level of complexity and interconnection of the CI, growth of emerging challenges such as climate change. Hence, higher frequency of extreme weather conditions, rapid development and urbanisation, demand patterns' changes and many other reasons have been and will be challenging CI (Petit *et al.* 2015; Lin *et al.* 2017; Ani *et al.* 2019). This can also affect CI's service restoration rate and consequently reduce their resilience in coping with these hazardous environmental events. To reduce these impacts, an integrated resilience-informed decision support system (DSS) is required, to map interdependent network vulnerable components and introduce adaptive capacities accordingly. This is of particular importance as CI owners and managers are investing more and more every day on improving the resilience of their assets in response to extreme environmental hazards.

While many well-defined models and simulations exist for infrastructure sectors such as electrical power grid models, water networks, traffic flow, rail systems, computer networks, very few models exist that seek to tie these

infrastructures together in a form representative of their actual implementation. Jeziah *et al.* (2016) reviewed some of the most popular simulation tools under development such as CIPDSS, HAZUS, I2Sim/DR-NEP and ESRI Sim Disaster. However, a study by Dudenhoeffer *et al.* (2006) showed that many of the models present a physics/engineering-based approach and are very good at individual sector analysis, but they do not necessarily support high level command and control systems. In their study 33 tools were investigated and a few (e.g. Athena, CIP/DSS, FINSIM and RAPIDware) proved to be capable of modelling and analysing multiple infrastructure networks.

A holistic view is key in integrated infrastructure modelling since infrastructure networks and their dependencies are highly non-linear and complex and cannot be predicted with traditional models (Dirks *et al.* 2015). The benefit of integrated modelling in response to extreme events is to provide tools for decision makers to understand the dynamics and complexity of the system and avoid ineffective responses and poor coordination for rescue, recovery, restoration and, mitigation. This study has approached CI nexus from resilience-informed CI's interdependency management point of view. It thrived to fill the gap of resilience-informed decision making, in the context of interdependent CI networks, by adopting a diagnostic approach. Drawing on this, a resilience-assessment framework was developed to model infrastructure elements and the relation between individual components through network modelling approaches. In the proposed framework, the actions and interactions of each individual infrastructure element (nodes and links) is modelled with a view to assess their effects on the system as a whole. In this project, the nature of the connection is reflected in the flow from source asset (interdependency provider) to sink asset (interdependency receiver). More detail on the nature of interdependencies has been provided in the methodology section.

METHODS

The proposed integrated framework in this study comprises the following three folds: network modelling using Network Theory, failure propagation mapping and resilience assessment using system functionality over time.

Network modelling

In this study, Network Theory has been used to generate and characterize the topology of the hypothetical benchmark network, comprising three key infrastructures of water,

energy and transport, utilized for resilience evaluation of the interconnected infrastructure network. Glass *et al.* (2003) define networks as flexible abstractions that can be used to study the interaction behaviour of independent infrastructure systems. The abstraction manifests a series of nodes (e.g. power plants, transformers), links (e.g. distribution lines, information exchange, roads) and flows (e.g. energy, information or people) in a given infrastructure system. For the benchmark case study, a network of a total of 21 nodes, 20 links and five interdependent links is produced to illustrate the resilience-informed decision support system framework. These nodes and links represent different critical assets and their corresponding connections in each network; for example, generators, transmission lines, switches and breakers in an energy network; reservoirs, water mains, pumping stations in a water network and bridges, junctions, roads, rail lines in a transport network. The links between assets also represent the physical or any functional connection between two assets. In the case of interdependency links, these are connections between two different systems.

For the infrastructure network k , network properties can be represented by $\Gamma_k = \{N_{\Gamma_k}, E_{\Gamma_k}, M_{\Gamma_k}\}$, where N_{Γ_k} denotes the node sets, E_{Γ_k} denotes edge sets, and M_{Γ_k} is a $N_{\Gamma_k} \times N_{\Gamma_k}$ matrix representing the function of edges to pair-wise nodes. For a network consisting of v number of nodes and ω number of edges, Γ_k is given as Equation (1):

$$\Gamma_k: \left\{ \begin{array}{l} N_{\Gamma_k} = \{n_{\Gamma_k,1}, \dots, n_{\Gamma_k,v}\}, E_{\Gamma_k} = \{e_{\Gamma_k,1}, \dots, e_{\Gamma_k,\omega}\} \\ M_{\Gamma_k} = \{e_{\Gamma_k,j} \rightarrow (n_{\Gamma_k,i}, n_{\Gamma_k,z}), \forall j \in [1, \omega], i, z \in [1, v]\} \end{array} \right\} \quad (1)$$

Each member of M_{Γ_k} represents the connection between the source node, $n_{\Gamma_k,i}$, providing service through $e_{\Gamma_k,j}$, and the sink node, $n_{\Gamma_k,z}$, receiving service through $e_{\Gamma_k,j}$. Every node in the network can act as source, sink or both depending on the role of the asset in the network. For the energy network in the benchmark case study, with six nodes and five dependency links, the N_{Γ_E} , M_{Γ_E} can be written as Equations (2)–(4):

$$N_{\Gamma_E} = \{n_{\Gamma_E,1}, n_{\Gamma_E,2}, n_{\Gamma_E,3}, n_{\Gamma_E,4}, n_{\Gamma_E,5}, n_{\Gamma_E,6}\} \quad (2)$$

$$E_{\Gamma_E} = \{e_{\Gamma_E,1}, e_{\Gamma_E,2}, e_{\Gamma_E,3}, e_{\Gamma_E,4}, e_{\Gamma_E,5}\} \quad (3)$$

$$M_{\Gamma_E} = \left[\begin{array}{ccccc} 0 & 0 & 0 & 0 & 0 \\ (n_{\Gamma_E,2}, n_{\Gamma_E,1}) & 0 & (n_{\Gamma_E,2}, n_{\Gamma_E,3}) & 0 & (n_{\Gamma_E,2}, n_{\Gamma_E,5}) \\ 0 & 0 & 0 & (n_{\Gamma_E,3}, n_{\Gamma_E,4}) & 0 \\ 0 & 0 & 0 & 0 & (n_{\Gamma_E,3}, n_{\Gamma_E,6}) \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{array} \right] \quad (4)$$

Table 1 | Asset inventory attributes

$n_{\Gamma_k,i-xy}$	Node coordinates (illustrating the geographical location of each asset)
$n_{\Gamma_k,i-sc}$	Asset importance score (demonstrating asset type classification associated with the asset) and asset importance to the network – this is an expert-driven scoring system as a function on type of asset, no. users, value of the asset, age and condition of the asset, redundancy level and community classification, all scored from 0 to 5, latter being of most importance. For example, importance score of 214125 implies high score in community importance and low score in number of users and age and condition of the asset
$n_{\Gamma_k,i-Pf^0}$	Status-quo performance indicator of the asset
$n_{\Gamma_k,i-Rec^0}$	Recovery initiation time which is a function of asset importance score ($n_{\Gamma_k,i-sc}$)
$n_{\Gamma_k,i-FS}$	Magnitude of failure in functionality as a function of failure in the source node
$n_{\Gamma_k,i-f_{FP}}$	Failure propagation function given $n_{\Gamma_k,i-FS^t}$
$n_{\Gamma_k,i-f_{Rec}}$	Recovery process function as a function of $n_{\Gamma_k,i-FS^t}$ and $n_{\Gamma_k,i-sc}$
$n_{\Gamma_k,i-Pf^t}$	Asset performance indicator in time as a function of $n_{\Gamma_k,i-Pf^0}$, $n_{\Gamma_k,i-FS^t}$, $n_{\Gamma_k,i-f_{FP}}$, $n_{\Gamma_k,i-Rec^0}$ and $n_{\Gamma_k,i-f_{Rec}}$
$n_{\Gamma_k,i-f_c}$	Cost associated with fluctuation in level of service, recovery process, $n_{\Gamma_k,i-f_{Rec}}$ and $n_{\Gamma_k,i-sc}$

Each node, $n_{\Gamma_k,i}$, is a vector of asset inventory attributes. To simplify the complexity of engineering assets, this study has considered the essential attributes as tabulated in Table 1.

Among these attributes, $n_{\Gamma_k,i-f_{FP}}$, $n_{\Gamma_k,i-f_{Rec}}$ and $n_{\Gamma_E,i-Pf^t}$ are a function of time. $n_{\Gamma_E,i-Pf^t}$ is formed by the definition of $n_{\Gamma_k,i-f_{FP}}$, $n_{\Gamma_k,i-f_{Rec}}$, $n_{\Gamma_E,i-Rec^0}$ as demonstrated in Figure 1. The failure propagation function itself, $n_{\Gamma_k,i-f_{FP}}$, is dependent on the nature of the infrastructure asset and the imposed failure on the asset. Depending on failure nature, $n_{\Gamma_k,i-f_{FP}}$ can vary from abrupt change in performance indicator (opt. 1 and 5 in Figure 1) to a linear (opt. 3) or highly nonlinear behaviour as demonstrated in opt. 2 and 4 in asset attribute definition. Similar behaviour can be expected in the recovery process (i.e. $n_{\Gamma_k,i-f_{Rec}}$). In practice, these functions can be defined based on historical data on failures and recovery mechanism or design failure mechanism for each asset.

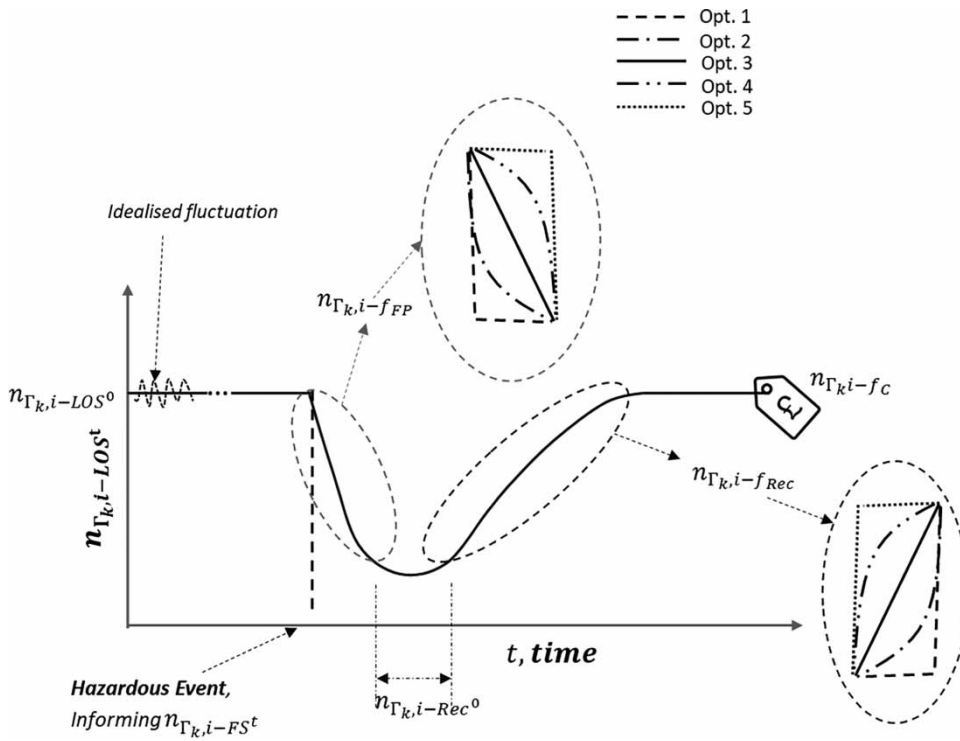


Figure 1 | Asset attribute definition.

In the case of an energy network, the attributes for the energy network can be summarised as Equation (5). For this study, the failure propagation pattern, $n_{\Gamma_E, i-f_{FP}}$, is simplified to an abrupt change, taking account of a failure propagation time (opt. 5). Similar assumption is made for recovery process using recovery duration time (i.e. opt. 1). The same assumption is extended to the other two networks in the benchmark case study (i.e. water and transport). Description of the actual failure propagation and recovery function is considered to be beyond the scope of this study.

The network system Γ_k itself is the subset of a multi-layered infrastructure system, Γ , containing mapping attributes of the interconnected u number of infrastructure systems. N_{Γ_k} and M_{Γ_k} , in turn, are subset of the multi-layered node vector and edge metric of N and M , respectively. The master edge metric, M , also contains the interdependency metrics, O representing the functional pathways of connectivity between different infrastructure systems. Therefore, Γ can be represented by Equation (6).

$n_{\Gamma_E, i}$	$n_{\Gamma_E, 1}$	$n_{\Gamma_E, 2}$	$n_{\Gamma_E, 3}$	$n_{\Gamma_E, 4}$	$n_{\Gamma_E, 5}$	$n_{\Gamma_E, 6}$
$n_{\Gamma_E, i-xy}$	[0.5, 1]	[0.5, 3]	[2.75, 5]	[6, 3.5]	[2, 1.5]	[5, 5.5]
$n_{\Gamma_E, i-sc}$	221555	544344	221555	555125	334324	544344
$n_{\Gamma_E, i-PI^0}$	5	15	5	50	10	15
$n_{\Gamma_E, i-Rec^0}$	1	1	6	9	10	1
$n_{\Gamma_k, i-FS}$	100%	100%	100%	100%	100%	100%
$n_{\Gamma_E, i-f_{FP}}$	$n_{\Gamma_E, 1-f_{FP}}$	$n_{\Gamma_E, 2-f_{FP}}$	$n_{\Gamma_E, 3-f_{FP}}$	$n_{\Gamma_E, 4-f_{FP}}$	$n_{\Gamma_E, 5-f_{FP}}$	$n_{\Gamma_E, 6-f_{FP}}$
$n_{\Gamma_E, i-f_{Rec}}$	$n_{\Gamma_E, 1-f_{Rec}}$	$n_{\Gamma_E, 2-f_{Rec}}$	$n_{\Gamma_E, 3-f_{Rec}}$	$n_{\Gamma_E, 4-f_{Rec}}$	$n_{\Gamma_E, 5-f_{Rec}}$	$n_{\Gamma_E, 6-f_{Rec}}$
$n_{\Gamma_E, i-PI^t}$	$n_{\Gamma_E, 1-PI^t}$	$n_{\Gamma_E, 2-PI^t}$	$n_{\Gamma_E, 3-PI^t}$	$n_{\Gamma_E, 4-PI^t}$	$n_{\Gamma_E, 5-PI^t}$	$n_{\Gamma_E, 6-PI^t}$
$n_{\Gamma_E, i-f_c}$	301	591	136	756	695	724

(5)

$$\Gamma: \begin{cases} \mathbf{N} = \{N_{\Gamma_1}, \dots, N_{\Gamma_u}\} \\ \mathbf{M} = \begin{bmatrix} M_{\Gamma_1} & \dots & O_{\Gamma_1, \Gamma_j} & \dots & O_{\Gamma_1, \Gamma_u} \\ \vdots & \ddots & \vdots & \ddots & \vdots \\ O_{\Gamma_j, \Gamma_1} & \dots & M_{\Gamma_j} & \dots & O_{\Gamma_j, \Gamma_u} \\ \vdots & \ddots & \vdots & \ddots & \vdots \\ O_{\Gamma_u, \Gamma_1} & \dots & O_{\Gamma_u, \Gamma_j} & \dots & M_{\Gamma_u} \end{bmatrix}, O_{\Gamma_j, \Gamma_l} = \{g_{\Gamma_j, \Gamma_l, s} \rightarrow (n_{\Gamma_j, r}, n_{\Gamma_l, s}), \forall j, l \in [1, k], j \neq l\} \end{cases} \quad (6)$$

Similar attributes to nodes are defined for each link representing dependency and interdependency connection, $e_{\Gamma_k, j}$ and $g_{\Gamma_j, \Gamma_l, s}$, respectively. Replacing the coordinates attribute, the sink-source vector is recorded as $e_{\Gamma_k, j-OD}$ and $g_{\Gamma_j, \Gamma_l, s-OD}$ for dependency and interdependency links, respectively. Similar to nodes, the state condition of the (inter)dependency links, $g_{\Gamma_j, \Gamma_l, s-FS}$, varies from 0 to 1, whereby 1 implies there is a full service flow from a source node, $n_{\Gamma_j, r}$ to a sink node, $n_{\Gamma_l, s}$ at time t .

For the benchmark case study with three subsystems and five links of interdependencies, two of which are energy-transport, one energy-water, one water-energy and one water-transport, \mathbf{M} and $\mathbf{O}_{\Gamma_j, \Gamma_l}$ can be written as Equations (7)–(10):

$$\mathbf{M} = \begin{bmatrix} M_{\Gamma_T} & O_{\Gamma_T, \Gamma_W} & O_{\Gamma_T, \Gamma_E} \\ O_{\Gamma_W, \Gamma_T} & M_{\Gamma_W} & O_{\Gamma_W, \Gamma_E} \\ O_{\Gamma_E, \Gamma_T} & O_{\Gamma_E, \Gamma_W} & M_{\Gamma_E} \end{bmatrix} \quad (7)$$

$$\mathbf{O}_{\Gamma_E, \Gamma_T} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & (n_{\Gamma_E, 4}, n_{\Gamma_T, 9}) \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & (n_{\Gamma_E, 6}, n_{\Gamma_T, 8}) & 0 & 0 \end{bmatrix} \quad (8)$$

$$\mathbf{O}_{\Gamma_E, \Gamma_W} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & (n_{\Gamma_E, 5}, n_{W, 2}) & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad (9)$$

$$\mathbf{O}_{\Gamma_T, \Gamma_E} = [0] \quad (10)$$

Figure 2 demonstrates the network configuration with the specified dependency and interdependency connections.

Failure scenarios and failure propagation

As the functionality of each system and the continuity of the functionality are of utmost importance for asset owners and managers, in this study, failure in a system is defined as any

event resulting in loss of functionality. The functionality of each system can vary depending on the decision-making criteria but ultimately, for utility services, this is tied to continuity of service provision to end-users.

Each component in a system can either be responsible for providing service directly to users or indirectly supporting component(s) that provide service directly, defined as $n_{\Gamma_k, i-PJ^0}$. Hence, the functionality of the entire system in status-quo is defined as aggregation of the number of users receiving service from the system, $\sum_{r=1}^{v_{\Gamma_j}} n_{i, r-PJ^0}$. The failure scenarios are then defined as percentage of loss of functionality for each failed component.

To generalise the analysis, the failure scenarios are defined regardless of the origin, type and severity of the initiating hazardous event (e.g. extreme rainfall, earthquake, etc.), so called ‘failure state’. Failure state represents the condition (operational condition and/or physical condition) of a network, causing a negative impact on network performance (partially or fully), regardless of the initiating source. The impact of these failure scenarios is reflected in the number of users remaining in service, $n_{\Gamma_k, i-PJ^t}$. Figure 3(a) illustrates an example of a single failure scenario, where asset 3 in energy network has lost 100% functionality (i.e. $n_{\Gamma_E, 3-FS} = 100\%$) at time t_0 , resulting in 5% immediate loss of users in this asset.

In case of failure of a source node $n_{\Gamma_j, r}$ at t_x , the magnitude of functionality on link $g_{\Gamma_j, \Gamma_l, s-FS}$ reduces to $n_{\Gamma_j, r-FS^t} \times g_{\Gamma_j, \Gamma_l, s-FS^t}$ by time $t_x + g_{\Gamma_j, \Gamma_l, s-f_{FP}}$. This is then reflected in sink node performance indicator reaching $n_{\Gamma_j, r-PJ^t} \times g_{\Gamma_j, \Gamma_l, s-FS^t}$ at time $t_x + g_{\Gamma_j, \Gamma_l, s-f_{FP}} + n_{\Gamma_j, r-f_{FP}}$. In a similar pattern, the failure will continue to propagate to the downstream source-sink pair to reach sink-only nodes (nodes with no service providing role). In the previous example and assuming that the failure in all assets propagates with a rate of 3 h per link ($g_{\Gamma_j, \Gamma_l, s-f_{FP}} = 3h$), this scenario will result in failure of assets 4 and 6 in energy network and assets 8 and 9 in the notational transport network at time $t_0 + 3h$. The impact on total number of users (system functionality) is demonstrated in Figure 3(b).

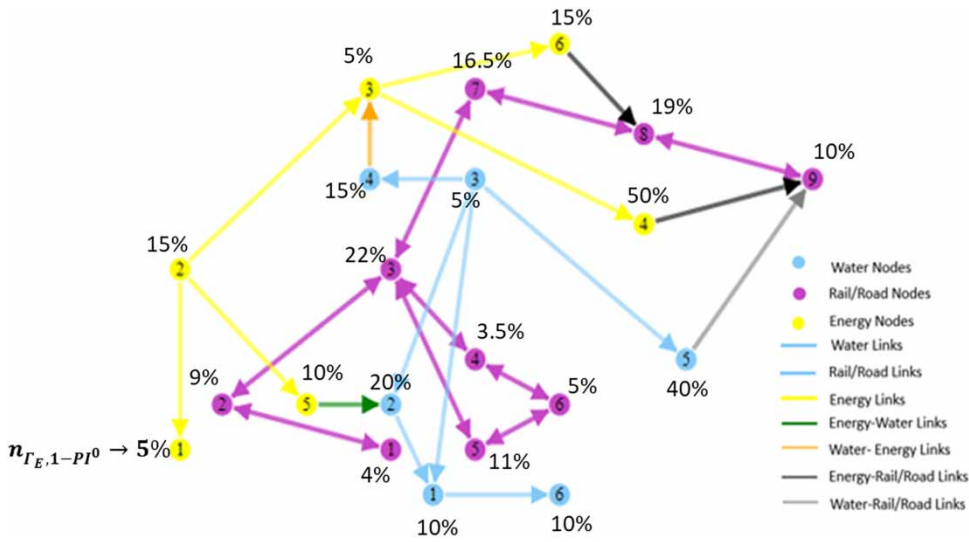
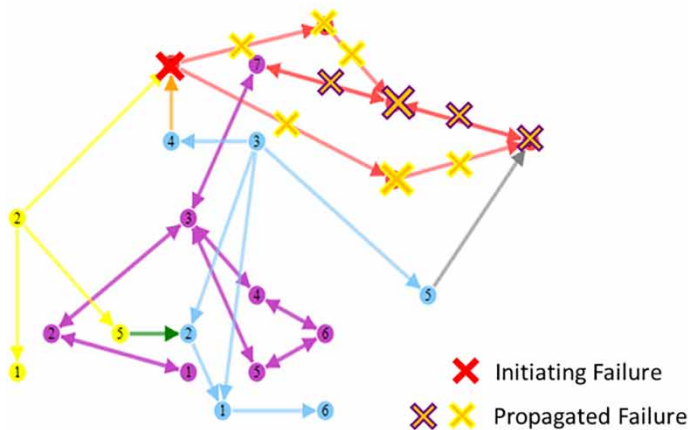


Figure 2 | Benchmark case study network.

(a)



(b)

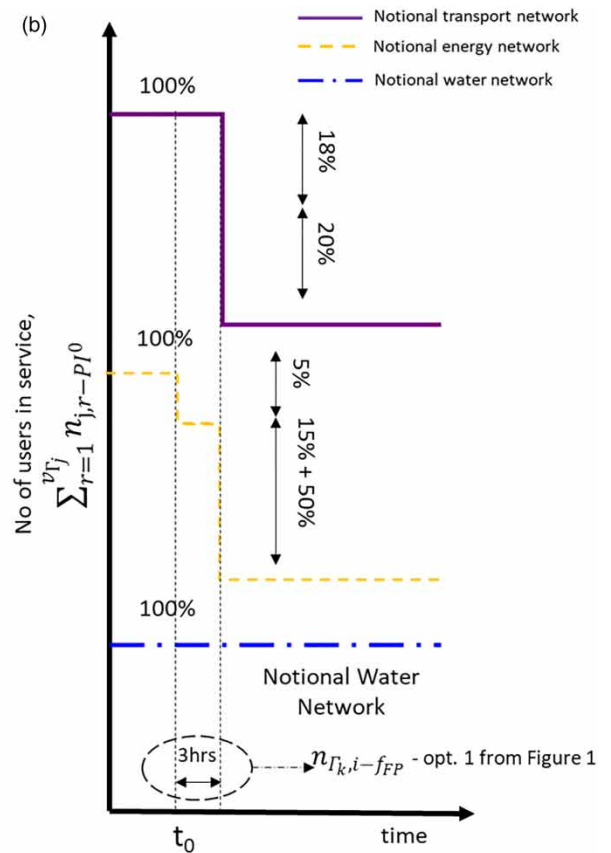


Figure 3 | (a) Failure propagation map for the node 3E; (b) corresponding functionality diagrams for each network.

Resilience assessment

In recent years, resilience of infrastructure has received significant attention and interest among different regulatory bodies, practitioners and researchers in four domains of organisational, social, economic and engineering, the latter being the focus of this study. Literature on definition of resilience indicates that there is not a consensus in the definition and even in engineering context, it varies for different systems' specifications and stakeholders' priorities and values. With resilience being a multi-disciplinary, cross-sectorial and complex context, it is crucial to establish a common understanding of the definition amongst all stakeholders (Ceré et al. 2017).

Considering that the performance of an engineering system is linked to its functionality, it is inevitable that the resilience of an engineering system gets defined as a function of performance indicator over time. In recent years there have been several studies exploring different resilience metrics as a function of system performance (Berkeley III & Wallace 2010; Wang et al. 2010; Hoque et al. 2012; Pant et al. 2014; Barker et al. 2015). To capture key inherent system properties such as robustness, recoverability, rapidity and resourcefulness in response to a failure event, a two-dimensional metric has been utilised in this study to quantify resilience.

For this purpose, resilience is defined as the area covered by the performance indicator diagram. Reflecting on the previous example upon the recovery of the failed asset(s), the performance indicator of the failed asset will bounce back to its initial performance indicator prior to failure by $t_x + g_{\Gamma_j, \Gamma_{L_s} - f_{FP}} + n_{\Gamma_j, r - f_{FP}} + n_{\Gamma_j, r - Rec^0} + n_{\Gamma_j, r - f_{Rec}}$. The

performance indicator of the assets with propagated failure will be restored to its initial state at the very same time. This assumption neglects the recovery travelling time between dependent and interdependent assets. After completion of the recovery process, the resilience can be calculated using Equation (11):

$$network\ resilience_{\Gamma_j} = \int_t^{\nu_{\Gamma_j}} n_{\Gamma_j, r - PI} \tag{11}$$

Figure 4(a) demonstrates the performance function for all three networks in response to failure of asset 3 in energy network and its subsequent recovery, assuming abrupt recovery with 4 h duration and 1 h recovery initiation (i.e. $n_{\Gamma_k, i - f_{Rec}} = 3h$), $n_{\Gamma_k, i - Rec^0} = 1hr$. Figure 4(b) demonstrates the impact of 1 h difference in recovery duration for the same failure scenario. This can be translated to change in recovery strategy either from resources point of view or rapidity of the resources available to a system. To better compare different recovery strategies, a concept entitled 'level of resilience' is introduced herein that demonstrates the resilience level in a network pre and post interventions. These values can be interpreted as acceptable risk zones in resilience context. The thresholds for each zone of resilience can vary depending on expert judgment on what is acceptable or tolerable for each system. The unit for these thresholds is 'number of user in service × time'. Hence, three resilience zones of low resilience zone (in red), medium resilience zone (in amber) and high resilience zone (in green) are created (Figure 4(c)). The improvement in recovery strategies can include increase in

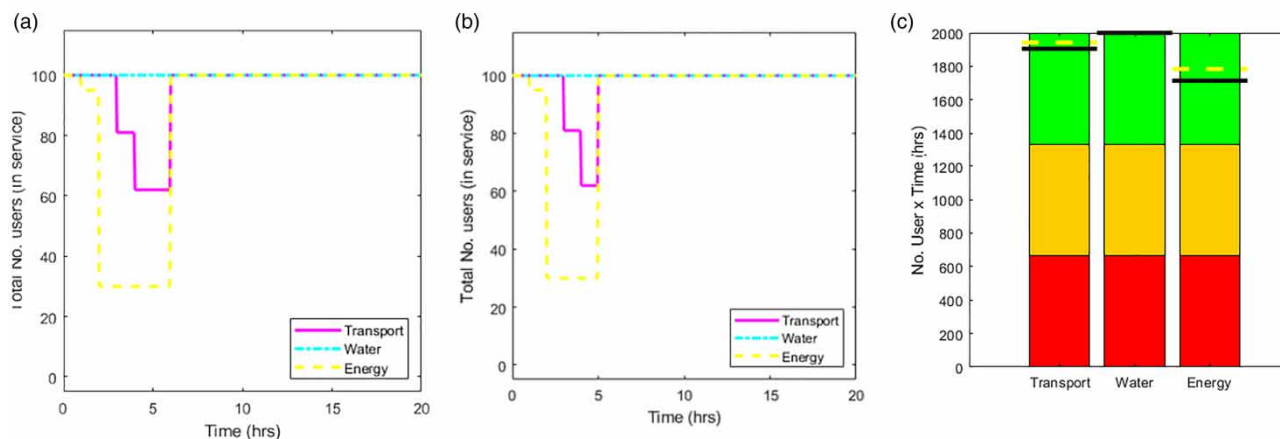


Figure 4 | (a) Change in performance indicator considering the recovery of the failed asset (2E) assuming recovery duration of 3 h; (b) assuming recovery duration of 2 h; (c) resilience level bar charts.

redundancy, robustness or resourcefulness in different parts of the interdependent network. It can be seen from this figure that for an hour change in recovery duration, the resilience of energy network changes from 1,750 (no. users \times time) to 1,800. Assuming unit cost of £100,000/(no. users \times time), this change represents £500,000 saving in resilience. This value then can represent the benefit in recovery measure against the cost of the recovery.

RESULTS AND DISCUSSION

It is crucial for infrastructure asset owners to have a better understanding of the dynamics of their networks' 'interdependency zones', their resilience levels and the impacts of the resilience changes across the integrated network. This will enable them to track the failure propagation at times of failure to make resilience-informed decisions for shared interventions. To demonstrate the importance of interdependency interactions, Figure 5 illustrates the impact of each single failure scenario on the entire network for all three notional networks. For this purpose, the impact of all single failure scenarios is simulated and reported as aggregated loss in number of users per network, shown by thickness of strands in the Figure 5. As can be expected each asset has an impact on the owner network which is typically monitored during the design and maintenance of

a network; however, the impact of interdependency-induced failures, shown here by different shades of grey colour for each network, are hidden to each network. Depending on level of interdependencies, this implies that a network may be vulnerable and sensitive to failure scenarios that not only have not been monitored during the design process but also are not under radar for maintenance purposes. As can be seen from Figure 5, given the dependency of the notional transport network on energy and water, failure in either one of these networks can result in equally significant loss of functionality in the network and if not considered in maintenance strategies could result in considerable costs and customer dissatisfaction.

To link the interdependency behaviour to graph theory driven properties, Figure 6 demonstrates the ranking of each nodal asset according to four importance metrics: (i) degree: measuring number of incoming edges to each node; (ii) betweenness: measuring the frequency of each node appearing on a shortest path between two nodes in the graph; (iii) out-closeness: measuring the inverse sum of the distance from a node to all other nodes; and (iv) in-closeness: measuring the inverse sum of the distance from all other nodes to a node. The intensity of colour (shade of grey) for each node demonstrates the ranking of the node in the entire multi-layered network. The first rank is shown by white colour.

As can be seen in Figure 6, betweenness is the closest metric to the findings of Figure 5; however, these metrics

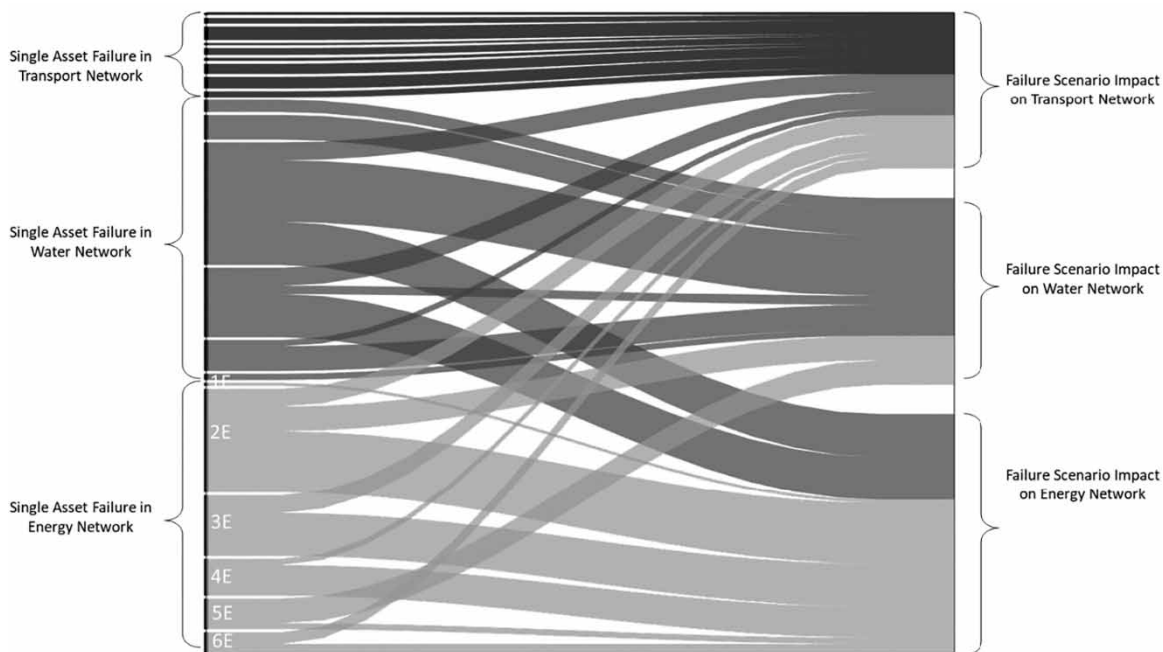


Figure 5 | Impact of single failure scenarios on three notional infrastructures.

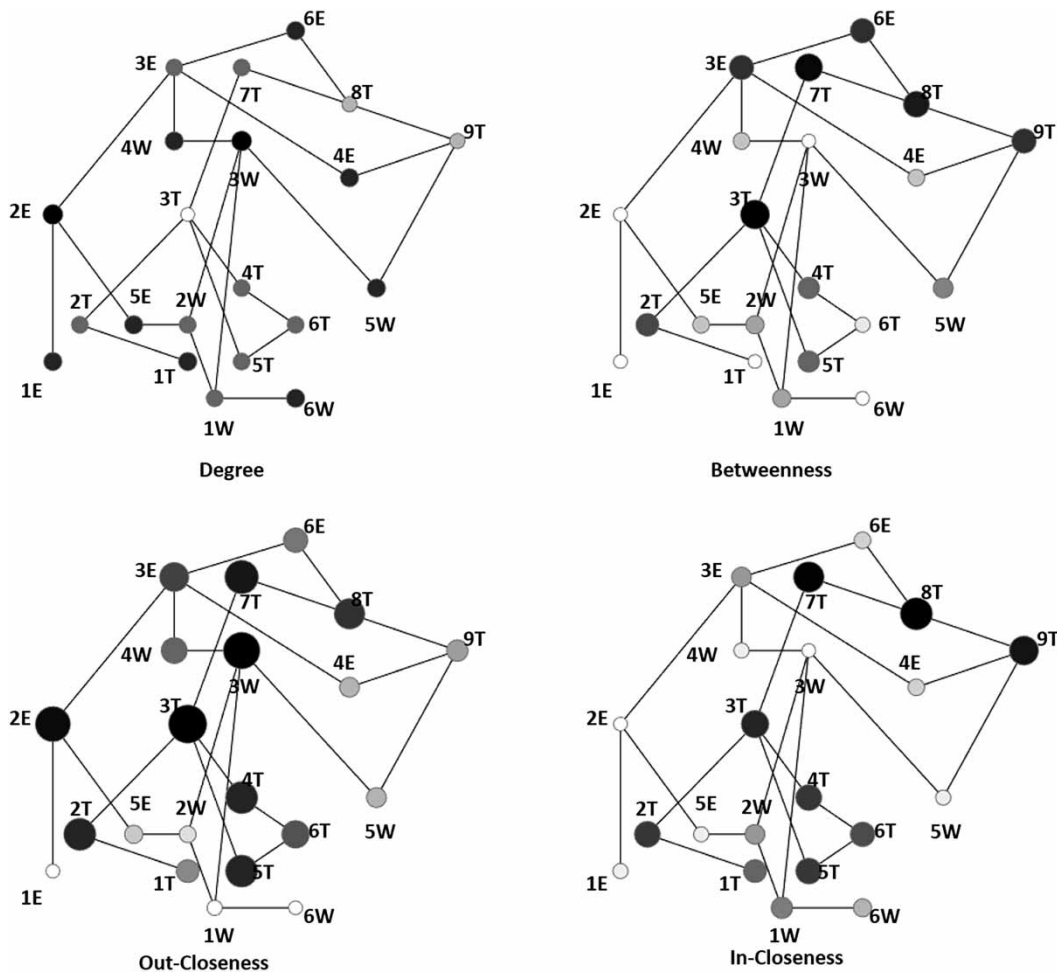


Figure 6 | Notional multi-layered network graph properties.

are rather limiting in terms of information they provide for decision making purposes. Furthermore, these properties can be calculated assuming that the information for all connected networks is accessible, which generally is not the case in practice.

Extending the failure scenarios considered to multi failure scenarios, Figure 7 demonstrates the resilience value versus maximum failure for all single-, double- and triple-concurrent failure scenarios. Each grey dot in Figure 7 represents a failure scenario and its impact on the loss of number of users for each notional network and resilience metric (considering a constant recovery duration and initiation for all scenarios). The area of the plot is divided into four zones for emphasis on criticality of failure scenarios. For example, a zone with high loss of functionality and low resilience is shown in a dark shade of grey and, in contrast, a zone with high resilience and low loss of functionality is shown in white.

As each notional network has some level of interdependencies, the trend in scattered scenarios is not entirely linear and as this level of interdependency increases (notional transport network in this example), so does the nonlinearity behaviour. This behaviour becomes more pronounced as the scenarios change from single to triple-concurrent failure scenarios.

CONCLUSION

This study presents the feasibility study of the resilience-informed decision support system framework by creating and testing a framework and its application to a numerical case study. This framework could be expanded and upgraded to other critical infrastructure networks (e.g. ICT) for more comprehensive analysis of interconnected systems.

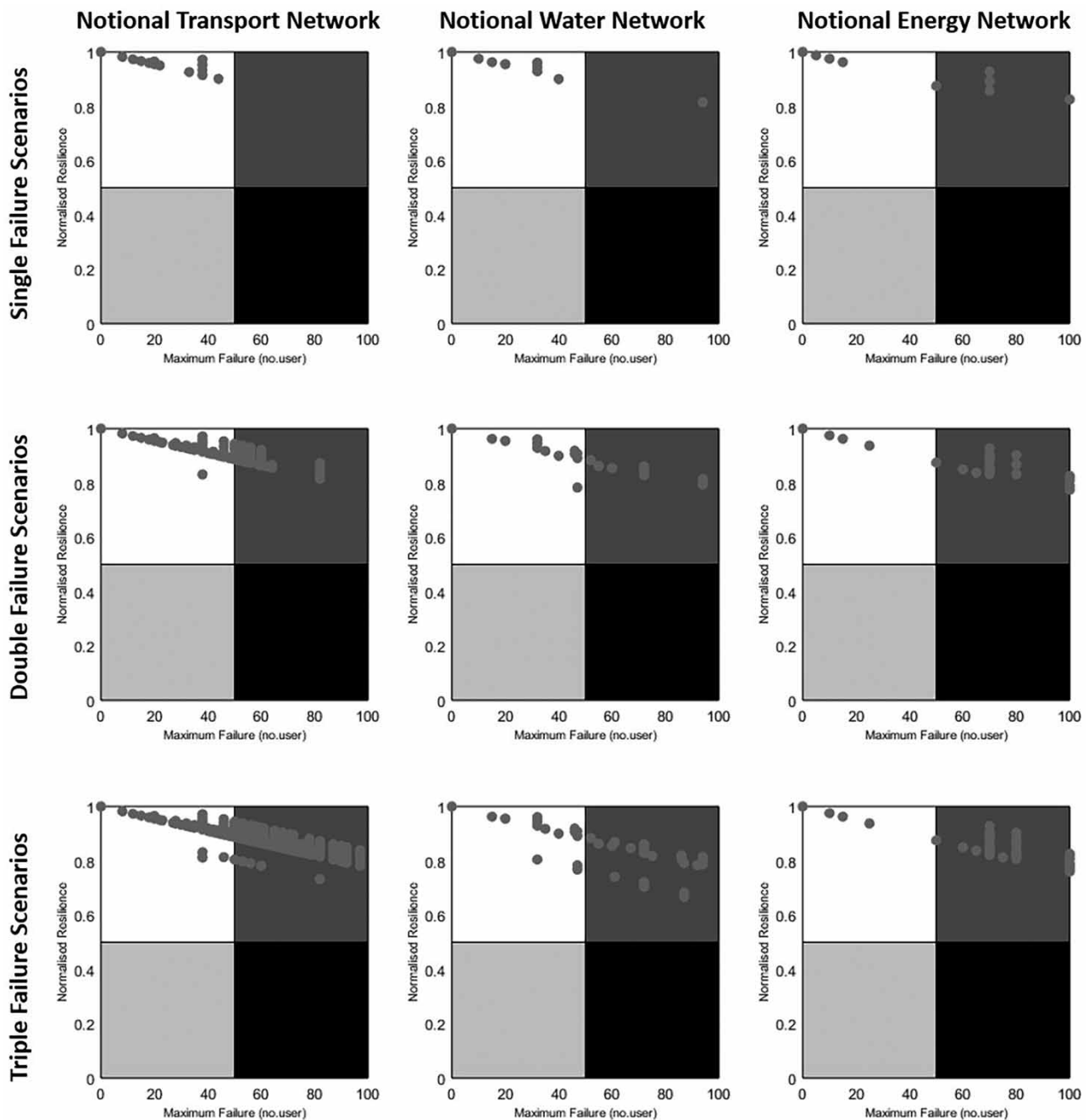


Figure 7 | Resilience vs maximum failure for all one, two and three concurrent failure scenarios.

The results show that as the level of interdependency increases, the nonlinearity behaviour increases. This behaviour becomes more pronounced as the scenarios change from single to triple-concurrent (or n -concurrent) failure scenarios. Failure to integrate modelling and overlooking these non-linearities can lead to underestimated failure impacts and consequently, inappropriate or insufficient interventions and eventually investments.

As can be expected, each asset has an impact on the owner network which is generally monitored during the design and maintenance of a network; however, the impacts of interdependency-induced failures, depending on level of interdependencies, imply that a network may be vulnerable and sensitive to failure scenarios that have not been monitored during the design process, and they are likely to be not considered for maintenance purposes. This highlights

the importance of shared intervention schemes in interdependent infrastructures.

As demonstrated using the notional example, resilience-informed decision making can complement the conventional risk-informed decision making for infrastructure management, particularly in dealing with low-probability high-impact events. Additionally, enhanced critical infrastructure interdependencies management requires collaboration and shared intervention amongst all the role players leading to effective transformation of the investment strategies in critical infrastructure sectors. Therefore, it is crucial for infrastructure asset owners to have a better understanding of the dynamics of their networks' 'interdependency zones', their resilience levels and the impacts of the resilience changes across the integrated network. This will enable them to track the failure propagation at times of failure to make resilience-informed decisions for shared interventions.

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